

**DOCUMENT ADDENDUM
FINAL LOCATION HYDRAULIC REPORT**

**S.R. 39
FROM I-4 to U.S. 301
HILLSBOROUGH AND PASCO COUNTIES, FLORIDA**

**Work Program Item Segment Nos: 255099 1 & 256289 1
Federal Aid Project No: F-321-1(4)**

This proposed project involves multi-lane improvements to S.R. 39 and the proposed extension of the Alexander Street Bypass from I-4 in Hillsborough County to U.S. 301 in Pasco County, a distance of approximately 21.2 km (13.2 mi)

Prepared for:

**Florida Department of Transportation
District Seven
11201 North McKinley Drive
Tampa, Florida 33612**

April 2001

The attached Final Location Hydraulic Report (LHR) was completed in October 1999. This addendum provides updated project information that was not available in the previous LHR that was available for public review prior to and at the Public Hearing that was held on April 20, 2000. This addendum improves consistency between the LHR and the Environmental Assessment/Finding of No Significant Impact (EA/FONSI) that was approved by the Federal Highway Administration (FHWA) on November 14, 2000.

INTRODUCTION

Through the Project Development and Environment (PD&E) Study process, the Florida Department of Transportation (FDOT) evaluated the expansion of S.R. 39 to a four-lane facility from the vicinity of Joe McIntosh Road in Hillsborough County to the vicinity of U.S. 301 in Pasco County (Addendum Figure 1). In addition, the FDOT evaluated the extension of Alexander Street Bypass as a four-lane facility from Interstate 4 (I-4) northward to S.R. 39 in the vicinity of Joe McIntosh Road.

The S.R. 39 corridor is functionally classified as a north/south minor arterial facility between I-4 and U.S. 301. S.R. 39 is part of the Federal-Aid Primary and State Highway System and is classified as an emergency evacuation route. The project limits extend from I-4 in Plant City and Hillsborough County to U.S. 301 in Pasco County, a distance of 21.2 kilometers (km) [13.2 miles (mi)].

The existing S.R. 39 within the project limits contains a two-lane undivided typical section with 3.658 meter (m) [12 foot (ft)] wide travel lanes, 1.219 m (4 ft) paved shoulders, and open roadside ditches on both sides of the roadway. The existing right-of-way (ROW) varies from 18.288 m (60 ft) to 45.720 m (150 ft).

S.R. 39 is currently a two-lane undivided roadway with drainage ditches adjacent to the existing roadway. A CSX Transportation railroad line parallels the existing roadway on the east side of S.R. 39 for approximately 17.7 km (11.0 mi) from the existing S.R. 39 and I-4 intersection to a point just north of Crystal Springs in Pasco County.

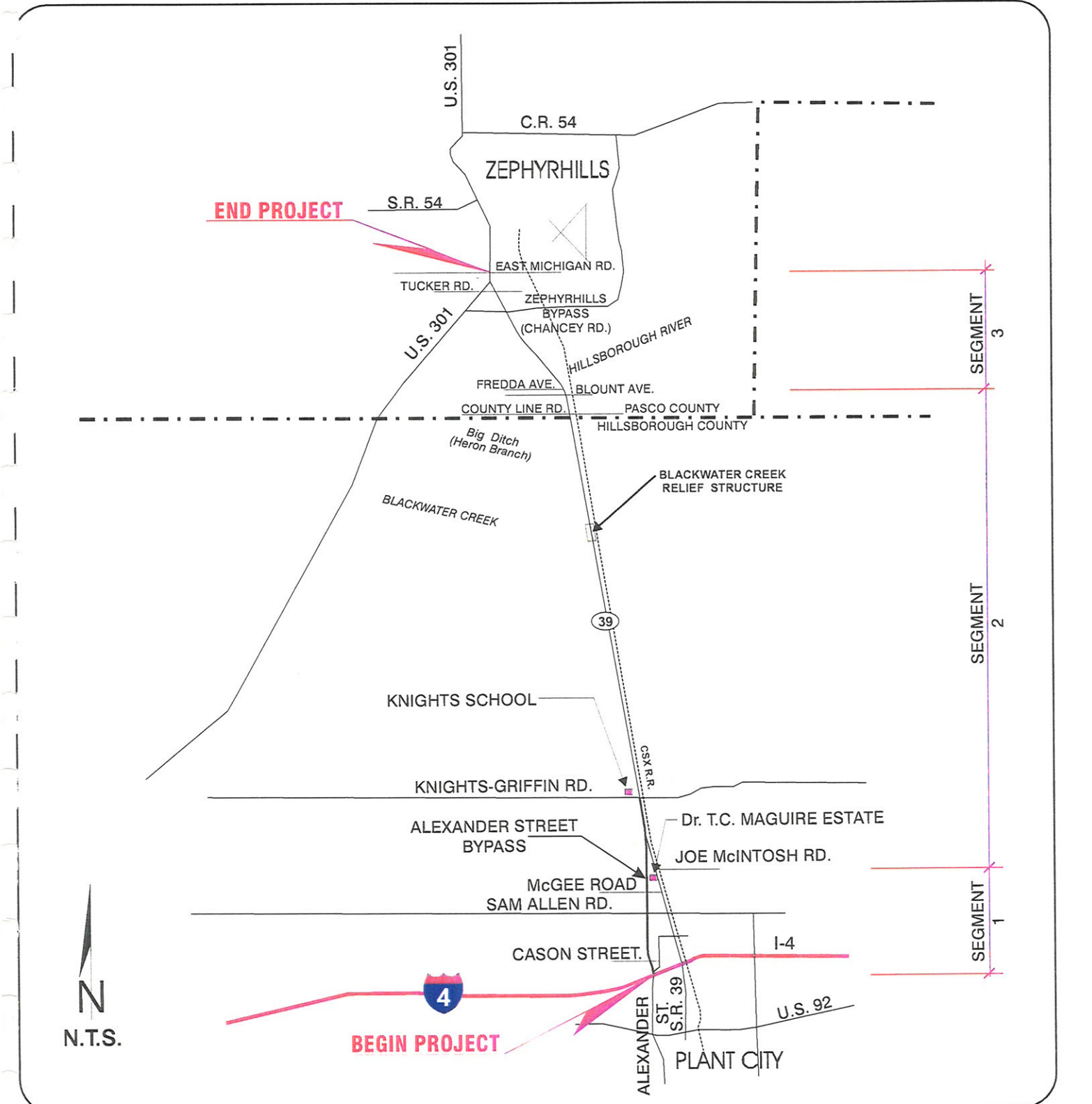
PROPOSED IMPROVEMENTS

The FHWA approved project involves multi-lane improvements to S.R. 39 and the planned extension of the Alexander Street Bypass from I-4 in Hillsborough County to U.S. 301 in Pasco County, a distance of approximately 21.2 km (13.2 mi). The Alexander Street Bypass portion from I-4 to the vicinity of Joe McIntosh Road is approximately 4.02 km (2.5 mi). This new alignment alternative is located to the west of S.R. 39 between I-4 and Joe McIntosh Road due to significant land use constraints on S.R. 39, including the Memorial Park Cemetery in the vicinity of I-4. Overall, improvements will consist of a four-lane divided roadway on new alignment (the Alexander Street Bypass) and improvement to S.R. 39 north of the merge point with the Alexander Street Bypass northward. The existing S.R. 39 north of the merge point will be improved from a two-lane undivided roadway to a four-lane divided facility.

DOCUMENT SPECIFIC UPDATES

This update to the LHR includes the following:

- Project Location Map has been updated (Addendum Figure 1).
- Refer to the Final Preliminary Engineering Report (October 2000) (PER) for project typical sections.
- All current FDOT design standards are to be used.
- Table 3 Proposed Cross Drain Information, missing from the October 1999 LHR has been included as part of this addendum (Addendum Table 3).



DR 13-
 CITY
 S.R. 39
 I.D.

FLORIDA DEPARTMENT OF TRANSPORTATION

S.R. 39
 From I-4 to U.S. 301
 Pasco County, Florida

PROJECT LOCATION MAP

Work Program Item Segment #: 255099 1 & 256289 1
 FAP #: F-321-1(4)

FIGURE 1

TABLE 3

PROPOSED CROSS DRAIN INFORMATION
S.R. 39 Location Hydraulics Report

Structure I.D.	Quantity	Type	Size CBC: m x m (ft x ft) RCP: mm (in)	Proposed Length m (ft)	Station (m)	Drainage Area hectares (acres)	Outfall Basin
AB-1	2	CBC	2.44 x 1.22 (8 x 4)	65.5 (215)	26 + 20	126 (312)	Pemberton Creek
AB-2	3	CBC (Bridge Culvert)	2.44 x 0.91 (8 x 3)	57.9 (190)	34 + 20	58 (144)	Pemberton Creek
AB-3	2	RCP	600 (24)	66.5 (218)	48 + 50	8 (20)	Hollomans Branch
AB-4	2	CBC	2.74 x 0.91 (9 x 3)	67.7 (222)	55 + 50	62 (153)	Hollomans Branch
AB-5	2	RCP	900 (36)	65.5 (215)	59 + 50	3 (7)	Hollomans Branch

FINAL LOCATION HYDRAULICS REPORT

**S.R. 39
FROM I-4 TO U.S. 301
HILLSBOROUGH AND PASCO COUNTIES, FLORIDA**

**Work Program Item Segment Nos: 255099 1 & 256289 1
Federal Aid Project No: F-321-1(4)**

This proposed project involves multi-lane improvements to S.R. 39 and the proposed extension at the Alexander Street Bypass from I-4 in Hillsborough County to U.S. 301 in Pasco County, a distance of approximately 21.2 kilometers (13.2 miles).

Prepared by:

**URS Corporation Southern
7650 W. Courtney Campbell Causeway
Tampa, Florida 33607**

October 1999

**DOCUMENT ADDENDUM
FINAL LOCATION HYDRAULIC REPORT**

**S.R. 39
FROM I-4 to U.S. 301
HILLSBOROUGH AND PASCO COUNTIES, FLORIDA**

**Work Program Item Segment Nos: 255099 1 & 256289 1
Federal Aid Project No: F-321-1(4)**

This proposed project involves multi-lane improvements to S.R. 39 and the proposed extension of the Alexander Street Bypass from I-4 in Hillsborough County to U.S. 301 in Pasco County, a distance of approximately 21.2 km (13.2 mi)

Prepared for:

**Florida Department of Transportation
District Seven
11201 North McKinley Drive
Tampa, Florida 33612**

April 2001

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EXECUTIVE SUMMARY

The proposed project involves multi-lane improvements to S.R. 39 from I-4 in Hillsborough County to U.S. 301 in Pasco County, a distance of approximately 21.2 kilometers (km) [13.2 miles (mi)]. From I-4 to the vicinity of Joe McIntosh Road, a segment of roadway on new alignment is being proposed, referred to as the Alexander Street Bypass, for a distance of approximately 4.02 km (2.5 mi). This new alignment alternative, located to the west of S.R. 39, is being proposed as an alternative to multi-lane improvements on S.R. 39 within these project limits due to significant land use constraints on S.R. 39, including the Memorial Park Cemetery in the vicinity of I-4. Overall, improvements will consist of a four-lane divided roadway on new alignment, the Alexander Street Bypass, and improvements to S.R. 39 on the existing alignment from the existing two-lane roadway to a four-lane divided facility. S.R. 39 is part of the Federal-Aid Primary and State Highway Systems, however, it is not classified as an emergency evacuation route.

This project involves modifications to existing drainage structures and would result in an insignificant change in their capacity to carry floodwater. This change would cause minimal increases in flood heights and flood limits. These minimal increases would not result in any significant adverse impacts on the natural and beneficial floodplain values or any significant change in flood risks or damage. There would not be a significant change in the potential for interruption or termination of emergency service routes. Therefore, it has been determined that this encroachment would not be significant.

This report addresses the existing and proposed cross drain structures and floodplain impacts for this project. Analyses were performed to determine preliminary sizes of all the proposed cross drain structures and the capacity of the "worst case," or critical existing cross drain for the 50-year storm event and 0.03 in (0.1-ft) of rise in headwater.

Five cross drains are proposed for construction along the new Alexander Street Bypass alignment, and are described in Table 1.

TABLE 1

**PROPOSED CROSS DRAINS
S.R. 39 Location Hydraulics Report**

Name	Location (m)	Size/Type
AB-1	26 + 20	Double 2.44 m x 1.22 m (8 ft x 4 ft) CBC
AB-2	34 + 20	Triple 2.44 m x 0.91 m (8 ft x 3 ft) CBC (Bridge Culvert)
AB-3	48 + 50	Double 600 mm (24 inches) RCP
AB-4	55+50	Double 2.74 m x 0.91 m (9 ft x 3 ft) CBC
AB-5	59+50	Double 900 mm (36 inches) CBC

The sizes provided in the above table are preliminary and may be revised in the final design stage of this project.

The critical existing cross drain that was analyzed is located at station 84 + 66, labeled D-5, which is immediately south of Lanier Road on the existing S.R. 39 alignment. Presently, D-5 is a double 1.83 m x 0.91 m (6 ft x 3 ft) CBC approximately 25.9 m (85 feet) long. The analysis shows that extending its length would not cause the headwater to rise more than 0.03 m (0.1 ft).

There are two bridges and one bridge culvert along the existing S.R. 39 alignment. The first bridge, proceeding north, traverses Blackwater Creek in Hillsborough County. The bridge crossing at Blackwater Creek is being studied by others and, therefore, is not described in detail in this LHR. A triple (3.05 x 1.22 m) (10- x 4-ft) CBC bridge culvert, crossing Big Ditch (also known as Heron Branch) is located in Hillsborough County. The second bridge is a 96.01 m (315-ft) steel girder bridge supported by timber piles crossing the Hillsborough River in Pasco County. The Hillsborough River is classified as an Outstanding Florida Water (OFW) and immediately downstream (west) of S.R. 39 it is a floodway as designated by the Federal Emergency Management Agency (FEMA). The addition of a bridge parallel to the existing bridge over the Hillsborough River would not cause adverse backwater effects.

Floodplain impacts would be kept to a minimum by using existing alignment and right-of-way to the extent possible. Avoidance of encroachments is not practical due to the high cost of changing the

roadway alignment. The proposed design indicates that there would be no significant impacts to the base flood, likelihood of flood risk, overtopping, or increased backwater.

SECTION 1.0
INTRODUCTION

The Florida Department of Transportation (FDOT) is conducting a Project Development and Environment (PD&E) Study to evaluate multi-lane improvement alternatives for the S.R. 39 study corridor from I-4 to U.S. 301 in Hillsborough and Pasco Counties, Florida

The objective of the PD&E Study is to provide documented environmental and engineering analyses that will help the FDOT and the Federal Highway Administration (FHWA) reach a decision on the type, conceptual design, and location of the necessary improvements along the S.R. 39 corridor to accommodate future transportation needs in a safe and efficient manner.

1.1 PROJECT DESCRIPTION

The proposed project involves multi-lane improvements to S.R. 39 from I-4 in Hillsborough County to U.S. 301 in Pasco County, a distance of approximately 21.2 kilometers (km) [13.2 miles (mi)]. From I-4 to the vicinity of Joe McIntosh Road, a segment of roadway on new alignment is being proposed, referred to as the Alexander Street Bypass, for a distance of approximately 4.02 km (2.5 mi). This new alignment alternative, located to the west of S.R. 39, is being proposed as an alternative to multi-lane improvements on S.R. 39 within these project limits due to significant land use constraints on S.R. 39, including the Memorial Park Cemetery in the vicinity of I-4. Overall, improvements will consist of a four-lane divided roadway on new alignment, the Alexander Street Bypass, and improvements to S.R. 39 on the existing alignment from the existing two-lane undivided roadway to a four-lane divided facility. S.R. 39 is part of the Federal-Aid Primary and State Highway Systems, however, it is not classified as an emergency evacuation route. The S.R. 39 corridor is functionally classified as a north/south minor arterial facility between I-4 and U.S. 301.

The project is located within Sections 5, 6, 8, 17, and 20 of Township 28 South, Range 22 East; Sections 6, 7, 18, 19, 30, and 31 of Township 27 South, Range 22 East; and Section 1 of Township 27 South, Range 21 East in Hillsborough County and Sections 14, 23, 24, 25, and 36 of Township

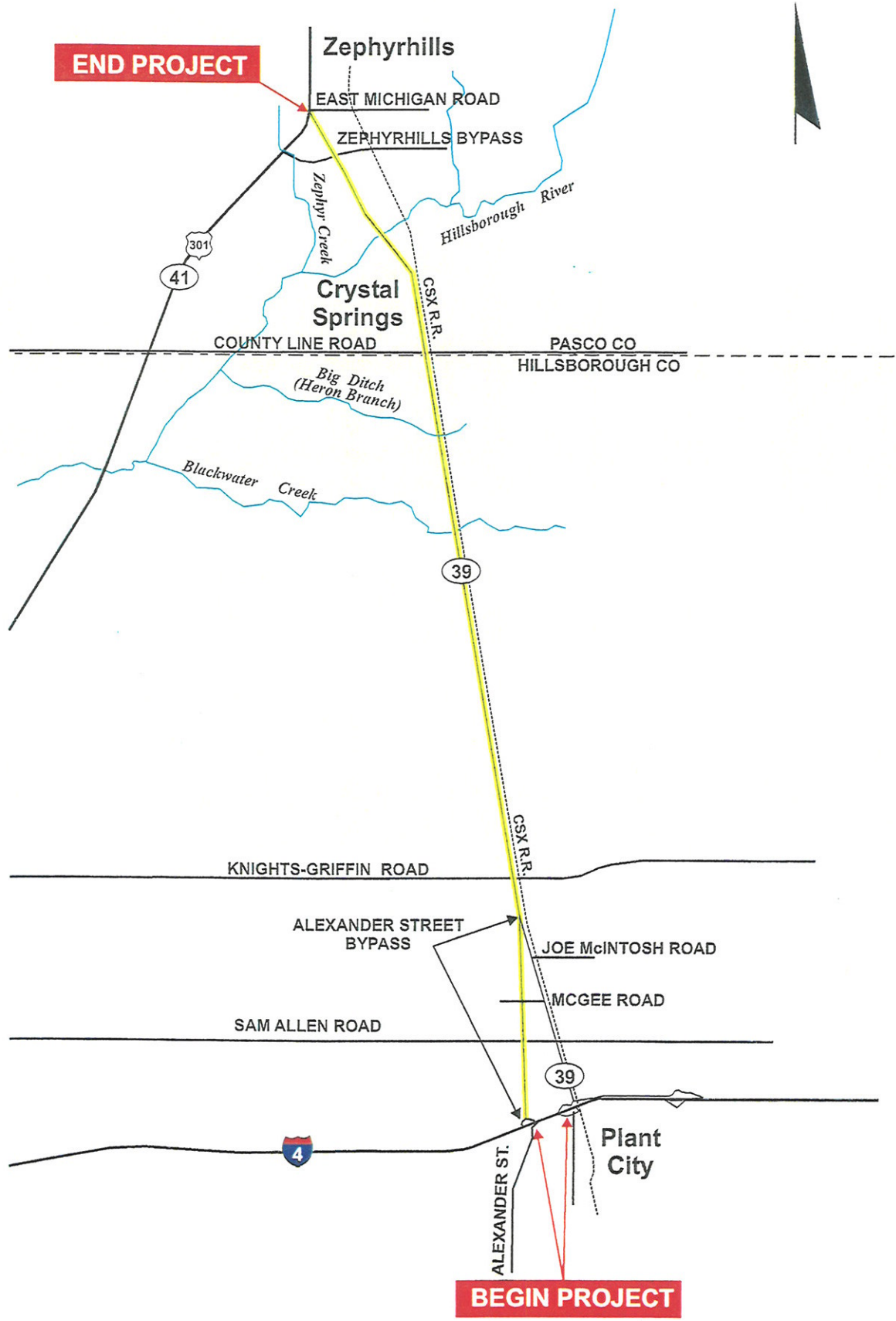
26 South, Range 21 East in Pasco County. The location and limits of the project are shown in Figure 1.

The project includes two bridges and one bridge culvert along the existing S.R. 39 alignment. The bridges include the crossings of the Blackwater Creek in Hillsborough County and the Hillsborough River in Pasco County. The bridge culvert crosses Big Ditch (Heron Branch) in Hillsborough County.

The Alexander bypass, approximately 4.0 km (2.5 mi) in length, will include crossings of upper tributaries of Pemberton Creek. Proposed typical sections will predominantly be rural with an urban typical section at the U.S. 301 intersection. The proposed improvements will provide a median ditch, upgrading two of the three bridge crossings, and extending or replacing the existing cross drains. The bridge crossings at Blackwater Creek are currently being designed (October 1999) for reconstruction/rehabilitation and details regarding these structures are contained in the Bridge Development Reports dated May 21, 1999 and August 1999. S.R. 39 in this project corridor is not designated as an evacuation route by the Tampa Bay Regional Planning Council.

S.R. 39 is currently a two-lane undivided roadway with drainage ditches adjacent to the existing roadway. A CSX Transportation railroad line parallels the existing roadway on the east side of SR 39 for approximately 17.7 km (11.0 mi) from the existing S.R. 39 and I-4 intersection to a point just north of Crystal Springs.

The existing land use patterns along the S.R. 39 corridor are both urban and rural in character. At the southern terminus, the Plant City urban district extends northward from I-4 to the vicinity of Sam Allen Road. This area is primarily residential in nature with minor commercial development. The Memorial Park Cemetery is located in the northwest quadrant of I-4 and S.R. 39. Land uses in the central portion of the study area from Sam Allen Road north to the vicinity of Zephyrhills consist of agricultural uses, rural residential development, vacant parcels, and a few commercial/industrial uses. Based on the Hillsborough County and Pasco County Comprehensive Plans, development activity adjacent to, and in the vicinity of, the S.R. 39 corridor is converting from agricultural land use to residential, commercial, and industrial land use. In addition, an ultra-light aircraft airport is



PROJECT LOCATION MAP
S.R. 39 FROM I-4 TO U.S. 301
 WPI SEGMENT No. 255099 1 FAP No. F-321-1(4)
 HILLSBOROUGH AND PASCO COUNTIES, FLORIDA

URS Greiner
 Figure 1

located to the east of S.R. 39. At the northern portion of the project in Zephyrhills, the land uses are primarily residential development.

The existing posted speed limit along the S.R. 39 corridor varies between 72 kilometers per hour (km/h) [45 miles per hour (mph)] and 86 km/h (55 mph).

1.2 GUIDELINES AND SOURCES

This Location Hydraulics Report (LHR) identifies impacts to the 100-year floodplains resulting from the proposed improvements, and is prepared according to the requirements set forth in Executive Order 11988, "Floodplain Management" and Federal Aid Policy Guide. Engineering specifics will be further addressed during the project design phase.

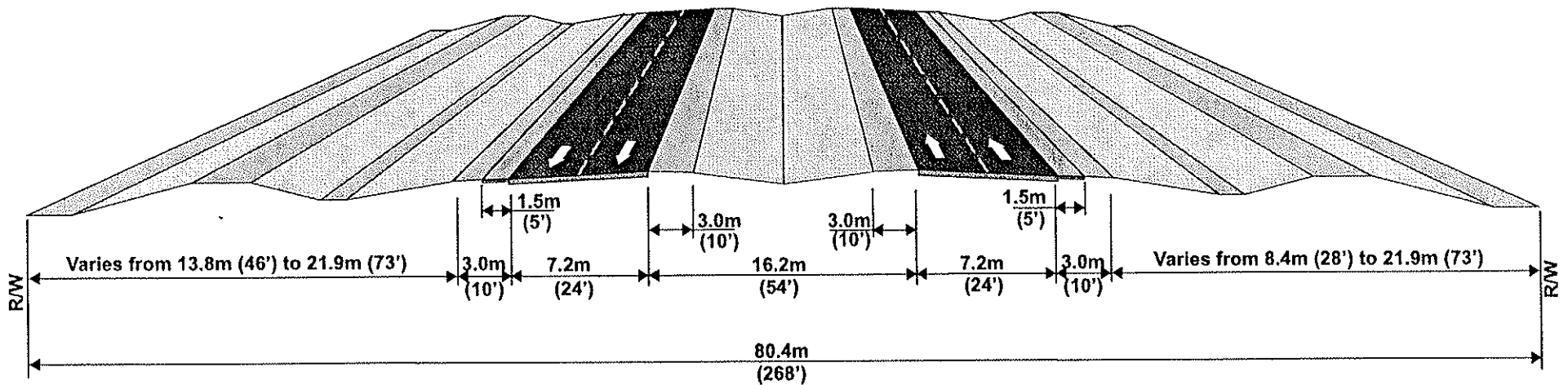
Sources of information for the investigation and development of this report include:

- USGS Quadrangle Maps;
- Southwest Florida Water Management District (SWFWMD) Contour Maps;
- FEMA Flood Insurance Rate Maps for Hillsborough and Pasco Counties;
- FEMA Flood Insurance Studies for Hillsborough and Pasco Counties;
- Soil Surveys of Hillsborough and Pasco Counties;
- Florida Department of Transportation S.R. 39 Widening Plans;
- Recent I-4 Plans and Drainage Calculations;
- City of Plant City, Westside Canal Stormwater Management Master Plan; and
- Floodplain Information on the Blackwater Creek and Hillsborough River Watershed by SWFWMD.

A detailed list of references is provided in Section 10.0 of this document.

The scope of this report covers general planning information. Much of the existing data was taken from FDOT construction plans and previous design information. Detailed calculations will be

required for each structure during the design phases of the project. All cross drains on S.R. 39 from I-4 to US 301 are addressed in this report. In determining the floodplain impacts, this report uses the typical sections shown in Figures 2 and 3.



FROM I-4 TO SHADY OAKS DRIVE

Based on 0.45m (1.5ft.) to 1.8m (6ft.) of Fill to Proposed PGL

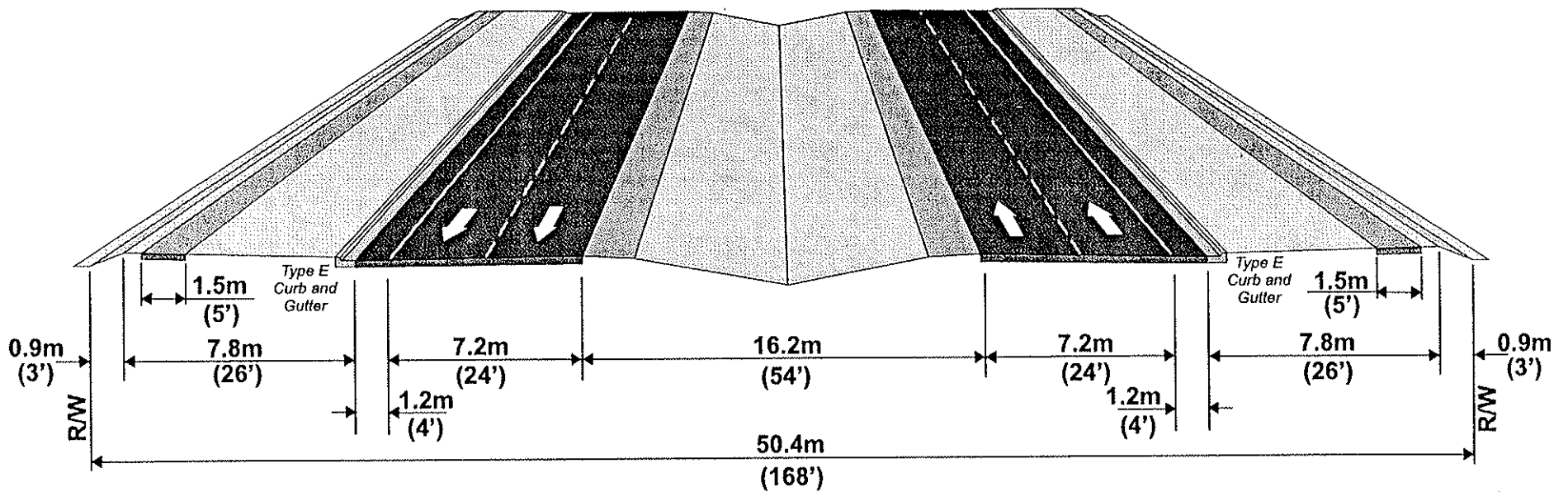
TYPICAL SECTION

S.R. 39 FROM I-4 TO U.S. 301
 WPI SEGMENT No. 255099 1 FAP No. F-321-1(4)
 HILLSBOROUGH AND PASCO COUNTIES, FLORIDA



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Figure 2



FROM SHADY OAKS DRIVE TO U.S. 301

Based on 0.45m (1.5ft.) of Fill to Proposed PGL



TYPICAL SECTION

S.R. 39 FROM I-4 TO U.S. 301
 WPI SEGMENT No. 255099 1 FAP No. F-321-1 (4)
 HILLSBOROUGH AND PASCO COUNTIES, FLORIDA

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Figure 3

SECTION 2.0

EXISTING DRAINAGE SYSTEM

Stormwater runoff for the project is currently conveyed through roadside ditches with outfalls to the following basins: Pemberton Creek, Holloman's Branch, East Canal, Itchepackesassa Creek, Two Hole Branch, Blackwater Creek, Big Ditch, Hillsborough River, and Zephyr Creek.

Historically, drainage flows that cross S.R. 39 in the project corridor are primarily from east to west, but in a few cases, the flows travel from west to east. In some fill sections, no ditches exist, and water simply flows from the road to natural ground. Presently, there are no formal or permitted stormwater management or treatment facilities for roadway runoff along the existing subject alignment.

The existing drainage structures along S.R. 39 were identified in the field in February 1999 and by examining existing roadway plans (see Appendix A for the Photograph Log). Twenty-one crossings were located, including 18 culverts, 1 bridge culvert, and 2 bridges, along the existing S.R. 39 alignment between Joe McIntosh Road and U.S. 301. Of the cross drains, nine are concrete box culverts that were originally constructed in 1915. Some existing structures have been extended from earlier widening(s) of S.R. 39. One of the box culverts has been extended with RCPs. Table 2 gives pertinent information about the existing cross drains. The first bridge, proceeding up-station, traverses Blackwater Creek in Hillsborough County and is a 49 m (161 ft) long composite steel bridge with a triple 13.71 m (45 ft) long semi-circular arch flood relief structure. A triple 3.05 x 1.22 m (10- x 4-ft) CBC bridge culvert, crossing Big Ditch (also known as Heron Branch) is located in Hillsborough County. The second bridge is a 96.01 m (315 ft) steel girder bridge supported by timber piles crossing the Hillsborough River in Pasco County. The Hillsborough River is classified as an Outstanding Florida Water (OFW) and immediately downstream of S.R. 39 is a FEMA designated floodway.

All structures are in good condition and are functioning properly with only silt removal of some of the culverts required for optimum performance. No traffic interruption is caused due to local flooding of the existing cross drains. FDOT maintenance staff members have reported that most of

TABLE 2

**EXISTING CROSS DRAIN INFORMATION
S.R. 39 Location Hydraulics Report**

Structure I.D.	Quantity	Type	Size CBC: m x m (ft x ft) RCP: mm (in) Bridge (Overall Length): m (ft)	Existing Length m (ft)	Milepost km (miles)	Drainage Area hectares (acres)	Outfall Basin
D-5	2	CBC	1.83 x 1.22 (6 x 4)	25.9 (85)	8.087 (5.026)	362.88 (896)	East Canal
D-6	1	CBC	2.13 x 0.91 (7 x 3)	25.9 (85)	10.560 (6.559)	99.23 (245)	Blackwater Creek
D-7	1	CBC	1.22 x 1.22 (4 x 4)	25.9 (85)	12.727 (7.905)	74.12 (183)	Blackwater Creek
D-8	1	CBC with 750 mm (30 in) Extension	0.61 x 0.61 (2 x 2)	25.0 (82)	13.862 (8.610)	3.24 (8)	Blackwater Creek
B-1 (Bridges at Backwater Creek)	2 (6 span and 3 span)	Composite steel bridge and triple semi-circular arch relief structure	49 (161) [main channel bridge] 13.71 (45) [relief structure]	7.4 (24.2) (curb-to-curb dimensions)	13.967 - 14.068 (8.675-8.738)	28,512.00 (70,400)	Blackwater Creek
D-9	1	CBC	1.22 x 0.91 (4 x 3)	22.9 (75)	14.786 (9.184)	29.16 (72)	Blackwater Creek
D-10	1	CBC	1.22 x 0.91 (4 x 3)	22.9 (75)	15.351 (9.535)	38.48 (95)	Blackwater Creek
D-11	2	CBC	2.44 x 0.91 (8 x 3)	22.9 (75)	15.614 (9.698)	87.08 (215)	Blackwater Creek
D-12	Does not exist						
B-2 (Bridge culvert at Big Ditch (Heron Branch))	3	Triple CBC bridge culvert	Triple 3.05 x 1.22 (10 x 4)	22.9 (75)	16.364 (10.164)	925.43 (2,285)	Big Ditch
D-13	1	CBC	0.91 x 0.91 (3 x 3)	24.3 (80)	16.659 (10.347)	3.65 (9)	Big Ditch (Heron Branch)
D-14	1	CBC	0.91 x 0.91 (3 x 3)	24.3 (80)	17.341 (10.771)	36.45 (90)	Big Ditch (Heron Branch)
D-15	2	RCP	750 (30)	25.9 (85)	0.138 (0.086)	20.25 (50)	Hillsborough River
D-16	1	RCP	750 (30)	25.6 (84)	0.068 (0.042)	2.43 (6)	Hillsborough River
D-17	2	RCP	900 (36)	23.5 (77)	1.594 (0.990)	2.84 (7)	Hillsborough River
D-18	1	RCP	450 (18)	22.9 (75)	1.835 (1.140)	8.10 (20)	Hillsborough River

2-2

TABLE 2 (Continued)

EXISTING CROSS DRAIN INFORMATION
S.R. 39 Location Hydraulics Report

Structure I.D.	Quantity	Type	Size CBC: m x m (ft x ft) RCP: mm (in) Bridge (Overall Length): m (ft)	Existing Length m (ft)	Milepost km (miles)	Drainage Area hectares (acres)	Outfall Basin
D-19	2	RCP	900 (36)	22.3 (73)	2.095 (1.301)	8.10 (20)	Hillsborough River
B-3 (Bridge at Hillsborough River)	(21 spans)	Steel girder bridge at Hillsborough River	96.0 (315)	7.9 (26) (roadway dimensions)	2.552-2.648 (1.585-1.645)	56,505.60 (139,520)	Hillsborough River
D-20	1	RCP	750 (30)	25.9 (85)	3.204 (1.990)	7.29 (18)	Hillsborough River
D-21	3	RCP	900 (36)	25.6 (84)	3.795 (2.357)	Not applicable (equalizer)	Zephyr Creek
D-22	1	RCP	900 (36)	25.6 (84)	4.832 (3.001)	20.25 (50)	Zephyr Creek
D-23	1	RCP	600 (24)	22.3 (73)	5.257 (3.265)	8.10 (20)	Zephyr Creek

2-3

the existing drainage system functions properly and adequately. The latest Bridge Inspection Report (BIR) for the bridge culvert at Heron Branch and the Hillsborough River Bridge are provided in Appendix B.

The BIR for the bridge culvert at Heron Branch states the sufficiency rating of the structure is 94.6, status 0, and the bridge culvert is generally in good condition with some siltation occurring. There are no guard rails existing at this structure, and the BIR recommends they be installed.

The BIR for the Hillsborough River Bridge states the sufficiency rating of the structure is 78 and has a status of 1. The bridge was constructed in 1947, and generally, the bridge is in good condition according to the BIR. All of the piles have small cracks appearing, and three of the piles exhibit rotting at their bases. One pile has more severe rotting occurring than the others. The recommended repair for this pile is to determine the depth of rot below grade and install a structural pile jacket.

2.1 EXISTING CROSS DRAINS

Personnel from the FDOT maintenance units were contacted concerning flooding occurrences at the existing cross drains (see Appendix E). The Tampa maintenance unit, which maintains the portion of S.R. 39 in Hillsborough County, identified two of the existing cross drains within the project limits having flooding problems, structures D-5 and D-7 (see maps in Appendix D). The reported flooding problems at the two cross drains do not appear to be due to insufficient culvert capacity but to inadequate outfall situations. The flooding problems at D-5 and D-7 appear to be caused by the downstream cross drains at the CSX railroad. The railroad cross drains were constructed with their inverts higher than those of the adjacent cross drains D-5 and D-7, or the highway culverts were constructed with their inverts lower than the invert of the railroad cross drains. Therefore, the flooding problems at D-5 and D-7 are not due to recent construction activities.

D-5 was deemed the, "worst case," or critical existing cross drain because it has the largest drainage area flowing to it. The existing D-5 cross drain is a double 1.83 m x 0.91 m (6 ft x 3 ft) CBC with a length of 25.9 m (85 feet). Extending D-5's length to 59.7 m (196 feet) will not cause the headwater for the 50-year storm to rise more than 0.03 in (0.1 ft). Therefore extending D-5 will not affect the 50-year floodplain significantly. See Appendix C for the D-5 culvert capacity analysis.

The Dade City maintenance unit was contacted concerning flooding problems occurring along the portion of S.R. 39 in Pasco County. Some flooding problems have occurred at existing side drains near Chancey Road, (C.R. 535) but the flooding does not appear to have been extensive during recent storm events. Larry Boone of this maintenance unit stated that some of side drains near the Crystal Springs Post Office appear to have been installed too high.

SECTION 3.0

PROPOSED DRAINAGE SYSTEM

The proposed drainage system for this project would be designed to carry stormwater runoff away from the roadway in the natural flow directions of that particular basin. In most cases, this would require modifications to existing structures, such as culvert extensions, to correspond to the new roadway sections and clear zone requirements. The existing structures could be extended without significant impacts to headwater elevations or negative effects to emergency services and evacuation. FDOT criteria requires that the proposed headwater at modified structures should not rise more than 0.03 m (0.1 ft) for the 50-year design storm event.

Stormwater management ponds will be required for this project, and potential pond sites will be evaluated and provided in the Pond Siting Report.

3.1 PROPOSED CROSS DRAINS

Five cross drains are proposed for the Alexander Street Bypass. Proceeding up-station from the proposed I-4 interchange, the first proposed cross drain AB-1 (AB, acronym for Alexander Bypass) would occur at Mill Creek, a tributary of Pemberton Creek, at approximately Station 26 + 20. This tributary drains most of the I-4/S.R. 39 (existing) interchange in a westerly direction. Mill Creek crosses below Franklin Street through double 165-mm (42-inch) RCPs, which are approximately 427 m (1,400 ft) upstream of the proposed AB-1 cross drain.

The next cross drain proposed up-station, AB-2, would occur at a second branch of Pemberton Creek. This tributary is not a well-defined channel but more like a broad floodplain crossing. This tributary flows in a southwesterly direction and drains much of the area southwest of the intersection of the existing S.R. 39 and Sam Allen Road. Proposed cross drain AB-2 would be constructed at approximately Station 34 + 20.

A third cross drain, AB-3, would be constructed at approximately Station 48 + 50. It would drain a small area west of the proposed Alexander Street Bypass to the east, similar to the natural drainage pattern.

A fourth proposed cross drain, AB-4, would be located at approximately Station 55 + 50 north of the proposed Alexander Street Bypass and I-4 intersection. An existing ditch occurs at this location and drains a large area from McGee Road up to Joe McIntosh Road west of S.R. 39 and a drainage area east of S.R. 39 and the CSX Railroad line. The portion the drainage area east of S.R. 39 and the CSX Railroad drains to the existing ditch via the existing S.R. 39 cross drain, D-4.

A fifth proposed cross drain, AB-5, would be located at station 59 + 50. It would drain a 7-acre area between the proposed Alexander Street Bypass and the existing S.R. 39 north of Joe McIntosh Road.

Table 3 shows the proposed cross drains, and the calculations are contained in Appendix C.

SECTION 4.0

FLOOD ZONE DESCRIPTIONS

The Federal Emergency Management Agency (FEMA) has developed Flood Insurance Rate Maps (FIRMs) for the unincorporated areas of Hillsborough, Pasco counties and Plant City in the vicinity of the project. Information from the FEMA FIRMs was transferred to USGS Quadrangle maps to show the floodplain limits on the maps provided in Appendix D. Base floodplain, or 100-year floodplain, impacts will occur at a total of 10 locations and all will be transverse in nature. FEMA FIRMs relevant for this project are listed in Section 10.0.

Of the cross drains proposed for the Alexander Street Bypass, two would transversely encroach onto 100-year floodplains. These proposed transverse floodplain crossings would occur at structures AB-1 (station 26 + 20) and AB-2 (station 34 + 20) over tributaries of Pemberton Creek. The proposed alignment will also encroach onto a 100-year floodplain at proposed structure AB-4 (station 55 + 50). There is an existing ditch at this location. The construction of AB-4 will be a transverse crossing and, therefore, it will be a transverse floodplain encroachment.

The proposed improvements to S.R. 39 along the existing alignment would transversely cross FEMA-designated 100-year floodplains at the following existing cross drains:

- D-6 (station 108 + 25),
- D-8 (station 142 + 00),
- B-1 (station 143 + 00),
- B-2 (station 166 + 00),
- D-14 (station 176 + 00), and
- B-3 (station 204 + 50).

The 100-year floodplain is adjacent to the existing alignment south of existing cross drain D-6 (station 104 + 30), near Bruton Road, and the proposed widening would minimally impact the floodplain at that location. The floodplain encroachment at station 104 + 30 is unavoidable in this

area because the existing alignment is adjacent to the floodplain and widening of S.R. 39 will encroach into it. Realignment of S.R. 39 would create greater floodplain encroachment. The realignment of S.R. 39 at the north terminus will create a transverse floodplain impact near U.S. 301 at station 231 + 00.

All floodplain impacts will require 1:1 volume compensation via excavation in the corresponding floodplain.

SECTION 5.0
SOIL CONDITIONS

The National Resource Conservation Service (NRCS, formerly Soil Conservation Service or SCS) soil survey for Hillsborough County shows 19 soil types within the existing and proposed alignments for S.R. 39, which are summarized in Table 4. Almost all of the soils in this section of the project have shallow depths to the Seasonal High Water Table (SHWT). The depths to the SHWT for this project range from 0.61 m (2.0 ft) above grade to greater than 1.83 m (6.0 ft) below grade.

TABLE 4
HILLSBOROUGH COUNTY SOILS
S.R. 39 Location Hydraulics Report

NRCS (SCS) Soil Type	NRCS (SCS) Map Symbol	Hydrologic Soil Group	Depth to Seasonal High Water Table [m (ft)]
Basinger	5	D	+0.61 - 0.30 (+2.0 - 1.0)
Candler	7	A	>1.83 (> 6.0)
Chobee	10 / 12	B/D	0.30 (1)
Eaton	13	D	0.30 (1)
Felda	15	B/D	0 - 0.30 (0.0 - 1.0)
Floridana	17	B/D	0 - 0.30 (0.0 - 1.0)
Ft. Meade	18	A	>1.83 (> 6.0)
Gainesville	19	A	>1.83 (> 6.0)
Lake	25	A	1.83 (> 6.0)

TABLE 4 (CONTINUED)

HILLSBOROUGH COUNTY SOILS
S.R. 39 Location Hydraulics Report

NRCS (SCS) Soil Type	NRCS (SCS) Map Symbol	Hydrologic Soil Group	Depth to Seasonal High Water Table [m (ft)]
Malabar	27	B/D	0 - 0.30 (0.0 - 1.0)
Myakka	29	B/D	0 - 0.30 (0.0 - 1.0)
Orlando	35	A	>1.83 (> 6.0)
St. Johns	46	B/D	0 - 0.30 (0.0 - 1.0)
Seffner	47	C	0.46 - 1.07 (1.5 - 3.5)
Smyrna	52	B/D	0 - 0.30 (0.0 - 1.0)
Tavares	53	A	1.07 - 1.83 (3.5 - 6.0)
Wabasso	57	B/D	0 - 0.30 (0.0 - 1.0)
Winder	59	B/D	0 - 0.30 (0.0 - 1.0)
Zolfo	61	C	0.61 - 1.07 (2.0 - 3.5)

The SCS soil survey for Pasco County shows 10 different soil types within the existing and proposed alignments for S.R. 39 and are summarized in Table 5. Almost all of the soils in this section of the project, like the section in Hillsborough County, have shallow depths to the SHWT. The depths to the SHWT for this project range from at grade to 1.83 m (6.0 ft) below grade.

TABLE 5
PASCO COUNTY SOILS
S.R. 39 Location Hydraulics Report

NRCS (SCS) Soil Type	NRCS (SCS) Map Symbol	Hydrologic Soil Group	Depth to Seasonal High Water Table [in (ft)]
Wauchula	1	B/D	0 - 0.30 (0.0 - 1.0)
Pomona	2	B/D	0 - 0.30 (0.0 - 1.0)
Tavares	6	A	1.07 - 1.83 (3.5 - 6.0)
Sparr	7	C	0.46 - 1.07 (1.5 - 3.5)
Vero	10	B/D	0 - 0.30 (0.0 - 1.0)
Zephyr	16	D	0.30 (1.0)
Electra Variant	18	C	0.61 - 1.07 (2.0 - 3.5)
Smyrna	21	A/D	0 - 0.30 (0.0 - 1.0)
Chobee	39	B/D	0 - 0.30 (0.0 - 1.0)
Lochloosa	48	C	0.76 - 1.52 (2.5 - 5.0)

SECTION 6.0
HYDROLOGY AND HYDRAULICS

As proposed, this project will widen the existing roadway from two to four lanes, with an ultimate six-lane section. This will require that existing cross drains be extended or replaced with a hydraulically equivalent culvert size. Table 6 summarizes the results of the backwater analyses for the worst-case existing cross drain, D-5, the proposed culverts for the Alexander Street Bypass, and the Hillsborough River Bridge.

TABLE 6
CROSS DRAIN BACKWATER ANALYSIS RESULTS
S.R. 39 Location Hydraulics Report

Cross Drain Number	50-Year Existing Headwater Elevation (m [ft] NGVD)	50-Year Proposed Headwater Elevation (m [ft] NGVD)	100-Year Existing Headwater Elevation (m [ft] NGVD)	100-Year Proposed Headwater Elevation (m [ft] NGVD)
D-5	31.46 (103.2)	31.49 (103.3)	31.65 (103.8)	31.70 (104.0)
AB-1	32.61 (107.1)	32.63 (107.1)	32.74 (107.4)	32.78 (107.5)
AB-2	32.89 (107.9)	32.92 (108.0)	32.92 (108.0)	32.97 (108.1)
AB-3	30.63 (100.5)	30.66 (100.6)	30.63 (100.5)	30.66 (100.6)
AB-4	31.39 (103.0)	31.42 (103.1)	31.39 (103.0)	31.43 (103.1)
AB-5	32.00 (105.0)	32.02 (105.0)	32.00 (105.0)	32.02 (105.1)
B-3 (Hillsborough River)	19.72 (64.7)	19.72 (64.7)	19.93 (65.4)	19.93 (65.4)

The sizes of the proposed culverts, AB-1 through AB-5, which produced the headwaters elevations in the above table are preliminary and may be changed in the final design stage of this project.

SECTION 7.0

STRUCTURE CATEGORIZATION

As set forth in the FDOT PD&E Guidelines, the proposed hydraulic improvements should be categorized based on type of improvement and the approximate floodplain impact. The existing culverts and bridges were evaluated and identified as either Categories 3 or 4 structures.

Category 3: Project Involving Modifications to Existing Drainage Structures.

This applies to structures D5 through D23 and B2. These drainage structures are in fairly good condition throughout the project. Silting is occurring in some areas, but no structure appeared to need replacement because of deterioration. The existing cross drains would be extended to accommodate the proposed additional two lanes including the 11 m (36 ft) clear zone. Using HY-8 software based on techniques provided in FHWA Hydraulic Design Series #5 for the hydraulic calculations, the change in the headwater for a 50-year storm was less than 0.030 m (0.1 ft), which is below the allowable high water. As a result of this computation, the following general statement can be made:

“The modifications to drainage structures included in this portion of the project will result in an insignificant change in their capacity to carry floodwater. This change will cause minimal increases to flood heights and flood limits. These minimal increases will not result in any significant adverse impacts on the natural and beneficial floodplain values or any significant change in the potential for interruption or termination of emergency service or emergency evacuation routes. Therefore, it has been determined that this encroachment is not significant.”

Category 4: Projects on Existing Alignment Involving Replacement of Existing Drainage Structures with No Record of Drainage Problems.

The two bridges included in this project were classified as Category 4. The proposed structures should not reduce the hydraulic performance of existing facilities. Also, there is no record of drainage problems and no unresolved drainage complaints from residents in these areas.

7.1 B1- BLACKWATER CREEK

Blackwater Creek downstream of S.R. 39 is a floodplain. Upstream of the bridge is a broad floodplain that is extremely sensitive to changes in backwater elevations. To maintain historical elevations in both directions replacement/rehabilitated structures are currently (October 1999) being designed to perform hydraulically equivalent to the existing structures. The existing S.R. 39 contains two narrow bridges in the Blackwater Creek area. The bridge over Blackwater Creek (Bridge #10036) will be lengthened from 49.33 m (161.8 ft.) to 63 m (206.7 ft.) with a replacement structure to improve hydraulic flow conditions. The Blackwater Creek Relief Structure (Bridge #100037) will be reconstructed/rehabilitated and maintain its current length of 21.4 m (70.2 ft.). Details regarding these structures are contained in the Bridge Development Reports dated May 21, 1999 and August 1999.

7.2 B3 - HILLSBOROUGH RIVER

The Hillsborough River, like Blackwater Creek, is FEMA-regulated from S.R. 39 downstream. Upstream, the bridge design must meet Pasco County criteria requiring no increase in head loss above existing conditions.

It is proposed to replace the existing bridge, in kind, with a parallel bridge of the same length constructed for the two new lanes. Preliminary WSPRO analyses show that the water surface elevations will not vary upstream or downstream from the existing conditions for dual 320-ft bridges. This will also meet the Pasco County requirement of no increase in head loss for new structures.

As a result of the WSPRO analysis, the following general statement can be made for Bridge B3:

“The proposed structure will perform hydraulically in a manner equal to or greater than the existing structure, and backwater surface elevations are not expected to increase. As a result, there will be no significant adverse impacts on natural and beneficial floodplain values, there will be no significant change in flood risks, and there will be no significant change in the

potential for interruption or termination of emergency service or emergency evacuation routes. Therefore, it has been determined that this encroachment is not significant.”

7.3 PROPOSED STRUCTURES

The five proposed cross drains for the Alexander Street Bypass are classified as either Category 1 or 6.

Category 1: Projects which will not involve any work below the 100-year flood elevation.

The 100-year floodplain areas were determined from applicable FEMA FIRM maps. The proposed structures along the Alexander Street Bypass which will be classified as Category 1 are AB-3 and AB-5 the following statement can be made:

Although this involves work within the horizontal limits of the 100-year floodplain, no work is being performed below the 100-year flood elevation and, as a result, this project does not encroach upon the base floodplain.”

Category 6: Projects on new alignment, and projects on existing alignment with potentially significant changes in 100-year flood elevations.

The proposed Alexander Street Bypass drainage structures which will be classified as Category 6 are AB-1, AB-2, and AB-4 and the following statement can be made:

“The construction of the drainage structure(s) proposed for this project will cause changes in flood stage and flood limits. These changes will not result in any significant adverse impacts on the natural and beneficial floodplain values or any significant changes in flood risk or damage. These changes have been reviewed by the appropriate regulatory authorities who have concurred with the determination that there will be no significant impacts. There will not be significant change in the potential for interruption or termination of emergency service or emergency evacuation routes. Therefore, it has been determined that this encroachment is not significant.”

SECTION 8.0
REGULATORY AUTHORITIES

8.1 LOCAL AGENCIES

Local government agencies with jurisdictions overlapping the project area include the cities of Zephyrhills and Plant City and Pasco County and Hillsborough County.

8.2 STATE AGENCIES

The state agencies involved in the permitting process for the S.R. 39 drainage systems would be the Florida Department of Environmental Protection (FDEP) and the Southwest Florida Water Management District (SWFWMD). Permits would be required for all dredge and fill work within, or areas connected to, Waters of the State (Chapter 17-4.23, FAR), and FDEP has delegated most dredge and fill permitting to SWFWMD.

Stormwater systems would be permitted through SWFWMD pursuant to Chapter 40D-4 FAC. The systems must provide storage for stormwater quantity and quality. The corridor lies adjacent to numerous wetlands areas that must be considered in the design of the stormwater systems. The Hillsborough River is an Outstanding Florida Water (OFW). Projects discharging directly to OFWs shall be required to provide treatment for a volume 50 percent more than required for the selected treatment system. This criteria also applies to existing treatment capacity being displaced by roadway projects.

One-to-one volume compensation would have to be made for storage volume lost due to roadway embankment in the 100-year floodplain.

8.3 FEDERAL AGENCIES

The U.S. Army Corp of Engineers (USACE) would be involved in permitting dredge and fill activities in Pasco and Hillsborough counties. The USACE issues permits for dredge and fill activities in the Waters of the United States.

A National Pollutant Discharge Elimination System (NPDES) permit is administered by the U.S. Environmental Protection Agency (EPA) for stormwater discharges into waters of the United States.

SECTION 9.0
CONCLUSION

The proposed drainage improvements consisting of extending existing culverts and adding or replacing existing bridges to accommodate improvements within the S.R. 39 study corridor should not adversely affect the surrounding area. The existing flood zones fit the surrounding flat lowland terrain and should not change because of the widening. The area surrounding the corridor is urban and rural in nature with numerous wetlands. This improvement to existing facilities should have minimal effect on development in flood zones. The improvement of the roadway should help emergency services. The widening of S.R. 39 adjacent to the existing alignment is the most viable solution because of the numerous wetland areas and the railroad to the east.

At the south end of the corridor, new drainage structures for the Alexander Bypass would have minor impacts, but such impacts are limited to 0.03 m (0.1 ft) of backwater in a 50-year event.

SECTION 10.0

REFERENCES

1. USGS Quad Maps, Plant City West, Fla, 1975 Zephyrhills, Fla. 1975.

2. The following SWFWMD Aerials

Sections 5, 6, 8, 17, 20; Township 28 E; Range 22S

Sections 6, 7, 18, 19, 30, 31; Township 27E; Range 22S

Section 1 Township 27E; Range 21S

Sections 14, 23, 24, 25, 36; Township 26E; Range 21S

3. FEMA Flood Insurance Rate Maps

Panel No.	Community	Effective Date
120113 0005B	Plant City	April 29, 1983
120112 0270D	Hillsborough County	August 3, 1992
120112 0260C	Hillsborough County	April 17, 1984
120112 0120C	Hillsborough County	April 17, 1984
120230 0470B	Pasco County	November 11, 1981
120230 0460D	Pasco County	September 30, 1992

4. FIS Hillsborough County, August 3, 1992.
FIS Pasco County, May 18, 1981.

5. NRCS Soils Surveys for Hillsborough County (1989) and Pasco County (June 1982).

6. Design Documentation for I-4 Drainage, (Volumes 1 through 4). Improvements (Segment 4) State Project Number :10190-431, Work Program Number: 7143200, Federal Aid and Project Number: DPI-0043-(1). Proposed for FDOT by Parsons Brinkerhoff, Revised March 1996.

7. City of Plant City, Florida, Westside Canal Stormwater Management Plan, May 1997, by Camp Dresser and McKee.

8. Floodplain Information on the Blackwater Creek Watershed, Blackwater Creek, East Canal and Itchepackesassa. Prepared by the staff of the Southwest Florida Water Management District, Brooksville, Florida, August 1980.
9. Floodplain Information on the Hillsborough River Watershed, Hillsborough River and New River. Prepared by the staff of the Southwest Florida Water Management District, Brooksville, Florida, August 1980.
10. Project Development Environmental Studies, Location Hydraulic Report For State Road 39, Hillsborough and Pasco Counties, WPINo.: 7113335 & 7115925, State Project No.: 10200-1508 and 14110-1503, 1993.
11. Draft Bridge Hydraulic Analysis, SR 39 Over Blackwater Creek, Hillsborough County, Florida," FPID No.: 257163-1-5201, State Project No.: 10200-1515, Work Program No.: 7113773, 1999.

APPENDIX A
PHOTOGRAPH LOG



VIEW OF D-1 LOOKING WEST



VIEW OF D-2 LOOKING WEST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-3 LOOKING NORTH

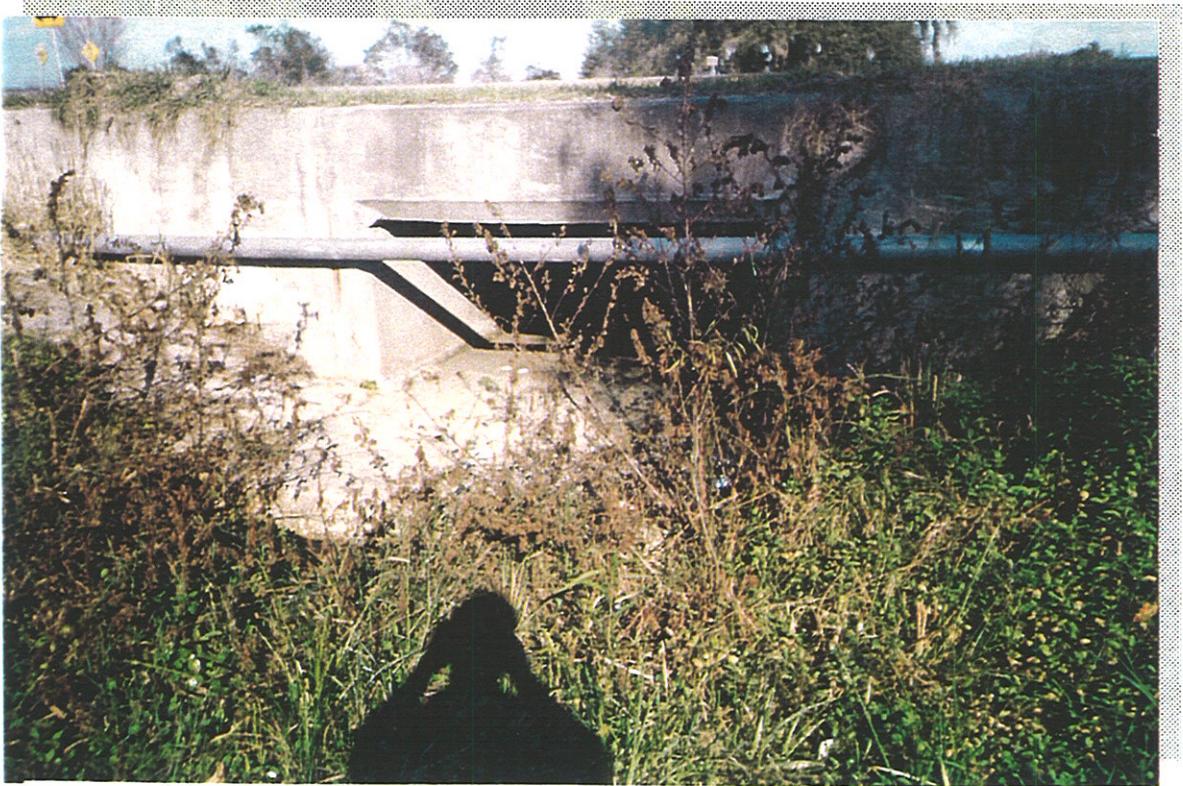


VIEW OF D-4 LOOKING WEST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-5 LOOKING EAST



VIEW OF D-6 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-7 LOOKING EAST



VIEW OF D-8 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-9 LOOKING WEST



VIEW OF D-10 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-11 LOOKING WEST



VIEW OF D-13 LOOKING WEST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-14 LOOKING WEST



VIEW OF D-15 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-16 LOOKING WEST



VIEW OF D-17 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-18 LOOKING EAST



VIEW OF D-19 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF D-20 LOOKING EAST



VIEW OF D-21 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES

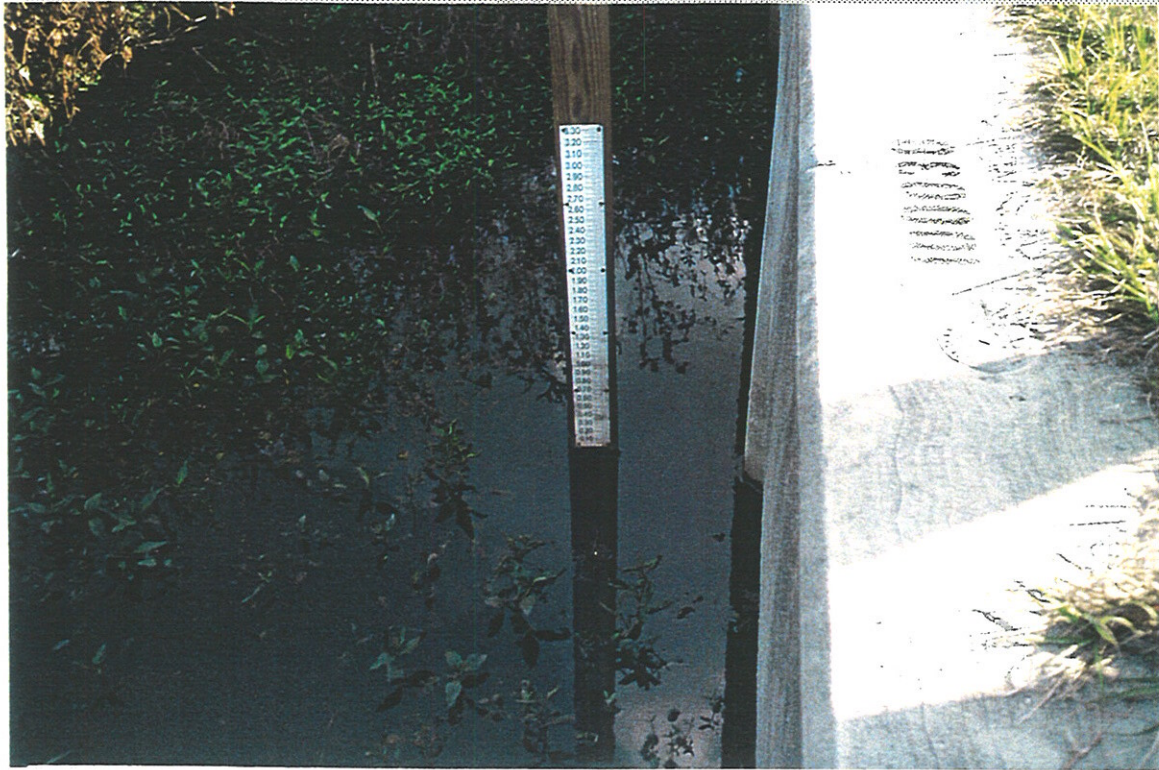


VIEW OF D-22 LOOKING WEST



VIEW OF D-23 LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF STAFF GAUGE AT BIG DITCH (B-2)



VIEW OF BIG DITCH (B-2) LOOKING WEST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES



VIEW OF THE HILLSBOROUGH RIVER (B-3)



VIEW OF THE HILLSBOROUGH RIVER (B-3) LOOKING EAST

S.R. 39 FROM I-4 TO U.S. 301
WORK PROGRAM ITEM SEGMENT NO. 225099 1
HILLSBOROUGH AND PASCO COUNTIES

APPENDIX B

BRIDGE INSPECTION REPORTS

**EXISTING BRIDGE CULVERT
OVER BIG DITCH (HERON BRANCH)**



BRIDGE INSPECTION REPORT
Prepared by
KISINGER, CAMPO, & ASSOCIATES

CONTENTS OF REPORT

- | | |
|--|------------------------------------|
| A. Condensed Inspection Report | * F. Field Preparation |
| B. Comprehensive Report of Deficiencies | * G. Fracture Critical Inspections |
| C. Evaluation of Previous Corrective Action | * H. Scour Evaluation |
| D. Required Maintenance Repair and Rehabilitation | I. Load Rating Analysis |
| * E. Methods, Quantities and Costs of Contract Corrective Action | J. BMIS Report |
- * This section is not included in this report.

REPORT IDENTIFICATION

Bridge No.: 100038 Bridge Name: SR 39 over Heron Branch
 Location: 1.2km South of Pasco County Line Section No. 10200
 NO YES US R. N/A
 This bridge contains fracture critical components? S.R. 39
 This bridge is scour critical? M.P. 10.164
 This report identifies deficiencies which require prompt corrective action? RD. SYS. 901

Type of inspection: Routine Interim Special _____
 Field Inspection Date: Above Water 01/06/98 Under Water: <1m

Name of Inspector/Diver	Initials	Engineering Registration Number	Certified Bridge Inspection No.
M.H. Betz, CBI (Senior Inspector In Charge)	<i>MHB</i>		00162
R.D. Uptegraff			
(Senior Diving Inspector/Diver)			

Reviewing Bridge Inspection Supervisor

Name: K.C. Reinhold, CBI 00025 Initials: KR
 PE or CBI Number: _____

Confirming Registered Professional Engineer

Name: P.G. Foley, PE P.E. Number: 40978

Signature *P.G. Foley* 2/4/98

(Handwritten initials)

* - Deficiencies exist in this element that warrant written and/or sketched descriptions that are provided in section B of this report.
 ** - NCR is an abbreviation for Numerical Condition Rating, the definitions of which can be found on the back of this pag

APPROACH ROADWAY		CHANNEL		NON-STRUCTURAL	
MAJOR FEATURE	CHANNL-MAJOR FEATURE	NON-STRUCTURAL FEATURES	BMS NO.	ELEMENT TITLE	NCR
64.00	Approach Roadway	Channel and Channel Protection Overall Rating	7	Lighting Systems	N
64.02	Retaining Walls/Approach Slopes/Embankments/Shoulder	Embankments/Slopes	7	Signs	N
64.03	Roadway-Bridge Transition	Degradation/Aggregation	*7	Striping (Roadway Reflective)	4
64.04	Guardrails	Alignment	8	Reflectors	4
64.05	Roadway Alignment	Flow	*6	Utility Attachments	N
65.00	Channel and Channel Protection Overall Rating	Channel and Channel Protection Overall Rating	7	Lighting Systems	N
65.01	Channel and Channel Protection Overall Rating	Channel and Channel Protection Overall Rating	7	Lighting Systems	N
65.02	Embankments/Slopes	Embankments/Slopes	7	Signs	N
65.03	Embankments/Slopes	Embankments/Slopes	7	Signs	N
65.04	Degradation/Aggregation	Degradation/Aggregation	*7	Striping (Roadway Reflective)	4
65.05	Alignment	Alignment	8	Reflectors	4
65.06	Flow	Flow	*6	Utility Attachments	N
66.01	Lighting Systems	Lighting Systems	7	Lighting Systems	N
66.02	Signs	Signs	7	Signs	N
66.03	Striping (Roadway Reflective)	Striping (Roadway Reflective)	*7	Striping (Roadway Reflective)	4
66.04	Reflectors	Reflectors	8	Reflectors	4
66.05	Utility Attachments	Utility Attachments	*6	Utility Attachments	N
66.08	Traffic Control and Monitoring Systems	Traffic Control and Monitoring Systems	66.08	Traffic Control and Monitoring Systems	N
66.09	Deck Cleanmess	Deck Cleanmess	66.09	Deck Cleanmess	N
66.12	Fences and Glare Screens	Fences and Glare Screens	66.12	Fences and Glare Screens	N

NUMERICAL CONDITION RATING DEFINITIONS FOR CHANNEL	
CODE DESCRIPTION	NUMERICAL CONDITION RATING DEFINITIONS FOR NON-STRUCTURE FEATURES
N	NOT APPLICABLE - Use when culvert is not over waterway.
9	EXCELLENT CONDITION - No noticeable or noteworthy deficiencies which effect the condition of the channel.
8	VERY GOOD CONDITION - Banks are protected or well vegetated. River control devices, such as spur dikes and embankment protection are not required or are in stable condition. Some minor scour has occurred near culvert.
7	GOOD CONDITION - Bank protection is in need of minor repairs. Waterway control devices and embankment protection have minor damage. Banks and/or channel have minor amounts of drift. Minor local scour developing near culvert.
6	SAISFACTORY CONDITION - Bank is beginning to slump. Waterway control devices and embankment protection have considerable minor damage. There is minor stream bed movement evident. Debris is restricting the waterway slightly. Scour holes deepening.
5	FAIR CONDITION - Bank protection is being eroded. Waterway control devices and/or embankment have major damage. Trees and brush restrict the channel. Scour holes are becoming more prominent, affecting the stability of the culvert.
4	POOR CONDITION - Bank and embankment protection undermined with corrective action required. Waterway control devices have severe damage. Large deposits of debris in the waterway. The stream bed has changed its location but is causing no problem.
3	SERIOUS CONDITION - Bank protection has failed completely. Scour holes forming in embankment. Waterway control devices have been destroyed. Stream bed aggragation or degradation has changed the waterway to now threaten the culvert and/or approach roadway.
2	CRITICAL CONDITION - Abutment has failed (portion has settled) due to undermining of footing. The waterway has changed and now threatens the culvert and/or embankment. Scour is of sufficient depth so that culvert is near state of collapse.
1	IMMINENT FAILURE CONDITION - Culvert closed corrective action may put structure back into light service.
0	FAILED CONDITION - Culvert closed. Replacement necessary.

NUMERICAL CONDITION RATING DEFINITIONS FOR CHANNEL	
CODE DESCRIPTION	NUMERICAL CONDITION RATING DEFINITIONS FOR NON-STRUCTURE FEATURES
N	NOT APPLICABLE - Use when culvert is not over waterway.
9	EXCELLENT CONDITION - No noticeable or noteworthy deficiencies which effect the condition of the channel.
8	VERY GOOD CONDITION - Banks are protected or well vegetated. River control devices, such as spur dikes and embankment protection are not required or are in stable condition. Some minor scour has occurred near culvert.
7	GOOD CONDITION - Bank protection is in need of minor repairs. Waterway control devices and embankment protection have minor damage. Banks and/or channel have minor amounts of drift. Minor local scour developing near culvert.
6	SAISFACTORY CONDITION - Bank is beginning to slump. Waterway control devices and embankment protection have considerable minor damage. There is minor stream bed movement evident. Debris is restricting the waterway slightly. Scour holes deepening.
5	FAIR CONDITION - Bank protection is being eroded. Waterway control devices and/or embankment have major damage. Trees and brush restrict the channel. Scour holes are becoming more prominent, affecting the stability of the culvert.
4	POOR CONDITION - Bank and embankment protection undermined with corrective action required. Waterway control devices have severe damage. Large deposits of debris in the waterway. The stream bed has changed its location but is causing no problem.
3	SERIOUS CONDITION - Bank protection has failed completely. Scour holes forming in embankment. Waterway control devices have been destroyed. Stream bed aggragation or degradation has changed the waterway to now threaten the culvert and/or approach roadway.
2	CRITICAL CONDITION - Abutment has failed (portion has settled) due to undermining of footing. The waterway has changed and now threatens the culvert and/or embankment. Scour is of sufficient depth so that culvert is near state of collapse.
1	IMMINENT FAILURE CONDITION - Culvert closed corrective action may put structure back into light service.
0	FAILED CONDITION - Culvert closed. Replacement necessary.

Bridge No.: 100038 Location: 1.2km South of Pasco County
 County Section No.: 10200 Inspection Date: 01/06/98
 State Road No.: 39 Inspector: M.H. Betz, CBI
 US Road No.: N/A Mile Post No.: 10.164

B. COMPREHENSIVE REPORT OF DEFICIENCIES

G4.04 GUARDRAILS

There are no guardrails present at this structure. The recovery zone from the northbound lane line is 8.6m, and from the southbound lane line 7.9m.

G5.04 DEGRADATION/AGGREGATION

The following are groundline measurements referenced to the top of the head wall. These measurements have been provided to compare and monitor scour or build up. All measurements were taken in meters.

	Left Side	Right Side
	07/97	07/97
Wall 1	1.5	1.5
Centerline	1.8	1.7
Wall 2	1.8	1.7
Centerline	1.7	1.6
Wall 3	1.8	1.7
Centerline	1.8	1.6
Wall 4	1.5	1.5
Waterline	1.1	1.2

No previous measurements have been taken to date.

G5.06 FLOW

An average of 1m of dirt has accumulated in the center of Barrel 1. Also, on the west side of the structure there is a moderate amount of vegetation growth.

G7.03 SIDE WALLS

There is Class 1 and Class 2 scaling, from the bottom up to less than 1m. Also, the side walls contain Class 1 and Class 2 vertical cracks in the old section of culvert.

G7.04 HEAD WALLS

Both head walls contain Class 1 vertical cracks, and there are Class 2 vertical cracks located at the northeast, southeast, and southwest corners of the structure.

NOTE: For G4.04, see page 5.
Crack Kelly 3/19/98

G5.06 FLOW

Activity: 805 MH Clean-Vegetation or Debris Removal
 Number of Units: 10
 Work Force: State

Repair Description: Remove the dirt from barrels, and clear vegetation from channel.

Evaluation: No corrective action was taken on above recommendation. Heavy rains have reduced the build-up in Barrels 2 and 3. Barrel 1 still contains dirt build-up.

G4.04 GUARDRAILS

Activity: 526 LF Guardrail Repair
 Number of Units: 500
 Work Force: State

Repair Description: Install guardrail on both sides of structure.

Evaluation: No corrective action was taken on the above recommendation.

C. Evaluation of Previous Corrective Action

Bridge No.:	100038	Location: 1.2km South of Pasco Coun
County Section No.:	10200	Inspection Date: 01/06/98
State Road No.:	39	Inspector: M.H. Betz, CBI
US Road No.:	N/A	Mile Post No.: 10.164

4/4

Bridge No.: 100038 Location: 1.2km South of Pasco County
 County Section No.: 10200 Inspection ^{Line} Date: 01/06/98
 State Road No.: 39 Inspector: M.H. Betz, CBI
 US Road No.: N/A Mile Post No.: 10.164

D. Required Maintenance Repair and Rehabilitation

STATE FORCES

TRAFFIC RESTRICTION: This structure currently requires no weight restriction posting as per the results of the most recent load rating analysis dated 09/09/91. Our inspection did not reveal significant deterioration to suggest the need for a new load rating analysis.

WORK ORDERS

G4.04 GUARDRAILS

Activity: 898 MH Miscellaneous Bridge M & R
 Number of Units: 40

Repair Description:
 Install guardrail on both sides of structure.

} FYI Item. E-Mail sent to the Local Maintenance Engineer on 3/19/98. *White Kelly*

98/11/28
 3/31/98

COMMENTS:

National Bridge Inventory Structure Inventory and Appraisal Report 100038

Last NBI Inspection 1/1/98

Sufficiency Rating	*	94.6
Status	0	

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<p>Identification</p> <p>State Name: Florida Region: Atlanta</p> <p>Bridge ID: 100038</p> <p>Inventory Route: (On/Under): On Route On Structure</p> <p>Kind Highway: 3 State Highway</p> <p>Level of Service: Mainline</p> <p>Route Number: 00039</p> <p>Directional Suffix: 1</p> <p>Highway Agency District: D7 - Tampa</p> <p>County Code: (10)Hillsborough Place Code: No city involved</p> <p>Features Intersected: HERON BRANCH</p> <p>Facility Name: SR 39</p> <p>Location: 1.2KM S/O PASCO CO LINE</p> <p>Kilometer Point: 10.164 km</p> <p>Onbasenet: 0</p> <p>-sivrt: 00102000 Subrt Num: 0</p> <p>Latitude: 280936</p> <p>Longitude: 820918</p> <p>Border Bridge State Code: -2 % Share: 0 %</p> <p>Border Bridge Structure No.:</p>	<p>Structure Type & Material</p> <p>Main NBI Unit</p> <p>Material Co</p> <p>Design Cul</p>
<p>Age and Service</p> <p>Year Built: 1941</p> <p>Year Reconstruction: 1987</p> <p>Type Service: On: 1</p> <p>Avg Daily Traffic: 6500</p> <p>Lanes: 2</p> <p>Detour Length: 18 km</p>	<p>Load Rating and Posting</p> <p>Design Load: M</p> <p>Operating Rating Method: 1</p> <p>Operating Rating: 99.9</p> <p>Inventory Rating Method: 1</p> <p>Inventory Rating: 72.5</p> <p>Bridge Posting: 5</p>
<p>Condition</p> <p>Deck: N</p> <p>Superstructure: N</p> <p>Substructure: N</p> <p>Channel and Channel Protection: 7</p> <p>Culverts: 7</p> <p>Structure Open, Posted, or Closed: A</p>	<p>Classification</p> <p>NBIS Bridge Length: Y</p> <p>Highway System: 3 State Highway</p> <p>Functional Class: 02 Rural Princ. Arterial - Other</p> <p>Defense Highway: 0</p> <p>Parallel Structure: N</p> <p>Directions of Traffic: 2</p> <p>Temporary Structure: 1</p> <p>Federal Lands Highways: 1</p> <p>Designated National Network: 0</p> <p>Toll: 3 On Free Road</p> <p>Maintenance Responsibility:</p> <p>1 State Highway Agency</p> <p>Owner: 1 State Highway Agency</p> <p>Historical Significance: 4</p> <p>Undeterminable Hist. Significance</p>

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Geometric Data

Length of Maximum Span: 3.3 m
 Structure Length: 9.9 m
 Curb or Sidewalk: Lt: 0 m Rt: 0 m
 Rdway Width Curb to Curb: 0 m
 Deck Width Out to Out: 0 m
 Appr Rdwy (w/Shoulders): 9.7 m
 Bridge Median: 0 # 0
 Skew: 0 Structure Flared: No flare
 Min Vert Clr/Inv Route: 99.99 m
 Invt Rte Total Horiz Clear: 23.8 m
 Min Vert Clear over Bridge Rdwy: 99.99 m
 Min Vert Underclear: Reference: ! 0 m
 Min Horiz Lat UndrClrs: Reference: ! Rt: 0 m Lt: 0 m

Appraisal

Structural Evaluation: 7
 Deck Geometry: !
 Underclrs, Vertical_Horizontal: N
 Waterway Adequacy: 7
 Approach Roadway Alignment: 9

Traffic Safety Features

Bridge Guardrails: !
 Transitions: !
 Approach Guardrails: !
 Approach Guardrail Ends: !
 Scour Critical Bridge: 8

Proposed Improvements

Type of Work -2 By: !
 Length of Structure Improvement: 0
 Bridge Improvement Cost \$Thousands: 0
 Roadway Improvement Cost \$Thousands: 0
 Total Project Cost \$Thousands: 0
 Improvement Cost Estimate (Yr.):
 Future ADT: 10185
 Year of Future ADT: 2018

Navigation Data

Navigation Control: 0
 Pier Protection: !
 Navigation Vertical Clearance: 0 m
 Vert-Lift Bridge Nav Min Vert Clear: 0 m
 Navigation Horizontal Clearance: 0 m

Past Inspections

Inspection Date: 01.01.1998 Type: 1
 Inspector: BID Pontis User Key: BID
 Inspection Notes:

Structural Units

Structural Unit: 0 MAIN SPAN 1 NBI Main Span NBI Approach Span
 Notes:

Bridge Notes

**EXISTING S.R. 39 BRIDGE
OVER THE HILLSBOROUGH RIVER**



BRIDGE INSPECTION REPORT

PREPARED BY DAVID VOLKERT & ASSOCIATES, INC.

CONTENTS OF REPORT

- | | |
|--|------------------------------------|
| A. Condensed Inspection Report | * F. Field Preparation |
| B. Comprehensive Report of Deficiencies | * G. Fracture Critical Inspections |
| C. Evaluation of Previous Corrective Action | * H. Scour Evaluation |
| D. Required Maintenance Repair and Rehabilitation | * I. Load Rating Analysis |
| * E. Methods, Quantities and Costs of Contract Corrective Action | J. BID Report |
- * This section is not included in this report.

REPORT IDENTIFICATION

Bridge No.: 140007 Bridge Name: SR-39 Over Hillsborough River

Location: 2 Miles south of US-301 Section No. 14110

NO	YES		
<input checked="" type="checkbox"/>	<input type="checkbox"/>	This bridge contains fracture critical components?	US R. <u>N/A</u>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	This bridge is scour critical?	S.R. <u>39</u>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	This report identifies deficiencies which require prompt corrective action?	M.P. <u>1.585</u>
			RD. SYS. <u>901</u>

Type of inspection: Routine Interim Special _____

Field Inspection Date: Above Water 02-19-97 Under Water: 02-27-97

Name of Inspector/Diver	Initials	Engineering Registration Number	Certified Bridge Inspection No.
K.S. King (Senior Inspector In Charge)	<i>KSK</i>		00265
R.C. Obi			
V.L. Griswold (Dive Tech) (Senior Diving Inspector/Diver)			00030
A. Bibelhauser (Dive Tech)			

Reviewing Bridge Inspection Supervisor

Name: D.B. Teal 42097 Initials: *DBT*

PE or CBI Number:

Confirming Registered Professional Engineer

Name: D.B. Teal P.E. Number: 42097

Signature

[Handwritten Signature]
5/27/97

Deficiencies exist in this element that warrant written and/or sketched descriptions that are provided in section 8 of this report.

** NCR is an abbreviation for Numerical Condition Rating, the definitions of which can be found on the back of this page.

DECK COMPONENT		SUPERSTRUCTURE COMPONENT		SUBSTRUCTURE COMPONENT	
BID NO.	ELEMENT TITLE	BID NO.	ELEMENT TITLE	BID NO.	ELEMENT TITLE
G1.00 (58)	Deck Overall Rating	G3.00 (60)	Substructure Overall Rating		
G1.01	Deck (Top)/Surfacing	G3.01	Piling/Shafts		
G1.02	Deck (Underside)	G3.02	Footings/Caissons		
G1.03	Expansion Joints	G3.03	Columns/Wall Piers		
G1.04	Construction Joints	G3.04	Intermediate Caps (Bent & Pier)		
G1.05	Drainage System	G3.05	Bracing/Struts/Web Walls		
G1.06	Curbs/Medians/Sidewalks	G3.06	Abutments/End Bents		
G1.07	Handrails/Barriers/Parapets	G3.07	Slope Protection/Slope		
G2.06	Lower Chords	G3.08	Upper Chords		
G2.07	Verticals	G3.09	Diagonals		
G2.10	Portals	G3.10	Fracture Critical Members		
CHANNEL- MAJOR FEATURE					
APPROACH ROADWAY		APPROACH ROADWAY			
BID NO.	ELEMENT TITLE	BID NO.	ELEMENT TITLE	NCR	
G4.00	Approach Roadway Overall Rating	G5.00 (61)	Channel and Channel Protection Overall Rating	7	
G4.01	Approach Slabs	G5.01	Fender System	7	
G4.02	Slopes/Embankments/Shoulder	G5.02	Navigation Lights and Aids	7	
G4.03	Roadway-Bridge Transition	G5.03	Embankments/Slopes/Fulkheads	N	
G4.04	Guardrails	G5.04	Degradation/Aggregation	7	
G4.05	Roadway Alignment	G5.05	Alignment	8	
		G5.06	Flow	8	
		G6.10	Superstructure Cleaness	4	
		G6.11	Substructure Cleaness	4	
		G6.12	Fences and Glare Screens	N	

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Bridge No.: 140007 Location: 2 Miles south of US-301
 County Section No.: 14110 Inspection Date: 02-19-97
 State Road No.: 39 Inspector: K.S. King
 US Road No.: N/A Mile Post No.: 1.585

B. COMPREHENSIVE REPORT OF DEFICIENCIES

G1.01 DECK (TOP)

The edges of the joints have class 1 to 2 spalls.

G3.01 PILING

All of the piles exhibit weathering splits up to 5mm (1/4") wide. Soft areas up to 5mm (1/4") deep are along the groundline. Pile 3-4 exhibits rot along the base up to 50mm (2") deep. Piles 17-3 and 20-4 have up to 5mm (1/4") deep rot around the piles at the groundline.

G3.07 SLOPE PROTECTION

There are 12 bags of riprap missing from the top of the slope under span 1.



Waterway Measurements

Inspection Date: 02-19-97

Bridge Number: 140007

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Distance from top of bridge/raill to water at time of inspection: 20.5
 DIST. Bent No. DIST. Bent No.
 LEFT RIGHT

Distance from top of bridge/raill to mudline

"-" Sign Denotes Degradation
 "+" Sign Denotes Aggregation

Bent No. Original Previous Present Difference

1	1.46	1.46	0	1.43	1.43	1.44	-0.01
2	3.29	3.35	0	3.14	3.14	3.14	0
3	5.06	5.06	0	4.79	4.69	4.69	0
4	5.06	5.03	-0.02	5.06	5.05	5.05	0.01
5	5.21	5.18	-0.02	5.36	5.35	5.35	0.01
6	5.36	5.33	0.13	5.55	5.58	5.60	-0.02
7	5.43	5.39	0	5.43	5.45	5.45	-0.02
8	5.43	5.39	-0.01	5.49	5.50	5.50	0.02
9	5.49	5.46	-0.03	5.61	5.60	5.60	0.01
10	5.61	5.55	0.02	5.49	5.50	5.50	-0.01
11	5.94	5.94	0.04	6.25	6.20	6.20	-0.01
12	7.07	7.07	-0.01	6.98	6.90	6.90	0.08
13	6.98	7.04	-0.01	7.07	7.00	7.00	0.01
14	6.58	6.49	-0.01	5.88	5.90	5.90	-0.02
15	5.27	5.27	-0.02	5.03	5.00	5.00	0
16	5.00	5.00	4.99	4.88	5.00	5.00	0

Remarks:

These measurements are in metric (meters).



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Bridge Number: 140007

Waterway Measurements

Inspection Date: 02-19-97

LEFT

RIGHT

Dist.

Bent No.

Dist.

Bent No.

Distance from water at time of inspection:

to

Distance from _____ to mudline

"-" Sign Denotes Degradation

"+" Sign Denotes Aggregation

Left

Right

Bent No.	Original	Previous	Present	Difference	Original	Previous	Present	Difference
17	5.18	5.5	5.19	0.31	5.06	5.06	5.05	0.01
18	5.15	5.09	5.10	-0.01	5.18	5.18	5.20	-0.02
19	5.06	5.00	5.00	0	5.00	5.00	5.00	0
20	4.72	4.72	4.75	-0.03	4.69	4.66	4.70	-0.04
21	3.29	3.23	3.20	0.03	3.20	3.14	3.15	-0.01
22	1.52	1.43	1.44	-0.01	1.52	1.37	1.44	-0.07
				0				0
				0				0
				0				0
				0				0
				0				0
				0				0
				0				0
				0				0
				0				0
				0				0

Remarks:

These measurements are in metric (meters).

Evaluation: The gutterline and scuppers have been adequately cleaned.

Repair Description: Clean sand and debris from the gutters and scuppers.

Activity: 805 SF Debris Removal
Number of Units: 200

G6.09 DECK CLEANNESS

Evaluation: Piles 11-5, 16-5, 19-1 and 20-2 have been jacketed.

Repair Description: Install a timber helper pile adjacent to Piles Nos. 11-5 and 20-2.

Activity: 855 LF Substructure-Timber Pile
Number of Units: 80

G3.01 PILING

C. Evaluation of Previous Corrective Action

Bridge No.:	140007	Location: 2 Miles south of US-301
County Section No.:	14110	Inspection Date: 02-19-97
State Road No.:	39	Inspector: K.S. King
US Road No.:	N/A	Mile Post No.: 1.585

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Bridge No.: 140007 Location: 2 Miles south of US-301
 County Section No.: 14110 Inspection Date: 02-19-97
 State Road No.: 39 Inspector: K.S. King
 US Road No.: N/A Mile Post No.: 1.585

D. REQUIRED MAINTENANCE REPAIR & REHABILITATION

STATE FORCES

G3.01 PILING

Activity: 850 MH Bridge Substructure M&R
 Number of Units: 30

Repair Description:
 On pile 3-4, determine the depth below ground of deep rot and install a structural pile jacket.

COMMENTS:

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National Bridge Inventory
 Structure Inventory and Appraisal Report
 140007

Last NBI Inspection 2/1/97

Sufficiency Rating	78
Status	1

Identification	
State Name: Florida	Region: Atlanta
Bridge ID: 140007	
Inventory Route: (On/Under): On Route On Structure	
Kind Highway: 3 State Highway	
Level of Service: Mainline	
Route Number: 00039	
Directional Suffix:	
Highway Agency District: D7 - Tampa	
County Code: (14)Pasco	Place Code: No city involved
Features Intersected: HILLSBOROUGH RIVER	
Facility Name: SR 39	
Location: 3.2 KM SOUTH OF US 301	
Kilometer Point: 1.585 km	
Onbasenet: 1	
SubRt Num: 0	
Latitude: 281148	
Longitude: 820948	
Border Bridge State Code: -2	% Share: 0 %
Border Bridge Structure No.:	
Structure Type & Material	
Main NBI Unit	
Material Co	
Design	Sla
Age and Service	
Year Built: 1947	
Year Reconstruction:	
Type Service: On: 1	Under: 5
Avg Daily Traffic: 6800	Year of ADT: 1993
Lanes: 2	Truck Pct: 20 %
Detour Length: 5 km	

Classification	
NBIS Bridge Length: Y	
Highway System: 3 State Highway	
Functional Class: 02 Rural Princ. Arterial - Other	
Defense Highway: 0	
Parallel Structure: N	
Directions of Traffic: 2	
Temporary Structure:	
Federal Lands Highways:	
Designated National Network: 0	
Toll: 3 On Free Road	
Maintenance Responsibility:	
Owner: 1 State Highway Agency	
Historical Significance: 5	
Not Eligible for Natl. Reg. Hist. Places	
Condition	
Deck: 7	
Superstructure: 7	
Substructure: 7	
Channel and Channel Protection:	
Culverts: 8	
Structure Open, Posted, or Closed: A	
Load Rating and Posting	
Design Load: M	
Operating Rating Method: 1	
Operating Rating: 58	
Inventory Rating Method: 1	
Inventory Rating: 35.3	
Bridge Posting: 5	

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Geometric Data

Length of Maximum Span: 4.6 m
 Structure Length: 96 m
 Curb or Sidewalk: Lt: 0.4 m Rt: 0.4 m
 Rdway Width Curb to Curb: 7.9 m
 Deck Width Out to Out: 9.3 m
 Appr Rdwy (w/Shoulders): 9.7 m
 Bridge Median: 0 # 0
 Skew: 0 Structure Flared: No flare
 Min Vert Ctr/Inv Route: 99.99 m
 Invt Rte Total Horiz Clear: 7.9 m
 Min Vert Clear over Bridge Rdwy: 99.99 m
 Min Vert Underclear: Reference: 0 m
 Min Horiz Lat UndrClrs: Reference: 0 m
 Rt: 0 m
 Lt: 0 m

Appraisal

Structural Evaluation: 7
 Deck Geometry: 2
 Underclrs, Vertical_Horizontal: N
 Waterway Adequacy: 8
 Approach Roadway Alignment: 8

Traffic Safety Features

Bridge Guardrails: 0
 Transitions: 1
 Approach Guardrails: 1
 Approach Guardrail Ends: 0
 Scour Critical Bridge: 3

Proposed Improvements

Type of Work 38 By: 1
 Length of Structure improvement: 9.6
 Bridge Improvement Cost \$Thousands: 74000
 Roadway Improvement Cost \$Thousands: 7000
 Total Project Cost \$Thousands: 81000
 Improvement Cost Estimate (Yr.): 1997
 Future ADT: 7980
 Year of Future ADT: 2018

Navigation Data

Navigation Control: 0
 Pier Protection: 1
 Navigation Vertical Clearance: 0 m
 Vert-Lift Bridge Nav Min Vert Clear: 0 m
 Navigation Horizontal Clearance: 0 m

Past Inspections

Inspection Date: 02.01.1997 Type: 1
 Inspector: BID Pontis User Key: BID
 Inspection Notes:

Structural Units

Structural Unit: 0 MAIN SPAN 1 NBI Main Span NBI Approach Span
 Notes:

Bridge Notes

APPENDIX C

CROSS DRAIN CALCULATIONS

CROSS DRAIN CALCULATIONS CONTENTS

- I. EXISTING CULVERT D-5
 - I.A. DISCHARGE RATES AND TAILWATER ELEVATIONS
 - I.B. TYPICAL SECTION
 - I.C. 50-YEAR AND 100-YEAR CULVERT CAPACITY ANALYSES
 - I.D. RESULTS

- II. PROPOSED CULVERT AB-1
 - II.A. DISCHARGE RATES AND TAILWATER ELEVATIONS
 - II.B. CULVERT LOCATION AND CROSS SECTION
 - II.C. 50-YEAR AND 100-YEAR CULVERT CAPACITY ANALYSES
 - II.D. RESULTS

- III. PROPOSED CULVERT AB-2
 - III.A. DISCHARGE RATES AND TAILWATER ELEVATIONS
 - III.B. CULVERT LOCATION AND CROSS SECTION
 - III.C. 50-YEAR AND 100-YEAR CULVERT CAPACITY ANALYSES
 - III.D. RESULTS

- IV. PROPOSED CULVERT AB-3
 - IV.A. DISCHARGE RATES AND TAILWATER ELEVATIONS
 - IV.B. CULVERT LOCATION AND CROSS SECTION
 - IV.C. 50-YEAR AND 100-YEAR CULVERT CAPACITY ANALYSES
 - IV.D. RESULTS

- V. PROPOSED CULVERT AB-4
 - V.A. DISCHARGE RATES AND TAILWATER ELEVATIONS
 - V.B. CULVERT LOCATION AND CROSS SECTION
 - V.C. 50-YEAR AND 100-YEAR CULVERT CAPACITY ANALYSES
 - V.D. RESULTS

- VI. PROPOSED CULVERT AB-5
 - VI.A. DISCHARGE RATES AND TAILWATER ELEVATIONS
 - VI.B. CULVERT LOCATION AND CROSS SECTION
 - VI.C. 50-YEAR AND 100-YEAR CULVERT CAPACITY ANALYSES
 - VI.D. RESULTS

- VII. HILLSBOROUGH RIVER WSPRO ANALYSIS
 - VII.A. S.R. 39 BRIDGE OVER THE HILLSBOROUGH RIVER REQUIREMENTS
 - VII.B. EXISTING CONDITIONS
 - VII.C. PROPOSED CONDITIONS
 - VII.D. WSPRO ANALYSIS, EXISTING CONDITIONS
 - VII.E. WSPRO ANALYSIS, PROPOSED CONDITIONS
 - VII.F. RESULTS

I. EXISTING CULVERT D-5

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET / OF 2 PROJ. NO. C100003240.19
DESCRIPTION: I.A. DISCHARGE RATES COMPUTED BY: Zinner DATE: 5-27-99
AND TAILWATER ELEVATIONS CHECKED BY: Pratt DATE: 5-28-99

Discharge rates for culvert D-5 were calculated using a USGS Regression Equation. The applicable USGS Regression Equation for natural flow conditions in Florida: Section A (Table 5-12, FDOT Drainage Manual, 1987) was used for computing the peak flow for this basin. See the enclosed calculations for the peak discharge rates and they are as follows:

<u>Event (year)</u>	<u>Discharge Rate (cfs)</u>	<u>Source</u>
50	234	USGS regression equation
100	288	USGS regression equation

The elevation of the crown of the proposed cross drain and the seasonal high water table (SHWT) elevation was compared, and the higher stage was used for the proposed D-5 capacity analyses. In this case the SHWT elevation was used. The nearest field verified SHWT elevation was located at the station 79+25 and the SHWT elevation is 101.99 NGVD (102.00 was used).

Table 5-12 USGS Regression Equations

Where:
 $Q_{50} = 496 DA^{0.690} SL^{0.234} (LK + 3)^{-0.705}$
 $Q_{100} = 609 DA^{0.685} SL^{0.227} (LK + 3)^{-0.695}$

DA = Drainage Area (mi²)
 SL = channel slope between points at 10% & 85% of total channel length (ft/mi) (Min. = 0.9)
 LK = lake area (% lake area of total number/total)

D-5

DA = 896 ac = 1.4 mi²
 SL = 10% - elev = 104
 85% - elev = 117
 $\Delta = 13'$
 $SL = 13' / 0.923 mi = 14.08$
 $LK = 2000' \times 1300' = 0.093 mi^2 = 6.7\%$

$Q_{50} = 496 (1.4)^{0.690} * (14.08)^{0.234} * (6.7+3)^{-0.705} = 234 cfs$
 $Q_{100} = 609 (1.4)^{0.685} * (14.08)^{0.227} * (6.7+3)^{-0.695} = 238 cfs$

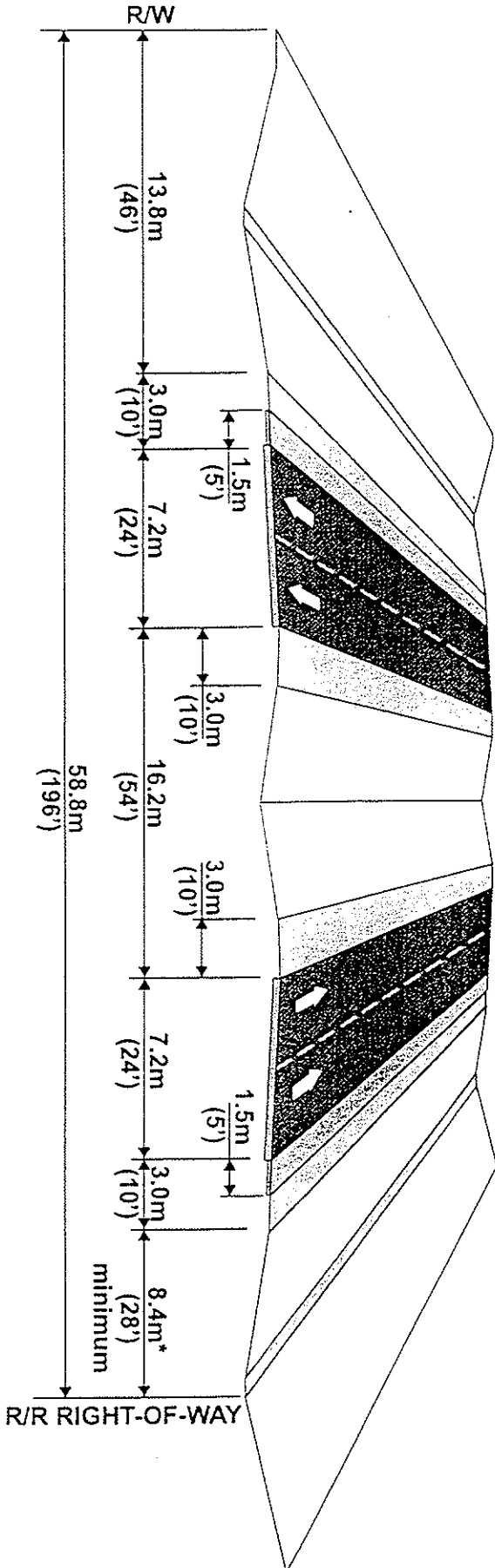
$DA = 183 ac = 0.286 mi^2$
 $SL = 6 ft / 0.568 mi = 10.56$
 $LK = 2\%$

$Q_{50} = 496 (0.286)^{0.690} * (10.56)^{0.234} * (2+3)^{-0.705} = 117 cfs$
 $Q_{100} = 609 (0.286)^{0.685} * (10.56)^{0.227} * (2+3)^{-0.695} = 144 cfs$

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET ² / OF ~~2~~ PROJ. NO. C100003240.19
DESCRIPTION: I. B. TYPICAL SECTION COMPUTED BY: Zinner DATE: 5-27-99
CHECKED BY: Pratt DATE: 5-28-99

See the enclosed typical section proposed for where D-5 will be located.



FROM S.R. 39 TO BLOUNT STREET

Based on 1.5' of Fill to Proposed PGL & Sharing R/R Right-of-Way

* Does Not Meet Border Criteria.
However, it does meet clear zone criteria.

TYPICAL SECTION 8

S.R. 39 FROM I-4 TO U.S. 301
WPI SEGMENT No. 255099 1 FAP No. F-321-1(4)
HILLSBOROUGH AND PASCO COUNTIES, FLORIDA



URS Greiner

Figure 4

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET / OF 7 PROJ. NO. C100003240.19
DESCRIPTION: I.C. 50-YEAR AND 100- COMPUTED BY: Zinner DATE: 5-27-99
YEAR CULVERT CAPACITY ANALYSES CHECKED BY: Pratt DATE: 5-28-99

The capacity of the proposed culvert AB-5 was analyzed for the 50- and 100-year storm events using HY-8, software based on the techniques provided in FHWA Hydraulic Design Series # 5. See the enclosed HY-8 output for the analyses.

EXISTING CONDITIONS

2/7

D-5

FILE DATE: 06-03-1999 FILE NAME: DSX.LC
 CURRENT DATE: 06-03-1999 CURRENT TIME: 22:30:56

FHWA CULVERT ANALYSIS
 HY-8, VERSION 6.0

SITE DATA		CULVERT SHAPE, MATERIAL, INLET			
U	L	INLET	OUTLET	CULVERT	BARRELS
NO.	ELEV. (ft)	ELEV. (ft)	ELEV. (ft)	LENGTH (ft)	SHAPE
V	98.66	98.52	98.52	85.00	2 RCB
L					
U					

SUMMARY OF CULVERT FLOWS (cfs) FILE: DSX.LC DATE: 06-03-1999

ELEV (ft)	TOTAL	1	2	3	4	5	6 ROADWAY ITR
103.21	234.0	234.0	0.0	0.0	0.0	0.0	1
103.27	239.4	239.4	0.0	0.0	0.0	0.0	1
103.33	244.8	244.8	0.0	0.0	0.0	0.0	1
103.39	250.2	250.2	0.0	0.0	0.0	0.0	1
103.45	255.6	255.6	0.0	0.0	0.0	0.0	1
103.51	261.0	261.0	0.0	0.0	0.0	0.0	1
103.57	266.4	266.4	0.0	0.0	0.0	0.0	1
103.64	271.8	271.8	0.0	0.0	0.0	0.0	1
103.70	277.2	277.2	0.0	0.0	0.0	0.0	1
103.77	282.6	282.6	0.0	0.0	0.0	0.0	1
103.84	288.0	288.0	0.0	0.0	0.0	0.0	1
104.33	323.6	323.6	0.0	0.0	0.0	0.0	0.0 OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DSX.LC DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
103.21	0.000	234.00	0.00	0.00
103.27	0.000	239.40	0.00	0.00
103.33	0.000	244.80	0.00	0.00
103.39	0.000	250.20	0.00	0.00
103.45	0.000	255.60	0.00	0.00
103.51	0.000	261.00	0.00	0.00
103.57	0.000	266.40	0.00	0.00
103.64	0.000	271.80	0.00	0.00
103.70	0.000	277.20	0.00	0.00
103.77	0.000	282.60	0.00	0.00
103.84	0.000	288.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010 <2> TOLERANCE (%) = 1.000

3/7

CURRENT DATE: 06-03-1999
CURRENT TIME: 22:30:56

FILE DATE: 06-03-1999
FILE NAME: D5X_LC

PERFORMANCE CURVE FOR CULVERT 1 - 2(6.00 (ft) BY 3.00 (ft)) RCB

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
234.00	103.21	4.03	4.55	4-FFt	3.00	2.28	3.00	3.47	6.50	0.00
239.40	103.27	4.11	4.61	4-FFt	3.00	2.32	3.00	3.47	6.65	0.00
244.80	103.33	4.19	4.67	4-FFt	3.00	2.35	3.00	3.47	6.80	0.00
250.20	103.39	4.28	4.73	4-FFt	3.00	2.39	3.00	3.47	6.95	0.00
255.60	103.45	4.36	4.79	4-FFt	3.00	2.42	3.00	3.47	7.10	0.00
261.00	103.51	4.45	4.85	4-FFt	3.00	2.45	3.00	3.47	7.25	0.00
266.40	103.57	4.54	4.91	4-FFt	3.00	2.49	3.00	3.47	7.40	0.00
271.80	103.64	4.63	4.98	4-FFt	3.00	2.52	3.00	3.47	7.55	0.00
277.20	103.70	4.72	5.04	4-FFt	3.00	2.55	3.00	3.47	7.70	0.00
282.60	103.77	4.82	5.11	4-FFt	3.00	2.59	3.00	3.47	7.85	0.00
288.00	103.84	4.91	5.18	4-FFt	3.00	2.62	3.00	3.47	8.00	0.00

El. inlet face invert	98.66 ft	El. outlet invert	98.52 ft
El. inlet throat invert	0.00 ft	El. inlet crest	0.00 ft

***** SITE DATA ***** CULVERT INVERT *****

INLET STATION	0.00 ft
INLET ELEVATION	98.66 ft
OUTLET STATION	85.00 ft
OUTLET ELEVATION	98.52 ft
NUMBER OF BARRELS	2
SLOPE (V/H)	0.0016
CULVERT LENGTH ALONG SLOPE	85.00 ft

***** CULVERT DATA SUMMARY *****

BARREL SHAPE	BOX
BARREL SPAN	6.00 ft
BARREL RISE	3.00 ft
BARREL MATERIAL	CONCRETE
BARREL MANNING'S n	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE (90-45 DEG.)
INLET DEPRESSION	NONE

CURRENT DATE: 06-03-1999
CURRENT TIME: 22:30:56
FILE DATE: 06-03-1999
FILE NAME: DSX.LC

3

TAILWATER

CONSTANT WATER SURFACE ELEVATION
101.99

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE
EMBANKMENT TOP WIDTH
CREST LENGTH
OVERTOPPING CREST ELEVATION
PAVED
32.00 ft
4500.00 ft
104.33 ft

4/7

5/7

D-5
PROPOSED CONDITIONS

1

CURRENT DATE: 06-03-1999
 CURRENT TIME: 21:22:30

FILE DATE: 06-03-1999
 FILE NAME: D5P_LC

FHWA CULVERT ANALYSIS
 HY-8, VERSION 6.0

C U L V E R T N O. 1 2 3 4 5 6	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	98.82	98.50	196.00	2 RCB	6.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: D5P_LC DATE: 06-03-1999

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
50 YR - 103.32	234.0	234.0	0.0	0.0	0.0	0.0	0.0	0.00	1
103.38	239.4	239.4	0.0	0.0	0.0	0.0	0.0	0.00	1
103.45	244.8	244.8	0.0	0.0	0.0	0.0	0.0	0.00	1
103.51	250.2	250.2	0.0	0.0	0.0	0.0	0.0	0.00	1
103.58	255.6	255.6	0.0	0.0	0.0	0.0	0.0	0.00	1
103.64	261.0	261.0	0.0	0.0	0.0	0.0	0.0	0.00	1
103.71	266.4	266.4	0.0	0.0	0.0	0.0	0.0	0.00	1
103.78	271.8	271.8	0.0	0.0	0.0	0.0	0.0	0.00	1
103.85	277.2	277.2	0.0	0.0	0.0	0.0	0.0	0.00	1
103.93	282.6	282.6	0.0	0.0	0.0	0.0	0.0	0.00	1
100 YR - 104.00	288.0	288.0	0.0	0.0	0.0	0.0	0.0	0.00	1
105.95	404.2	404.2	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: D5P_LC DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
103.32	0.000	234.00	0.00	0.00
103.38	0.000	239.40	0.00	0.00
103.45	0.000	244.80	0.00	0.00
103.51	0.000	250.20	0.00	0.00
103.58	0.000	255.60	0.00	0.00
103.64	0.000	261.00	0.00	0.00
103.71	0.000	266.40	0.00	0.00
103.78	0.000	271.80	0.00	0.00
103.85	0.000	277.20	0.00	0.00
103.93	0.000	282.60	0.00	0.00
104.00	0.000	288.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 06-03-1999
 CURRENT TIME: 21:22:30
 FILE NAME: DSP.LC
 FILE DATE: 06-03-1999

PERFORMANCE CURVE FOR CULVERT 1 - 2 (6.00 (ft) BY 3.00 (ft)) RCB

DIS- CHARGE	HEAD- INLET	OUTLET	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	DEPTH	
(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
TM	OUTLET	TM	OUTLET	TM	OUTLET	TM	OUTLET	TM	OUTLET	TM	OUTLET	TM	OUTLET	TM	OUTLET	TM	OUTLET	TM	OUTLET
VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)	VEL. (fps)

234.00	103.32	3.68	4.50	4-ft	3.00	2.28	3.00	3.49	6.50	0.00
239.40	103.38	3.75	4.56	4-ft	3.00	2.32	3.00	3.49	6.65	0.00
244.80	103.45	3.82	4.63	4-ft	3.00	2.35	3.00	3.49	6.80	0.00
250.20	103.51	3.89	4.69	4-ft	3.00	2.39	3.00	3.49	6.95	0.00
255.60	103.58	3.96	4.76	4-ft	3.00	2.42	3.00	3.49	7.10	0.00
261.00	103.64	4.04	4.82	4-ft	3.00	2.45	3.00	3.49	7.25	0.00
266.40	103.71	4.11	4.89	4-ft	3.00	2.49	3.00	3.49	7.40	0.00
271.80	103.78	4.19	4.96	4-ft	3.00	2.52	3.00	3.49	7.55	0.00
277.20	103.85	4.26	5.03	4-ft	3.00	2.55	3.00	3.49	7.70	0.00
282.60	103.93	4.34	5.11	4-ft	3.00	2.59	3.00	3.49	7.85	0.00
288.00	104.00	4.42	5.18	4-ft	3.00	2.62	3.00	3.49	8.00	0.00

El. inlet face invert 98.82 ft El. outlet invert 98.50 ft
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA *****
 INLET STATION 0.00 ft
 INLET ELEVATION 98.82 ft
 OUTLET STATION 196.00 ft
 OUTLET ELEVATION 98.50 ft
 NUMBER OF BARRELS 2
 SLOPE (V/H) 0.0016
 CULVERT LENGTH ALONG SLOPE 196.00 ft
 ***** CULVERT DATA SUMMARY *****

BARREL SHAPE BOX
 BARREL SPAN 6.00 ft
 BARREL RISE 3.00 ft
 BARREL MATERIAL CONCRETE
 BARREL MANNING'S n 0.012
 INLET TYPE CONVENTIONAL
 INLET EDGE AND WALL 1:1 BEVEL
 INLET DEPRESSION NONE

6/7

7/7

CURRENT DATE: 06-03-1999
CURRENT TIME: 21:22:30

FILE DATE: 06-03-1999
FILE NAME: DSP_LC

TAILWATER

CONSTANT WATER SURFACE ELEVATION
101.99

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	182.00 ft
CREST LENGTH	1600.00 ft
OVERTOPPING CREST ELEVATION	105.95 ft

JOB: SR 39 FROM I-4 TO U.S. 301
 SHEET 7 OF 7 PROJ. NO. C100003240.19
 DESCRIPTION: I.D. RESULTS
 COMPUTED BY: Zinner DATE: 5-27-99
 CHECKED BY: Pratt DATE: 5-28-99

The cross drain which satisfies the 0.1' rise for the 50-year storm event is a double 6'x3' CBC.

The results of the HY-8 analyses for the proposed culvert D-5 are shown below:

Event (Year)	Existing Headwater/ Tailwater Elevation feet (NGVD)	Proposed Headwater Elevation feet (NGVD)
50	103.21	103.32
100	103.84	104.00

II. PROPOSED CULVERT AB-1

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET / OF / PROJ. NO. C100003240.19
DESCRIPTION: II. A. DISCHARGE RATES COMPUTED BY: Zinner DATE: 5-27-99
AND TAILWATER ELEVATIONS CHECKED BY: Pratt DATE: 5-28-99

Available discharge rates for proposed culvert AB-1 were taken from City of Plant City, Florida, WESTSIDE CANAL, STORMWATER MANAGEMENT MASTER PLAN, MAY 1997" by Camp Dresser & McKee (CDM). See the enclosed title sheet, maps, and HEC-1 outputs (partial) obtained from the aforementioned CDM report. The basin where the proposed cross drain AB-1 will be located is node number 6405 in the CDM model. The storm events provided in the report were the 10, 25, and 100 year frequencies; and all of those events were for a 24 hours duration. The discharge rates for the 25 year and the 100 year were taken from the HEC-1 outputs and the 50 year discharge rate was interpolated from them. See the enclosed interpolation for the 50 year peak discharge rate. The peak discharge rates are as follows:

<u>Event (year)</u>	<u>Discharge Rate (cfs)</u>	<u>Source</u>
50	100	interpolation
100	131	CDM report

The peak stage for the 50-year event was interpolated from the peak stages obtained from Table 4-1 of the CDM report. See the enclosed Table 4-1 from the CDM report. For the proposed cross drain AB-1 capacity analysis, the existing conditions tailwater and headwater was assumed to be the same as the peak stage within node number 6405 because of its central location within the basin/node. See the enclosed interpolation for the 50 year peak stage. The existing peak stages are as follows:

<u>Event (year)</u>	<u>Peak Stage (ft. NGVD)</u>	<u>Source</u>
50	107.0	interpolation
100	107.4	CDM report

Report

CDM

Camp Dresser & McKee

2/10

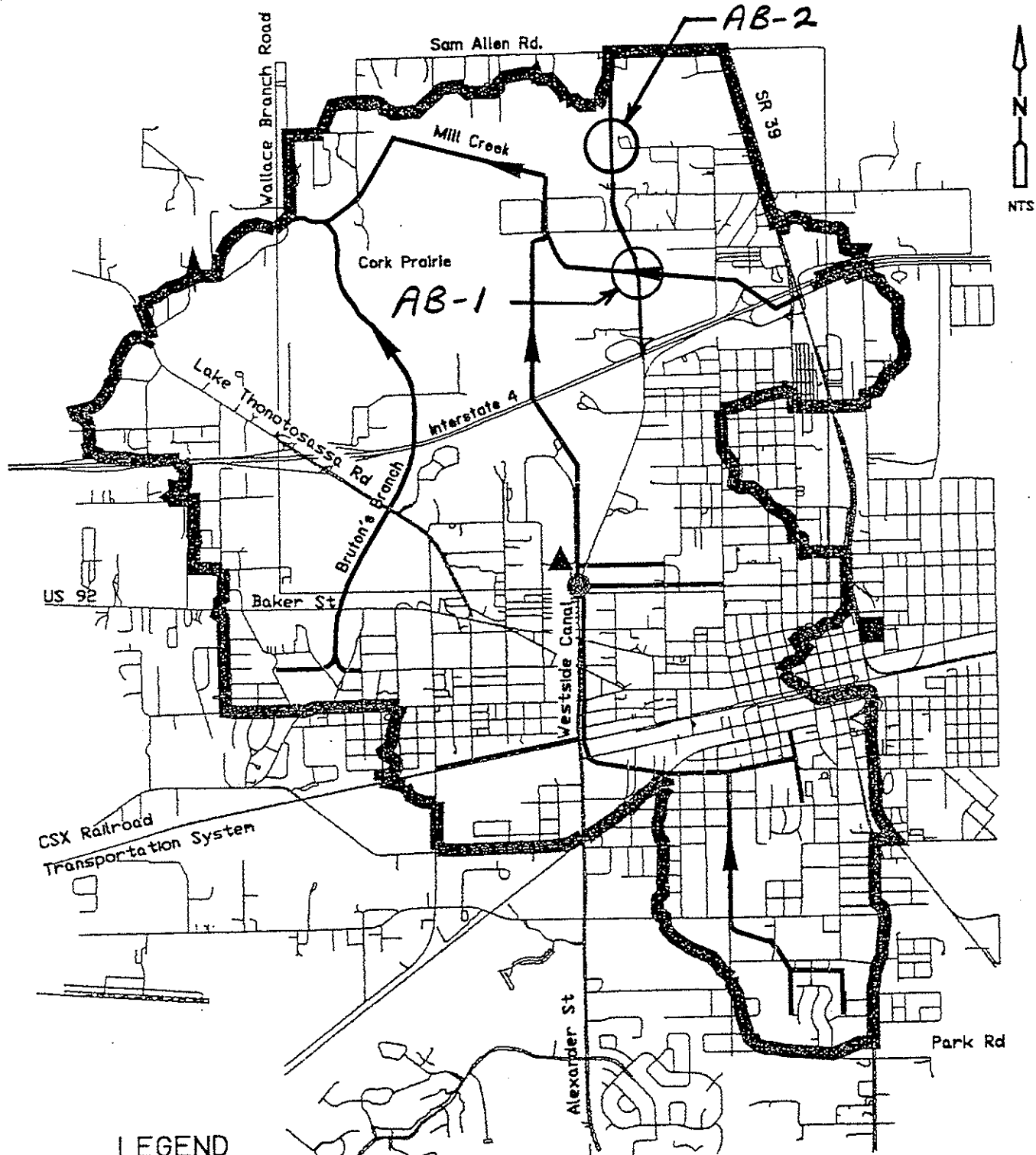
City of Plant City, Florida

WESTSIDE CANAL




STORMWATER MANAGEMENT MASTER PLAN

MAY 1997

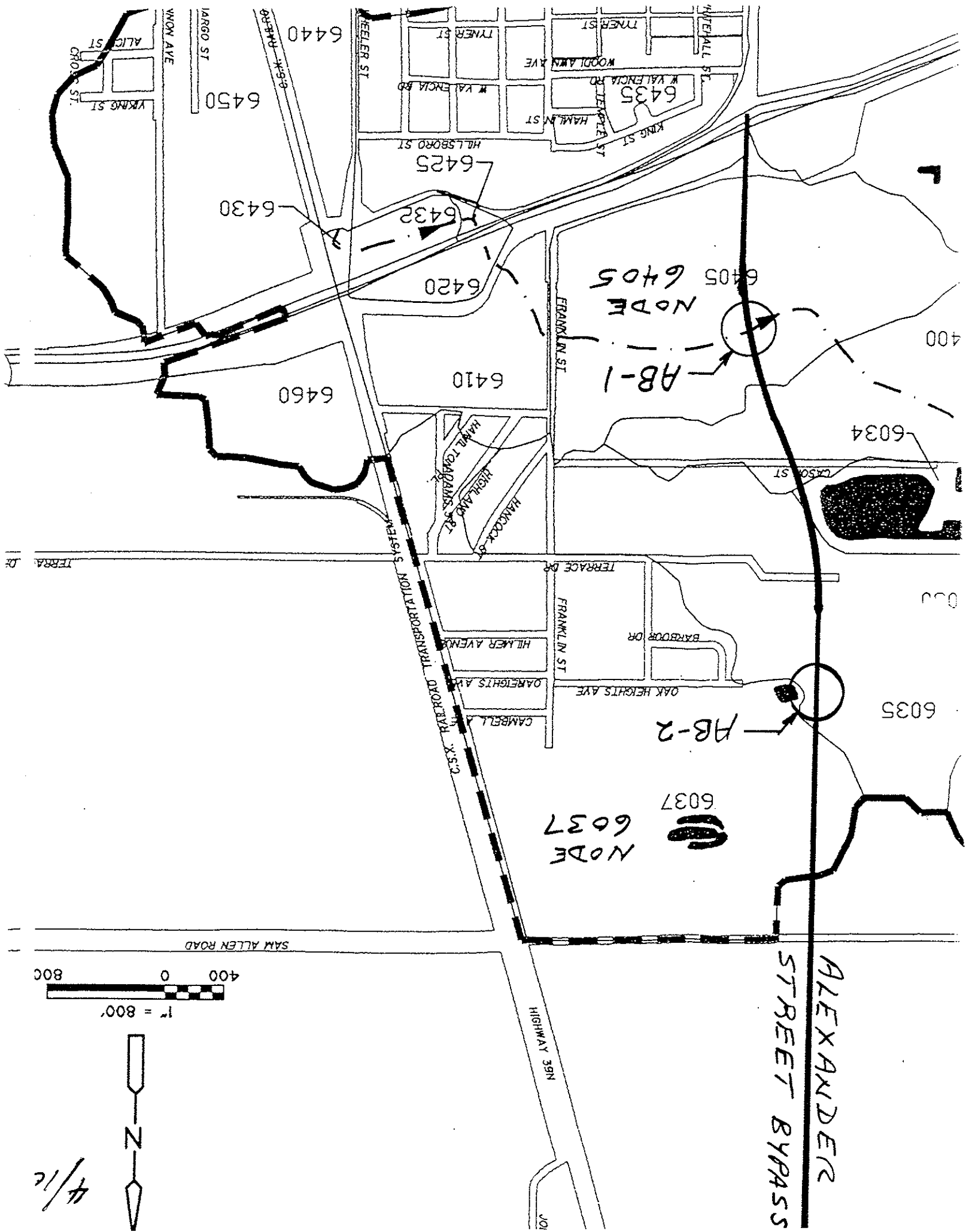
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LEGEND

-  VICTORIA ST. CROSSING
STAGE/FLOW MONITOR
-  NATIONAL WEATHER SERVICE
DAILY RAINFALL STATION
-  PLANT CITY HERRING ST. WATER PLANT
10-MINUTE RAIN GAUGE

**CITY OF PLANT CITY WESTSIDE CANAL
STORMWATER MANAGEMENT MASTER PLAN
STAGE/FLOW MONITOR AND RAIN GAUGE LOCATION**



5/10

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* FEBRUARY 1991 *
* VERSION 4.0.1 (LOCAL) *
* RUN DATE 06/15/98 TIME 09:20:36 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> Plant City Westside Canal SMMP 25 YEAR STORM EVENT HEC-1: FLOOD HYDROGRAPH PACKAGE </div>									
2	ID										
3	ID										
*** FREE ***											
4	IT	3	07JAN98	0	601						
5	IN	15	07JAN98	0							
6	IO	5	0								
7	JR	PREC	7.5								
8	PG	DC24	1.00								
9	PC	0	0.0001	0.0002	0.0003	0.0005	0.0007	0.001	0.0014	0.0018	0.0023
10	PC	0.0029	0.0036	0.0045	0.0055	0.0065	0.0076	0.0089	0.0115	0.0143	0.0172
11	PC	0.0203	0.0239	0.0277	0.0316	0.0357	0.042	0.0485	0.055	0.0616	0.0701
12	PC	0.0787	0.0873	0.096	0.1086	0.1212	0.1339	0.1466	0.1626	0.1786	0.1946
13	PC	0.2106	0.2315	0.2524	0.2734	0.2945	0.3306	0.3668	0.403	0.4392	0.4918
14	PC	0.5445	0.5972	0.6499	0.6737	0.6975	0.7213	0.7451	0.7638	0.7825	0.8012
15	PC	0.82	0.8342	0.8484	0.8626	0.8769	0.8875	0.8981	0.9087	0.9192	0.9273
16	PC	0.9354	0.9435	0.9516	0.957	0.9625	0.968	0.9734	0.9768	0.98	0.9831
17	PC	0.9862	0.9882	0.9902	0.9922	0.9941	0.995	0.9958	0.9965	0.9972	0.9977
18	PC	0.9982	0.9986	0.999	0.9993	0.9996	0.9998	1	1	1	1
19	PC	1	1	1	1						
20	KK	6005									
21	KM			RUNOFF FROM		6005					
22	KO	0	0	0	0	21					
23	BA	0.01547									
24	PR	DC24									
25	LS	0	57	0	0	0	0	0.05			
26	UD	0.240									
27	KK	6006									
28	KM			RUNOFF FROM		6006					
29	KO	0	0	0	0	21					
30	BA	0.02109									
31	PR	DC24									
32	LS	0	61	0	0	0	0	0.05			
33	UD	0.190									
34	KK	9999									
35	HC	2									
36	KK	6005									
37	KM			RUNOFF FROM		6010					
38	KO	0	0	0	0	21					
39	BA	0.02844									
40	PR	DC24									
41	LS	0	57	0	0	0	0	0.05			
42	UD	0.330									

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
43	KK	9999									

Handwritten: $\Sigma = 76 \text{ CFS} = 0.25$
Confirmed by Jack Adams at CDM

ID	Flow Type	Flow Rate	Time	Notes
6425	HYDROGRAPH AT	0.00	13.00	
9999	2 COMBINED AT	2.37	13.20	
6420	HYDROGRAPH AT	0.01	13.00	
9999	2 COMBINED AT	2.36	13.25	
6410	HYDROGRAPH AT	0.06	13.25	
9999	2 COMBINED AT	2.30	13.25	
6405	HYDROGRAPH AT	0.13	13.35	
9999	2 COMBINED AT	2.17	13.20	
6040	HYDROGRAPH AT	0.07	13.25	
9999	2 COMBINED AT	2.10	13.20	
6360	HYDROGRAPH AT	0.07	13.15	
9999	2 COMBINED AT	2.03	13.20	
6350	HYDROGRAPH AT	0.03	13.15	
9999	2 COMBINED AT	1.99	13.25	
6344	HYDROGRAPH AT	0.04	13.20	
9999	2 COMBINED AT	1.95	13.25	
6342	HYDROGRAPH AT	0.01	13.10	
9999	2 COMBINED AT	1.94	13.25	
6341	HYDROGRAPH AT	0.01	13.15	
9999	2 COMBINED AT	1.93	13.25	
6340	HYDROGRAPH AT	0.10	13.30	
9999	2 COMBINED AT	1.82	13.25	
6335	HYDROGRAPH AT	0.14	13.30	
	TIM		13.20	

Handwritten: 6/10

7/10

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*****
FLOOD HYDROGRAPH PACKAGE (HEC-1)
FEBRUARY 1991
VERSION 4.0.1 (LOCAL)
*****
RUN DATE 02/16/98 TIME 14:40:07
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*****
U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 551-1748
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X X XXXXXXX XXXXX XXX
    
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID
2 ID
3 ID
*** FREE ***
4 IT 3 02FEB98 0 601
5 IN 15 02FEB98 0
6 IO 5 0
7 JR PREC 10.5
8 PG DC24 1.00
9 PC 0 0.0001 0.0002 0.0003 0.0005 0.0007 0.001 0.0014 0.0018 0.0023
10 PC 0.0029 0.0036 0.0045 0.0055 0.0065 0.0076 0.0089 0.0115 0.0143 0.0172
11 PC 0.0203 0.0239 0.0277 0.0316 0.0357 0.042 0.0485 0.055 0.0616 0.0701
12 PC 0.0787 0.0873 0.096 0.1086 0.1212 0.1339 0.1466 0.1626 0.1786 0.1946
13 PC 0.2106 0.2315 0.2524 0.2734 0.2945 0.3306 0.3668 0.403 0.4392 0.4918
14 PC 0.5445 0.5972 0.6499 0.6737 0.6975 0.7213 0.7451 0.7638 0.7825 0.8012
15 PC 0.82 0.8342 0.8484 0.8626 0.8769 0.8875 0.8981 0.9087 0.9192 0.9273
16 PC 0.9354 0.9435 0.9516 0.957 0.9625 0.966 0.9734 0.9768 0.98 0.9831
17 PC 0.9862 0.9882 0.9902 0.9922 0.9941 0.995 0.9958 0.9965 0.9972 0.9977
18 PC 0.9982 0.9986 0.999 0.9993 0.9996 0.9998 1 1 1 1
19 PC 1 1 1 1
20 KK 6005
21 KM RUNOFF FROM 6005
22 KO 0 0 0 21
23 BA 0.01547
24 PR DC24
25 LS 0 57 0 0 0 0 0.05
26 UD 0.230
27 KK 6006
28 KM RUNOFF FROM 6006
29 KO 0 0 0 21
30 BA 0.02109
31 PR DC24
32 LS 0 61 0 0 0 0 0.05
33 UD 0.180
34 KK 9999
35 HC 2
36 KK 6005
37 KM RUNOFF FROM 6010
38 KO 0 0 0 21
39 BA 0.02844
40 PR DC24
41 LS 0 57 0 0 0 0 0.05
42 UD 0.310
    
```

HEC-1 INPUT

1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
43 KK 9999
    
```

8/10

2 COMBINED AT	9999	2.10	1	FLOW TIME	1519. 13.20
HYDROGRAPH AT	6040	0.07	1	FLOW TIME	56. 13.25
2 COMBINED AT	9999	2.17	1	FLOW TIME	1576. 13.20
HYDROGRAPH AT	6405	0.13	1	FLOW TIME	94 13.30
2 COMBINED AT	9999	2.30	1	FLOW TIME	1668. 13.20
HYDROGRAPH AT	6410	0.06	1	FLOW TIME	37 13.20
2 COMBINED AT	9999	2.36	1	FLOW TIME	1706. 13.20
HYDROGRAPH AT	6420	0.01	1	FLOW TIME	11. 13.00
2 COMBINED AT	9999	2.37	1	FLOW TIME	1715. 13.20
HYDROGRAPH AT	6425	0.00	1	FLOW TIME	2. 13.00
2 COMBINED AT	9999	2.38	1	FLOW TIME	1716. 13.20
HYDROGRAPH AT	6430	0.01	1	FLOW TIME	11. 13.00
2 COMBINED AT	9999	2.39	1	FLOW TIME	1726. 13.20
HYDROGRAPH AT	6432	0.00	1	FLOW TIME	2. 13.00
2 COMBINED AT	9999	2.39	1	FLOW TIME	1728. 13.20
HYDROGRAPH AT	6435	0.13	1	FLOW TIME	71. 13.30
2 COMBINED AT	9999	2.52	1	FLOW TIME	1798. 13.20
HYDROGRAPH AT	6440	0.03	1	FLOW TIME	17. 13.20
2 COMBINED AT	9999	2.55	1	FLOW TIME	1814. 13.20
HYDROGRAPH AT	6450	0.12	1	FLOW TIME	92. 13.20
2 COMBINED AT	9999	2.67	1	FLOW TIME	1906. 13.20
HYDROGRAPH AT	6460	0.04	1	FLOW TIME	28. 13.15
2 COMBINED AT	9999	2.71	1	FLOW TIME	1934. 13.20

$\Sigma = 131 \text{ cfs} = Q_{100}$
 confirmed by
 Jack Adams
 of CDM

1

HEC-1 INPUT

PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

TABLE 4-1

City of Plant City
 Westside Canal Stormwater Management Master Plan
 Summary of Peak Flood Stages for Design Storms and Problem Areas

Model Node	Location	Top of Road (ft-NGVD)	10-yr/24-hr		25-yr/24-hr		100-yr/24-hr		Problem ID Number
			Peak Stage (ft-NGVD)	Depth of Flooding (ft)	Peak Stage (ft-NGVD)	Depth of Flooding (ft)	Peak Stage (ft-NGVD)	Depth of Flooding (ft)	
6309	Dirt Crossing	106.9	108.1	1.2	108.1	1.2	108.2	1.3	
6310			108.2		108.3		108.5		
6320	I-4	112.5	109.8		110.1		111.0		
6325			111.3		111.4		111.6		
6328			109.8		110.1		111.0		
6330	Thonotossa Road (SR 600)	114.5	110.7		110.9		111.8		
6331			110.7		110.9		111.8		
6332			110.7		110.9		111.8		
6335			109.2		109.3		109.5		
6337			110.7		110.9		111.8		
6340	US 92	112.0	112.1	0.1	112.2	0.2	112.5	0.5	
6341			113.0		113.0		113.2		
6342	Strawberry Festival Service Rd. E.	115.6	114.3		114.5		115.2		
6343			114.4		114.5		115.2		
6344	Ritter Street	120.0	114.4		114.5		115.2		
6349			112.1		112.2		112.5		
6350	Strawberry Festival Service Rd. W.	113.6	112.2		112.3		112.8		
6355			112.2		112.3		112.8		
6360	Seminole Lake Road	112.8	112.6		112.7		113.0	0.2	
6380			112.1		112.2		112.5		
6390	Bennett Road	107.1	107.5	0.4	107.6	0.5	107.6	0.5	
6405			106.4		106.7		107.4		
6409			106.9		107.0		107.4		
6410	Franklin Street	115.9	111.0		111.3		112.3		
6415			111.1		111.4		112.3		
6420	I-4 Westbound Ramp	117.4	111.4		111.8		113.0		
6425	I-4	118.8	111.6		112.0		113.3		
6430	I-4 Eastbound Entrance Ramp	117.5	111.6		112.0		113.4		
6432	Wheeler Street (SR 39)	116.0	115.2		115.4		116.0	0.0	
6435	I-4 Eastbound Exit Ramp	117.6	112.1		112.7		114.8		
6440	Frontage Road S.	117.8	115.5		115.6		115.7		
6450	CSX Railroad/Frontage Road S.	121.5	115.2		115.5		116.6		
6460			117.3		117.3		117.5		



← Peak Stages Utilized

9/10

Note: Level of service is 0.5 ft of road flooding for the 25-yr/24-hr storm and 0.75 ft of road flooding for the 100-yr/24-hr storm.

URS Greiner

JOB: SR 39/ALEXANDER ROAD BYPASS	SHEET 10 of 10	PROJ. NO. C100003240.19
DESCRIPTION: AB-1, 50-yr Q & HW	COMPUTED BY Jim Zinner	DATE 05-25-99
	CHECKED BY <i>RWR</i>	DATE 5-28-99

Input/Output Boxes Explanation

= manually input values

= unknown, previously input, or computed output values

Frequency versus Discharge Log-slope Interpolation

when: $f_3 > f_1$ & $f_3 < f_2$

	frequency (yrs)		discharge (cfs)
f1 =	<input type="text" value="25"/>	Q1 =	<input type="text" value="77"/>
f2 =	<input type="text" value="100"/>	Q2 =	<input type="text" value="131"/>
f3 =	<input type="text" value="50"/>	Q3 =	<input "="" type="text" value="?"/>

$$M = \frac{\log(Q_2) - \log(Q_1)}{\log(f_2) - \log(f_1)} = \text{input } 2.6088$$

$$Q_3 = 10^{[(\log(Q_2) - \log(Q_1)) / M + \log(f_1)]} = \text{input } 100$$

The peak discharge for the year event =

Discharge versus Stage Linear Interpolation

	discharge (cfs)		stage (ft)
Q1 =	<input type="text" value="77"/>	S1 =	<input type="text" value="106.7"/>
Q2 =	<input type="text" value="131"/>	S2 =	<input type="text" value="107.4"/>
Q3 =	<input type="text" value="100.43"/>	S3 =	<input "="" type="text" value="?"/>

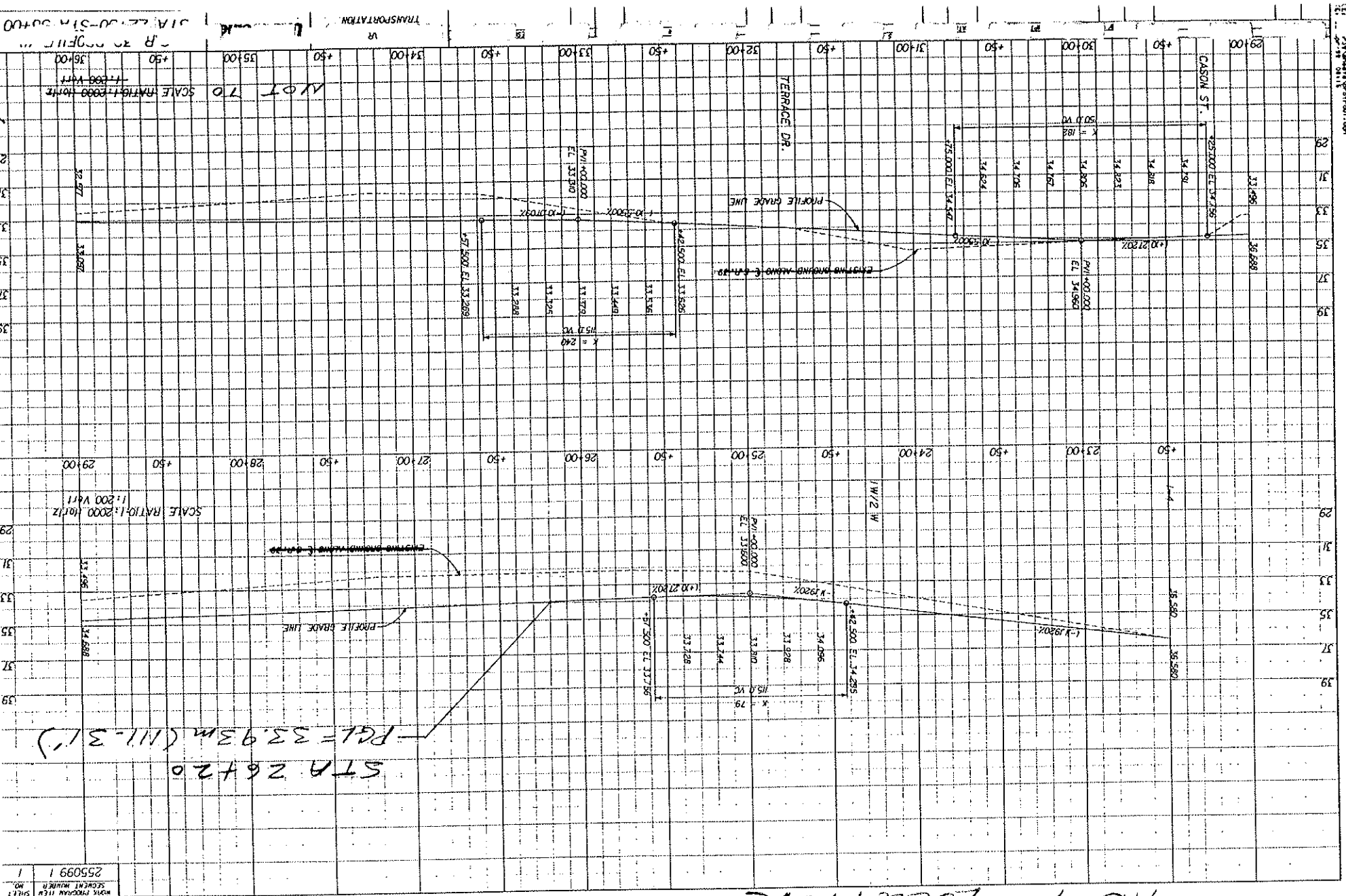
$$S_3 = S_1 + ((S_2 - S_1) \times (Q_3 - Q_1)) / (Q_2 - Q_1) = \text{input } 107.0$$

The peak stage for the year event =

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 4 PROJ. NO. C100003240.19
DESCRIPTION: II.B. CULVERT LOCATION COMPUTED BY: Zinner DATE: 5-27-99
AND CROSS SECTION CHECKED BY: Pratt DATE: 5-28-99

A conceptual vertical profile was developed for this PD&E. See the enclosed portion of the vertical profile and where AB-1 will be located. Also enclosed is a sketch of a half cross section of the proposed cross drain AB-1.

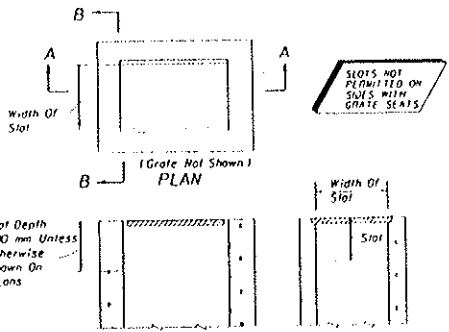


AB-1 Location

STA 26+20
 PGL = 33.93m (111.31')

SCALE RATIO: 1:2000 Horiz
 1:200 Vert

NOT TO SCALE HORIZ: 1:2000 HORIZ
 1:200 VERT



SECTION AA SECTION BB

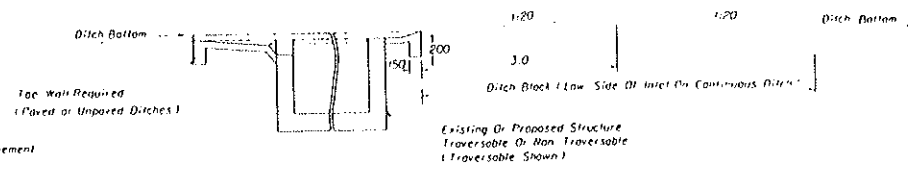
NOTE: See Index No. 229 For Application Guidelines
NON-TRAVERSABLE SLOTS

Inlet	Sod		Inlet	Pavt		Sod
	m ²	m ³		m ²	m ³	
C	5	0.23	C	0.23	7	
D	5	0.28	D	0.28	8	
E	6	0.28	E	0.28	8	
H	7	0.34	H	0.34	9	

PAVT. AND SOD

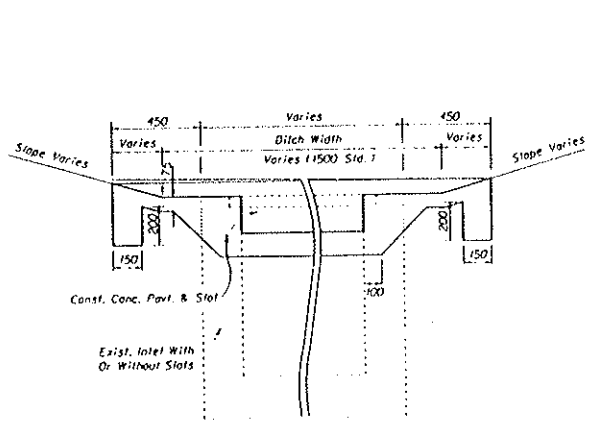
NOTE: See General Notes Nos. 6 and 7

SODDING AND PAVEMENT
FOR INLETS WITHOUT
SLOTS AND INLETS WITH
NON-TRAVERSABLE SLOTS

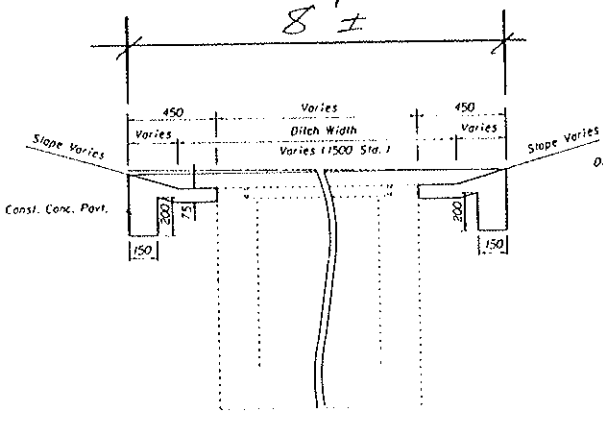


DITCH BLOCK FOR INLETS WITH OR WITHOUT SLOTS

Anticipated DBI to collect off site runoff.



SECTION AA

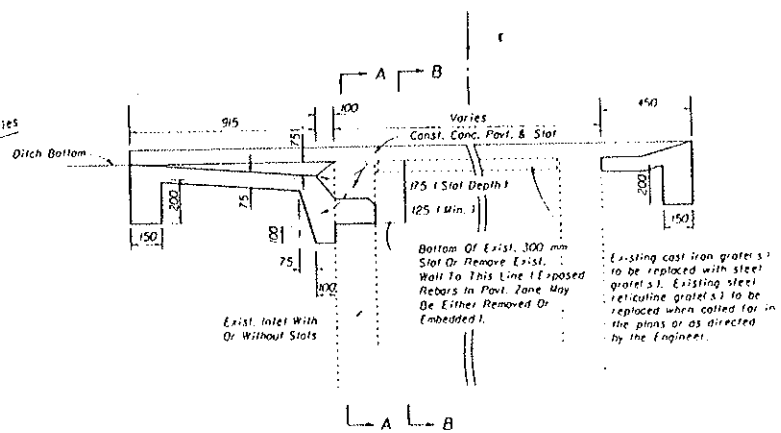


SECTION BB

Inlet	PAVEMENT AND SODDING QUANTITIES FOR TRAVERSABLE SLOTS				Sod	
	Pavement		Sod		Single Slot	Double Slot
	Single Slot	Double Slot	Single Slot	Double Slot		
C	4.07	0.59	5	0.71	10	14
D	5.01	0.70	6	0.84	12	16
E	4.92	0.70	6	0.83	12	15

NOTE: For plan view and additional details see sheet 2 of 4.
For payment see General Notes Nos. 6 and 7.

TRAVERSABLE SLOTS FOR EXISTING INLETS



SINGLE SLOT SHOWN (DOUBLE SLOTS SYMMETRICAL ABOUT CENTERLINE)
SECTION CC (CASE 1)

STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION
ROAD DESIGN

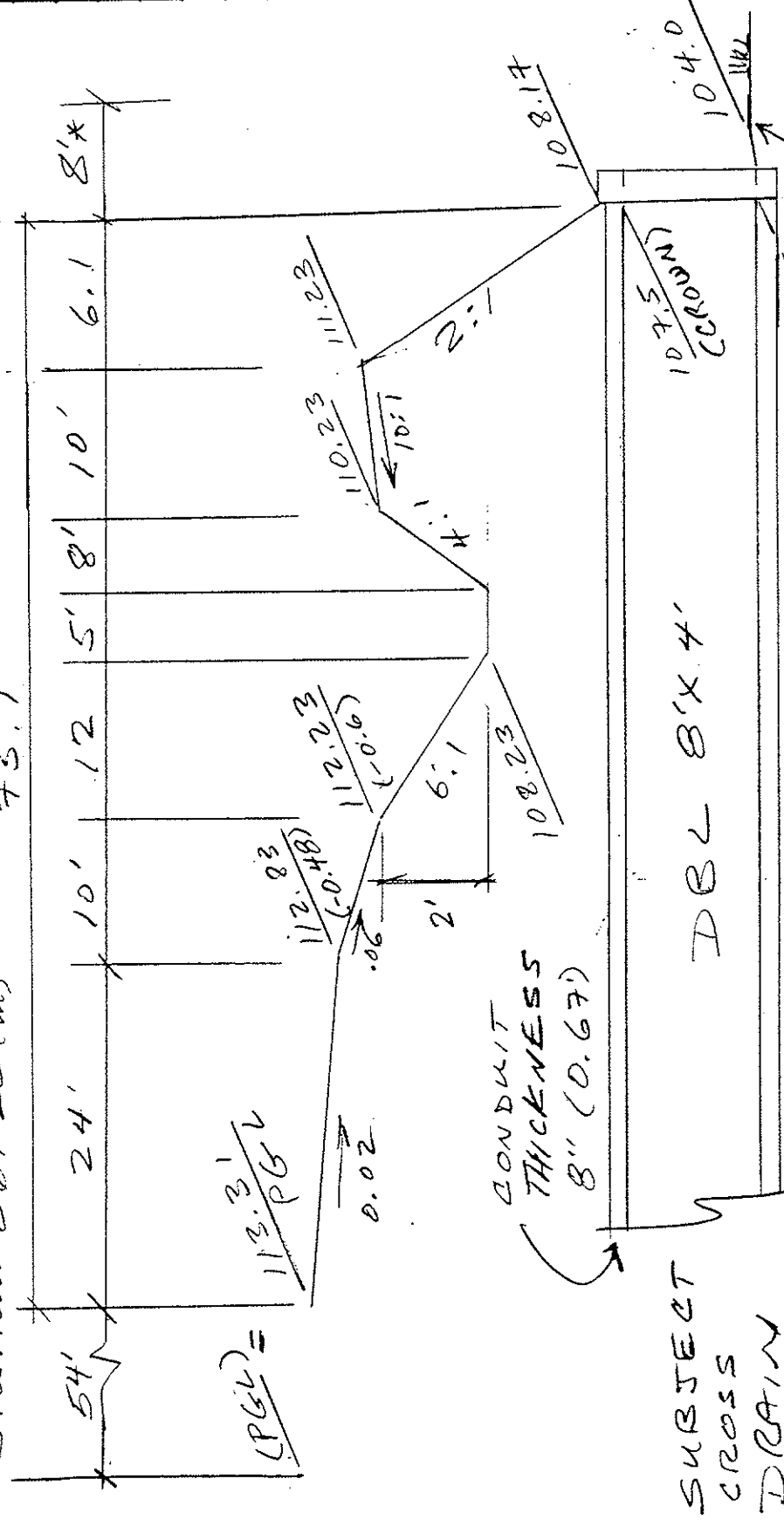
**DITCH BOTTOM INLETS
TYPES C, D, E & H**

DESIGNED BY: JCA	CHECKED BY: JCA	DATE: 07/22	PROJECT NO.:	SHEET NO.:
DRAWN BY: JCA	APPROVED BY: JCA	DATE: 07/22	PROJECT NO.:	SHEET NO.:
<p style="text-align: right;"><i>J.A. McGraw</i></p>			PROJECT NO.:	SHEET NO.:
<p style="text-align: right;">T. H. W. S. 2010-01-01-01</p>			PROJECT NO.:	SHEET NO.:

232

7/1/06

AB-1: Total Length = 54' + 2 x (75.1) + 8' = 212.1
 Station: 26+20 (m) 75.1
 USE 215'



* 8' FOR DBI WITH TRAVERSABLE SLOTS TO ACCEPT OFFSITE FLOWS ON UPSTREAM END OF CROSS DRAIN ONLY.

Not to Scale

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 7 PROJ. NO. C100003240.19
DESCRIPTION: II.C. 50-YEAR AND 100- COMPUTED BY: Zinner DATE: 5-27-99
YEAR CULVERT CAPACITY ANALYSES CHECKED BY: Pratt DATE: 5-28-99

The capacity of the proposed culvert AB-1 was analyzed for the 50- and 100-year storm events using HY-8, software based on the techniques provided in FHWA Hydraulic Design Series # 5. See the enclosed HY-8 output for the analyses.

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 7 PROJ. NO. C100003240.19
DESCRIPTION: I.I.C. 50-YEAR AND 100- COMPUTED BY: Zinner DATE: 6-9-99
YEAR CULVERT CAPACITY ANALYSES CHECKED BY: _____ DATE: _____

The capacity of the proposed culvert AB-1 was analyzed for the 50- and 100-year storm events using HY-8, software based on the techniques provided in FHWA Hydraulic Design Series # 5. See the enclosed HY-8 output for the analyses.

2/7

CURRENT DATE: 06-03-1999
CURRENT TIME: 14:49:59

FILE DATE: 06-03-1999
FILE NAME: AB1_50

FHWA CULVERT ANALYSIS
HY-8, VERSION 6.0

C U L V E R T N O. 1 2 3 4 5 6	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	103.50	102.50	215.00	2 RCB	8.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs)

FILE: AB1_50

DATE: 06-03-1999

50
YR

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.07	101.0	101.0	0.0	0.0	0.0	0.0	0.0	0.00	1
111.31	691.3	691.3	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS

FILE: AB1_50

DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00
107.07	0.000	101.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

3/7

CURRENT DATE: 06-03-1999
CURRENT TIME: 14:49:59

FILE DATE: 06-03-1999
FILE NAME: AB1_50

PERFORMANCE CURVE FOR CULVERT 1 - 2(8.00 (ft) BY 4.00 (ft)) RCB

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00
101.00	107.07	1.84	3.57	1-S1f	0.90	1.08	4.00	4.50	1.58	0.00

El. inlet face invert	103.50 ft	El. outlet invert	102.50 ft
El. inlet throat invert	0.00 ft	El. inlet crest	0.00 ft

***** SITE DATA ***** EMBANKMENT TOE *****

UPSTREAM STATION	0.00 ft
UPSTREAM ELEVATION	103.50 ft
UPSTREAM EMBANKMENT SLOPE (X:1)	0.00
DOWNSTREAM STATION	215.00 ft
DOWNSTREAM ELEVATION	102.50 ft
DOWNSTREAM EMBANKMENT SLOPE (X:1)	0.00

***** CULVERT DATA SUMMARY *****

BARREL SHAPE	BOX
BARREL SPAN	8.00 ft
BARREL RISE	4.00 ft
BARREL MATERIAL	CONCRETE
BARREL MANNING'S n	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE (90-45 DEG.)
INLET DEPRESSION	NONE

4/7

3

CURRENT DATE: 06-03-1999
CURRENT TIME: 14:49:59

FILE DATE: 06-03-1999
FILE NAME: AB1_50

TAILWATER

CONSTANT WATER SURFACE ELEVATION
107.00

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	192.00 ft
CREST LENGTH	1600.00 ft
OVERTOPPING CREST ELEVATION	111.31 ft

5/7

CURRENT DATE: 06-03-1999
 CURRENT TIME: 15:14:26

FILE DATE: 06-03-1999
 FILE NAME: AB1_100

FHWA CULVERT ANALYSIS
 HY-8, VERSION 6.0

C U L V E R T N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	103.50	102.50	215.00	2 RCB	8.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: AB1_100 DATE: 06-03-1999

100
4R

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.53	131.0	131.0	0.0	0.0	0.0	0.0	0.0	0.00	1
111.31	691.3	691.3	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: AB1_100 DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00
107.53	0.000	131.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

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CURRENT DATE: 06-03-1999
 CURRENT TIME: 15:14:26

FILE DATE: 06-03-1999
 FILE NAME: AB1_100

PERFORMANCE CURVE FOR CULVERT 1 - 2(8.00 (ft) BY 4.00 (ft)) RCB

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00
131.00	107.53	2.18	4.03	4-FFt	1.07	1.28	4.00	4.90	2.05	0.00

El. inlet face invert 103.50 ft El. outlet invert 102.50 ft
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA ***** EMBANKMENT TOE *****
 UPSTREAM STATION 0.00 ft
 UPSTREAM ELEVATION 103.50 ft
 UPSTREAM EMBANKMENT SLOPE (X:1) 0.00
 DOWNSTREAM STATION 215.00 ft
 DOWNSTREAM ELEVATION 102.50 ft
 DOWNSTREAM EMBANKMENT SLOPE (X:1) 0.00

***** CULVERT DATA SUMMARY *****
 BARREL SHAPE BOX
 BARREL SPAN 8.00 ft
 BARREL RISE 4.00 ft
 BARREL MATERIAL CONCRETE
 BARREL MANNING'S n 0.012
 INLET TYPE CONVENTIONAL
 INLET EDGE AND WALL SQUARE EDGE (90-45 DEG.)
 INLET DEPRESSION NONE

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CURRENT DATE: 06-03-1999
CURRENT TIME: 15:14:26

FILE DATE: 06-03-1999
FILE NAME: AB1_100

TAILWATER

CONSTANT WATER SURFACE ELEVATION
107.40

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	192.00 ft
CREST LENGTH	660.00 ft
OVERTOPPING CREST ELEVATION	111.31 ft

III. PROPOSED CULVERT AB-2

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 5 PROJ. NO. C100003240.19
DESCRIPTION: III. A. DISCHARGE RATES COMPUTED BY: Zinner DATE: 5-27-99
AND TAILWATER ELEVATIONS CHECKED BY: Pratt DATE: 5-28-99

Available discharge rates for culvert AB-2 were taken from the CDM report mentioned in the previous AB-1 analysis. The basin where the proposed cross drain AB-2 will be located is in node number 6037 of the CDM model. See the maps from the CDM report in the previous analysis. The discharge rates for the 25 year and the 100 year were taken from the following HEC-1 outputs (partials) and the 50 year discharge rate was interpolated from them. The peak discharge rates are as follows:

<u>Event (year)</u>	<u>Discharge Rate (cfs)</u>	<u>Source</u>
50	120	interpolation
100	157	CDM report

The peak stage for the 50-year event was interpolated from the stages obtained from peak stages in Table 4-1 from the CDM report (see attached). For the proposed cross drain AB-2 capacity analysis, the existing conditions tailwater and headwater was assumed to be the same as the peak stage within node number 6037. See the enclosed interpolations for the 50 year peak stage. The existing peak stages are as follows:

<u>Event (year)</u>	<u>Peak Stage (ft. NGVD)</u>	<u>Source</u>
50	107.9	interpolation
100	108.0	CDM report

2/5

2 COMBINED AT	9999	0.06	1	FLOW TIME	34. 13.10
HYDROGRAPH AT	6020	0.18	1	FLOW TIME	78. 13.35
2 COMBINED AT	9999	0.24	1	FLOW TIME	109. 13.20
HYDROGRAPH AT	6025	0.11	1	FLOW TIME	48. 13.40
2 COMBINED AT	9999	0.35	1	FLOW TIME	156. 13.25
HYDROGRAPH AT	6030	0.00	1	FLOW TIME	2. 13.00
2 COMBINED AT	9999	0.36	1	FLOW TIME	157. 13.25
HYDROGRAPH AT	6032	0.01	1	FLOW TIME	10. 13.00
2 COMBINED AT	9999	0.37	1	FLOW TIME	165. 13.20
HYDROGRAPH AT	6034	0.03	1	FLOW TIME	18. 13.00
2 COMBINED AT	9999	0.40	1	FLOW TIME	181. 13.15
HYDROGRAPH AT	6030	0.15	1	FLOW TIME	51. 13.40
2 COMBINED AT	9999	0.55	1	FLOW TIME	230. 13.20
HYDROGRAPH AT	6036	0.01	1	FLOW TIME	6. 13.00
2 COMBINED AT	9999	0.56	1	FLOW TIME	235. 13.15
HYDROGRAPH AT	6037	0.23	1	FLOW TIME	92. 13.35
2 COMBINED AT	9999	0.79	1	FLOW TIME	325. 13.25
HYDROGRAPH AT	6040	0.03	1	FLOW TIME	14. 13.35
2 COMBINED AT	9999	0.82	1	FLOW TIME	339. 13.25
HYDROGRAPH AT	6050	0.16	1	FLOW TIME	46. 13.60
2 COMBINED AT	9999	0.98	1	FLOW TIME	382. 13.30
HYDROGRAPH AT	6060	0.11	1	FLOW TIME	32. 13.50
2 COMBINED AT	9999	1.09	1	FLOW TIME	414. 13.35
HYDROGRAPH AT	6061	0.05	1	FLOW TIME	33. 13.00

flow from 6035

92.45M = Q25

3/5

IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 601 LAST ORDINATE PUNCHED OR SAVED
 TIMINT 0.050 TIME INTERVAL IN HOURS

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				FLOW	TIME
				RATIO 1	10.50
HYDROGRAPH AT	6005	0.02	1	14.	13.05
2 COMBINED AT	9999	0.04	1	34.	13.05
HYDROGRAPH AT	6005	0.03	1	23.	13.15
2 COMBINED AT	9999	0.06	1	57.	13.05
HYDROGRAPH AT	6020	0.18	1	131.	13.35
2 COMBINED AT	9999	0.24	1	184.	13.15
HYDROGRAPH AT	6025	0.11	1	82.	13.35
2 COMBINED AT	9999	0.35	1	264.	13.20
HYDROGRAPH AT	6030	0.00	1	3.	13.00
2 COMBINED AT	9999	0.36	1	267.	13.20
HYDROGRAPH AT	6032	0.01	1	15.	13.00
2 COMBINED AT	9999	0.37	1	281.	13.15
HYDROGRAPH AT	6034	0.03	1	29.	13.00
2 COMBINED AT	9999	0.40	1	308.	13.10
HYDROGRAPH AT	6030	0.15	1	91.	13.35
2 COMBINED AT	9999	0.55	1	395.	13.15
HYDROGRAPH AT	6036	0.01	1	10.	13.00
2 COMBINED AT	9999	0.56	1	404.	13.15
HYDROGRAPH AT	6037	0.23	1	157.	

flow from 6035

6037

157. = Q₁₀₀

TABLE 4-1

City of Plant City
 Westside Canal Stormwater Management Master Plan
 Summary of Peak Flood Stages for Design Storms and Problem Areas

Model Node	Location	Top of Road (ft-NGVD)	10-yr/24-hr		25-yr/24-hr		100-yr/24-hr		Problem ID Number
			Peak Stage (ft-NGVD)	Depth of Flooding (ft)	Peak Stage (ft-NGVD)	Depth of Flooding (ft)	Peak Stage (ft-NGVD)	Depth of Flooding (ft)	
6176	Wheeler Street (SR 39)	123.5	122.4		123.1		123.9	0.4	
6178	SR 39 storm sewer (Collins St.)	138.5	129.7		130.2		137.8		
6180	Ball Street	121.0	121.3	0.3	121.3	0.3	121.8	0.8	P-7
6182			121.3		121.4		121.8		
6190			121.4		121.4		121.8		
6196			123.3		123.3		123.6		
6198	Grant Street	128.6	128.9	0.3	129.0	0.4	129.2	0.6	
6200			129.1		129.2		129.5		
6201	Dirt Path	132.6	128.4		128.6		129.0		
6202			128.5		128.6		129.1		
6203	Strawberry Lane	133.9	128.8		128.9		129.5		
6204			128.9		129.0		129.5		
6205	W. Prosser Drive	133.7	130.2		130.5		131.9		
6210			130.3		130.6		131.9		
6220	Essex Drive	132.5	131.0		131.5		132.8	0.3	
6230			131.1		131.5		132.8		
6250	Warren Street storm sewer	121.0	121.4	0.3	121.6	0.6	122.1	1.1	P-5
6251			121.4		121.6		122.1		
6252			121.4		121.6		122.1		
6253			121.4		121.6		122.1		
6254	N. side of Evers St. Kash-N-Karry	122.6	121.4		121.6		122.5		
6255			121.4		121.6		122.5		
6260			121.4		121.6		122.1		
6261		121.4	121.4	0.0	121.6	0.2	122.1	0.7	
6262	CSX Railroad	127.5	121.4		121.6		122.2		
6270			122.4		122.5		123.3		
6271	Ball Street storm sewer	126.9	123.6		124.1		125.8		
6275	Alsobrook Street storm sewer	121.5	121.1		121.2		121.7	0.2	
6280	Hunter Street storm sewer	119.9	121.1	1.2	121.3	1.4	121.7	1.8	P-7
6282	Hunter Street storm sewer	120.3	121.2	0.9	121.3	1.0	121.8	1.5	P-7
6290	Alexander Street storm sewer	120.0	117.0		117.5		118.0		
6291	Alexander Street	120.0	117.1		117.5		118.0		
6292			117.1		117.6		118.0		
6303			105.0		105.1		105.7		
6304			103.6		103.9		105.2		
6305			105.0		105.1		105.7		
6306			107.0		107.1		107.4		
6307			107.9		107.9		108.0		
6308			107.6		107.6		107.7		

Note: Level of service is 0.5 ft of road flooding for the 25-yr/24-hr storm and 0.75 ft of road flooding for the 100-yr/24-hr storm.

4/5

HW stage utilized

URS Greiner

JOB: SR 39 ALEXANDER ROAD BYPASS	SHEET <u>5</u> of <u>5</u>	PROJ. NO. C100003240.19
DESCRIPTION: AB-2 50-yr Q, HW, & TW	COMPUTED BY Jim Zinner	DATE 05-25-99
	CHECKED BY <u>JWZ</u>	DATE <u>5-28-99</u>

Input/Output Boxes Explanation

= manually input values

= unknown, previously input, or computed output values

Frequency versus Discharge Log-slope Interpolation

when: $f_3 > f_1$ & $f_3 < f_2$

	frequency (yrs)		discharge (cfs)
f1 =	<input type="text" value="25"/>	Q1 =	<input type="text" value="92"/>
f2 =	<input type="text" value="100"/>	Q2 =	<input type="text" value="157"/>
f3 =	<input type="text" value="50"/>	Q3 =	<input "="" type="text" value="?"/>

$$M = \log(Q_2) - \log(Q_1) / \log(f_2) - \log(f_1) = \text{[2.5938]}$$

$$Q_3 = 10^{[(\log(Q_2) - \log(Q_1)) / M + \log(f_1)]} = \text{[120]}$$

The peak discharge for the year event =

Discharge versus Stage Linear Interpolation

	discharge (cfs)		stage (ft)
Q1 =	<input type="text" value="92"/>	S1 =	<input type="text" value="107.9"/>
Q2 =	<input type="text" value="157"/>	S2 =	<input type="text" value="108"/>
Q3 =	<input type="text" value="120.18"/>	S3 =	<input "="" type="text" value="?"/>

$$S_3 = S_1 + ((S_2 - S_1) \times (Q_3 - Q_1)) / (Q_2 - Q_1) = \text{[107.9]}$$

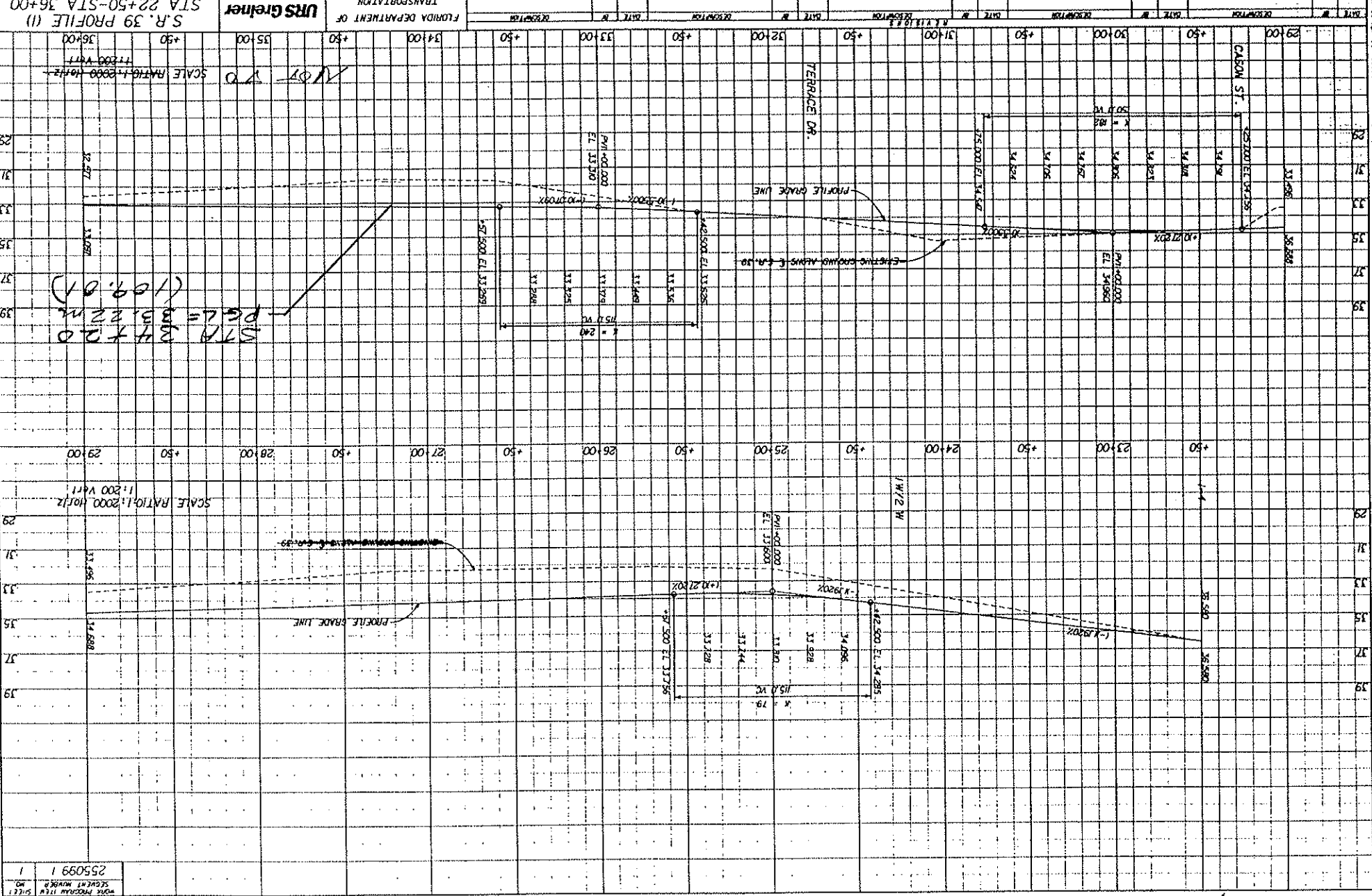
The peak stage for the year event =

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 3 PROJ. NO. C100003240.19
DESCRIPTION: III.B. CULVERT LOCATION COMPUTED BY: Zinner DATE: 5-27-99
AND CROSS SECTION CHECKED BY: Pratt DATE: 5-28-99

A conceptual vertical profile was developed for this PD&E. See the enclosed portion of the vertical profile and where AB-2 will be located. Also enclosed is a sketch of a half cross section of the proposed cross drain AB-2.

DATE: 11/11/10
 TIME: 10:00 AM
 DRAWN BY: J. B. BROWN



AB-2 Location

WORK PROGRAM 117W
 SHEET NO. 255099 1

DATE	DESCRIPTION	DATE	DESCRIPTION	DATE	DESCRIPTION	DATE	DESCRIPTION
11/11/10	11/11/10	11/11/10	11/11/10	11/11/10	11/11/10	11/11/10	11/11/10

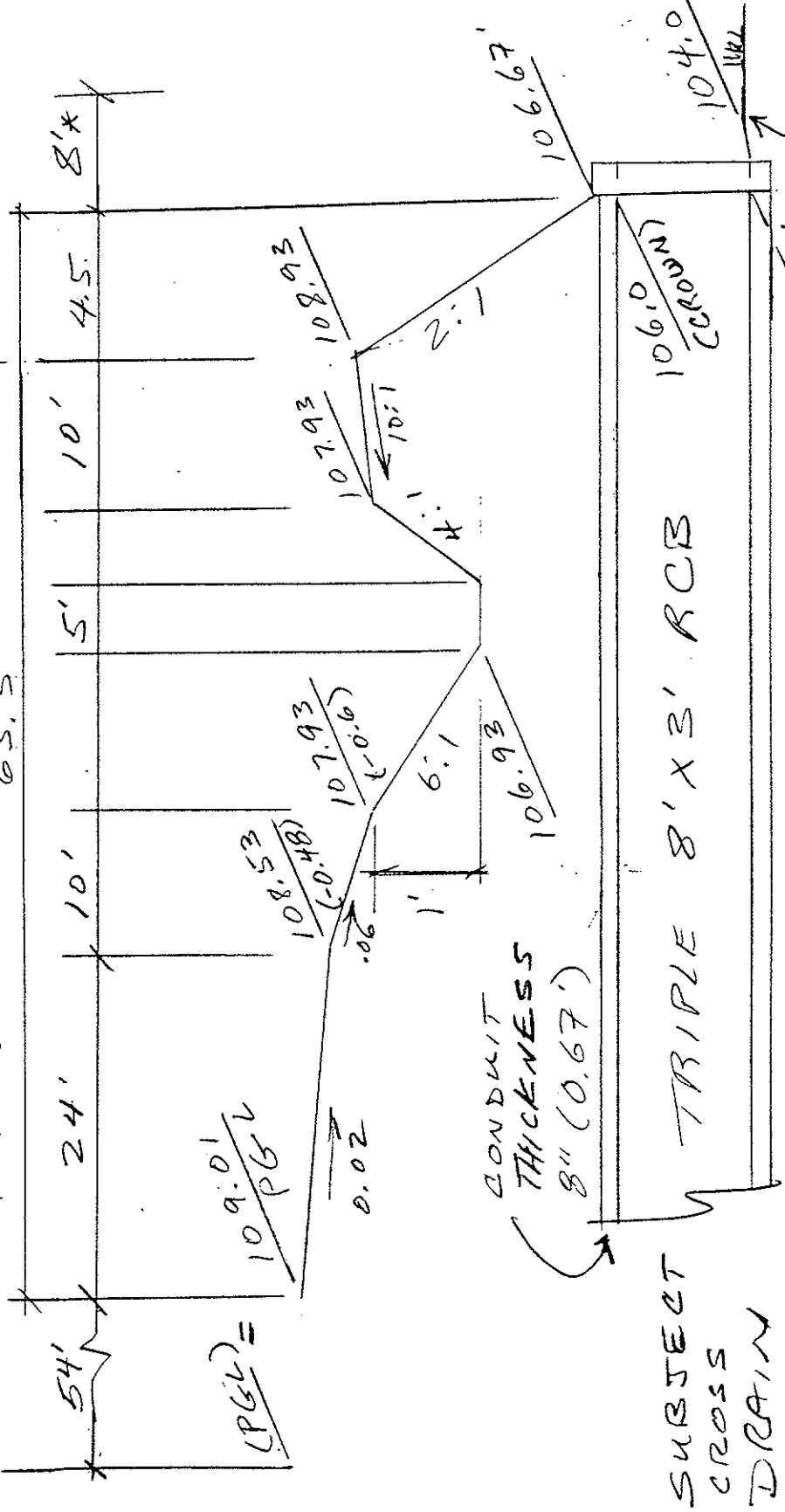
FLORIDA DEPARTMENT OF TRANSPORTATION
 URS Greiner

S.R. 39 PROFILE (I)
 STA 22+50-STA 36+00

JOB Alex. St. Bypass / SR 39
 DESCRIPTION AB-1 Length Calc.

SHEET 3 OF 3 PROJ. NO. C100003240.91
 COMPUTED BY Zimmer DATE 6-4-99
 CHECKED BY _____ DATE _____

AB-2 : Total Length = 54' + 2 x (63.5) + 78' = 189.0
 Station: 34 + 20 m
 63.5



103.0 ELEV. 4/5 #

* 8' FOR DBI WITH TRAVELABLE SLOTS TO ACCEPT OFFSITE FLOWS ON UPST REAK END OF CROSS DRAIN ONLY.

1/2" TO CORNER

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 7 PROJ. NO. C100003240.19
DESCRIPTION: III.C. 50-YEAR AND 100- COMPUTED BY: Zinner DATE: 5-27-99
YEAR CULVERT CAPACITY ANALYSES CHECKED BY: Pratt DATE: 5-28-99

The capacity of the proposed culvert AB-2 was analyzed for the 50- and 100-year storm events using HY-8, software based on the techniques provided in FHWA Hydraulic Design Series # 5. See the enclosed HY-8 output for the analyses.

CURRENT DATE: 06-08-1999
 CURRENT TIME: 09:28:14

FILE DATE: 06-08-1999
 FILE NAME: AB2_50

FHWA CULVERT ANALYSIS
 HY-8, VERSION 6.0

C U L V E R T N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	103.00	102.00	190.00	3 RCB	8.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: AB2_50 DATE: 06-08-1999

50 -
4R

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
107.99	120.2	120.2	0.0	0.0	0.0	0.0	0.0	0.00	1
109.01	410.8	410.8	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: AB2_50 DATE: 06-08-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00
107.99	0.000	120.20	0.00	0.00

<1> TOLERANCE (ft) = 0.010 <2> TOLERANCE (%) = 1.000

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CURRENT DATE: 06-08-1999
CURRENT TIME: 09:28:14

FILE DATE: 06-08-1999
FILE NAME: AB2_50

TAILWATER

CONSTANT WATER SURFACE ELEVATION
107.90

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	172.00 ft
CREST LENGTH	2300.00 ft
OVERTOPPING CREST ELEVATION	109.01 ft

5/7

CURRENT DATE: 06-03-1999
CURRENT TIME: 15:13:56

FILE DATE: 06-03-1999
FILE NAME: AB2_100

FHWA CULVERT ANALYSIS
HY-8, VERSION 6.0

C U L V N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	103.00	102.00	190.00	3 RCB	8.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: AB2_100 DATE: 06-03-1999

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
108.16	157.0	157.0	0.0	0.0	0.0	0.0	0.0	0.00	1
109.01	392.1	392.1	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: AB2_100 DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00
108.16	0.000	157.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

6/7

CURRENT DATE: 06-03-1999
CURRENT TIME: 15:13:56

FILE DATE: 06-03-1999
FILE NAME: AB2_100

PERFORMANCE CURVE FOR CULVERT 1 - 3(8.00 (ft) BY 3.00 (ft)) RCB

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00
157.00	108.16	1.87	5.16	4-FFt	0.89	1.10	3.00	6.00	2.18	0.00

El. inlet face invert	103.00 ft	El. outlet invert	102.00 ft
El. inlet throat invert	0.00 ft	El. inlet crest	0.00 ft

***** SITE DATA ***** EMBANKMENT TOE *****

UPSTREAM STATION	0.00 ft
UPSTREAM ELEVATION	103.00 ft
UPSTREAM EMBANKMENT SLOPE (X:1)	0.00
DOWNSTREAM STATION	190.00 ft
DOWNSTREAM ELEVATION	102.00 ft
DOWNSTREAM EMBANKMENT SLOPE (X:1)	0.00

***** CULVERT DATA SUMMARY *****

BARREL SHAPE	BOX
BARREL SPAN	8.00 ft
BARREL RISE	3.00 ft
BARREL MATERIAL	CONCRETE
BARREL MANNING'S n	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE (90-45 DEG.)
INLET DEPRESSION	NONE

7/7

CURRENT DATE: 06-03-1999
CURRENT TIME: 15:13:56

FILE DATE: 06-03-1999
FILE NAME: AB2_100

TAILWATER

CONSTANT WATER SURFACE ELEVATION
108.00

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	172.00 ft
CREST LENGTH	2300.00 ft
OVERTOPPING CREST ELEVATION	109.01 ft

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET / OF / PROJ. NO. C100003240.19
DESCRIPTION: III.D. RESULTS COMPUTED BY: Zinner DATE: 5-27-99
CHECKED BY: Pratt DATE: 5-28-99

The cross drain which satisfies the 0.1' rise for the 50-year storm event is a triple 8'x3' reinforced concrete box culvert (RCB).

The results of the HY-8 analyses for the proposed culvert AB-2 are shown below:

<u>Event (year)</u>	<u>Existing Headwater Elevation feet (NGVD)</u>	<u>Proposed Headwater Elevation feet (NGVD)</u>
50	107.90	107.99
100	108.00	108.16

IV. PROPOSED CULVERT AB-3

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 3 PROJ. NO. C100003240.19
DESCRIPTION: IV.A. DISCHARGE RATES COMPUTED BY: Zinner DATE: 5-27-99
AND TAILWATER ELEVATIONS CHECKED BY: Pratt DATE: 5-28-99

Discharge rates for culvert AB-3 were calculated using the Rational method. See the enclosed calculations for the peak discharge rates and they are as follows:

<u>Event (year)</u>	<u>Discharge Rate (cfs)</u>	<u>Source</u>
50	8	Rational method
100	9	Rational method

The elevation of the crown of the proposed cross drain and the seasonal high water table (SHWT) elevation was compared and the higher stage was used for the proposed AB-3 capacity analyses. In this case the SHWT elevation was used. The nearest field verified SHWT elevation was located at the station 48+00 and the SHWT elevation is 100.50 NGVD.

URS Greiner

JOB: SR 39 ALEXANDER ROAD BYPASS	SHEET 2 of 3	PROJ. NO. C100003240.19
DESCRIPTION: Rational C & Q calc.s	COMPUTED BY Jim Zinner	DATE 05-26-99
Drainage Area AB-3	CHECKED BY	DATE

Input/Output = manually input values
 Boxes
 Explanation = unknown, previously input, or computed output values

Drainage Area = ac

Land Use	Area (ac)	C	C x A (ac)
Pavement	0.85	0.95	0.8
Industrial / Commercial	0	0.95	0.0
Pasture, grass, farmlands	18.75	0.2	3.8
Woodlands	0	0.25	0.0
Total =			19.6
			4.56

C coefficients assumed for sandy soils and flat (0-2%) slopes

composite C = (C x A) / Area = 4.56 / 19.6 =

TOC = mins = hours (see following worksheet)

Intensities from FDOT Zone IDF Curve

frequency = year

Intensity in / hour

Q = CIA = * * = cfs

frequency = year

Intensity in / hour

Q = CIA = * * = cfs

Project: S.R. 39 Alexander Street Bypass
 Subject: Time of Concentration Calculations Proposed Conditions
 Project No.: C100003240.19

Sheet of
 Computed By: JYZ Date: 04-07-99
 Checked By: RWP Date: 5-28-99

Basin #	Sheet Flow						Shallow Concentrated Flow					Channel Flow							Total Time Tc (min)	Total Time Tc (hr)				
	Surface Type	Mannings Coeff. n	Flow Length <=300 ft. L (ft)	2yr-24hr Rainfall P2 (in)	Land Slope s (ft/ft)	Time T1 (min)	Surface Type	Flow Length L (ft)	Water Course Slope s (ft/ft)	Avg. Vel. V (ft/s)	Time T2 (min)	Cross Sectional Flow Area a (ft^2)	Wetted Perimeter Pw (ft)	Hydraulic Radius r = a/Pw (ft)	Channel Slope s (ft/ft)	Mannings Roughness Coeff. n	Vel. V (ft/s)	Flow Length L (ft)			Time T3 (min)			
AB3	Cultivat. >20% cover	0.17	300	4.0	0.006	37.8	unpavd	900	0.014	1.4	10.7													
		Total					37.8	Total					10.7	Total							0	48	0.81	
AB4	Cultivat. >20% cover	0.17	300	4.0	0.028	20.4	unpavd	1000	0.008	1.4	11.9	18.000	21.300	0.845	0.0004	0.1	0.266	2700	169					
		Total					20.4	Total					11.9	310.000	320.100	0.968	0.0046	0.1	0.989	650	11	Total		180
AB5	Pasture, grass, farmland	0.17	300	4.0	0.004	44.4	unpavd	700	0.004	1.4	8.3													
		Total					44.4	Total					8.3	Total							0	53	0.88	

- NOTES: (1) Sheet Flow Mannings Roughness Coefficient obtained from Table 3-1 Roughness Coefficients for Sheet Flow, Urban Hydrology for Small Watersheds, TR55 Manual
 (2) Maximum hydraulic length for sheet Flow is 300 ft. (TR 55 Manual)
 (3) Maximum hydraulic length for shallow concentrated flow is 1000 ft.
 (4) 2yr-24hr rainfall amount (P2) was obtained from SWFWMD 2yr-24hr return period rainfall map
 (5) Average Velocity for Paved Surface = 20.3282(s)^0.5 (See Appendix F TR55 Manual)
 (6) Average Velocity for Unpaved Surface = 16.1345(s)^0.5 (See Appendix F TR55 Manual)

5/3

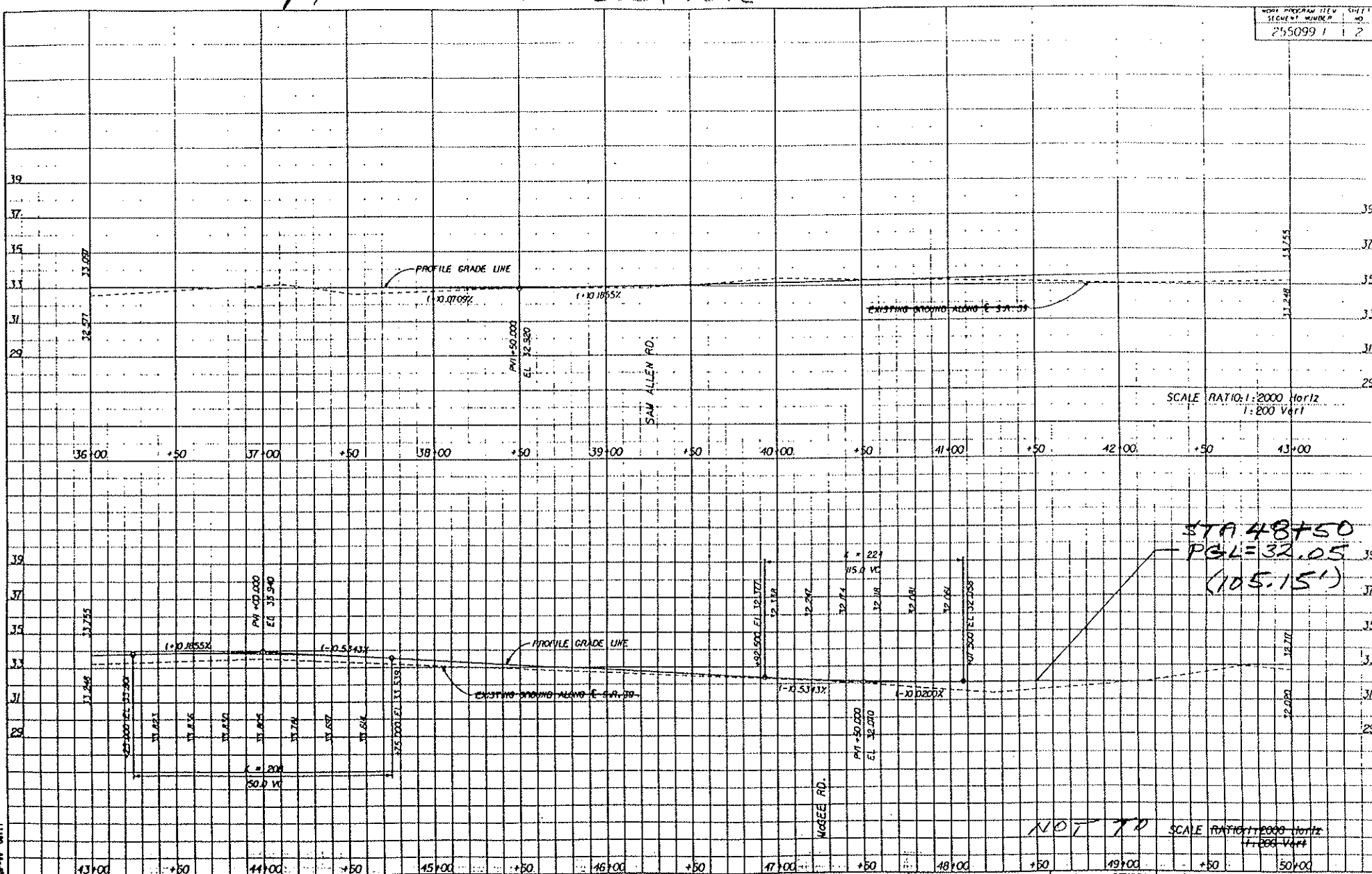
URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 3 PROJ. NO. C100003240.19
DESCRIPTION: IV.B. CULVERT LOCATION COMPUTED BY: Zinner DATE: 5-27-99
AND CROSS SECTION CHECKED BY: Pratt DATE: 5-28-99

A conceptual vertical profile was developed for this PD&E. See the enclosed portion of the vertical profile and where AB-3 will be located. Also enclosed is a sketch of a half cross section of the proposed cross drain AB-3.

AL-3 Location

WORK PROGRAM ITEM SHEET NO. 255099 1 1 2



SCALE RATIO: 1:2000 Horiz
1:800 Vert

NOT TO SCALE RATIO: 1:2000 Horiz
1:800 Vert

DATE	DESCRIPTION	DATE	DESCRIPTION	DATE	DESCRIPTION	DATE	DESCRIPTION

FLORIDA DEPARTMENT OF TRANSPORTATION

URS Greiner

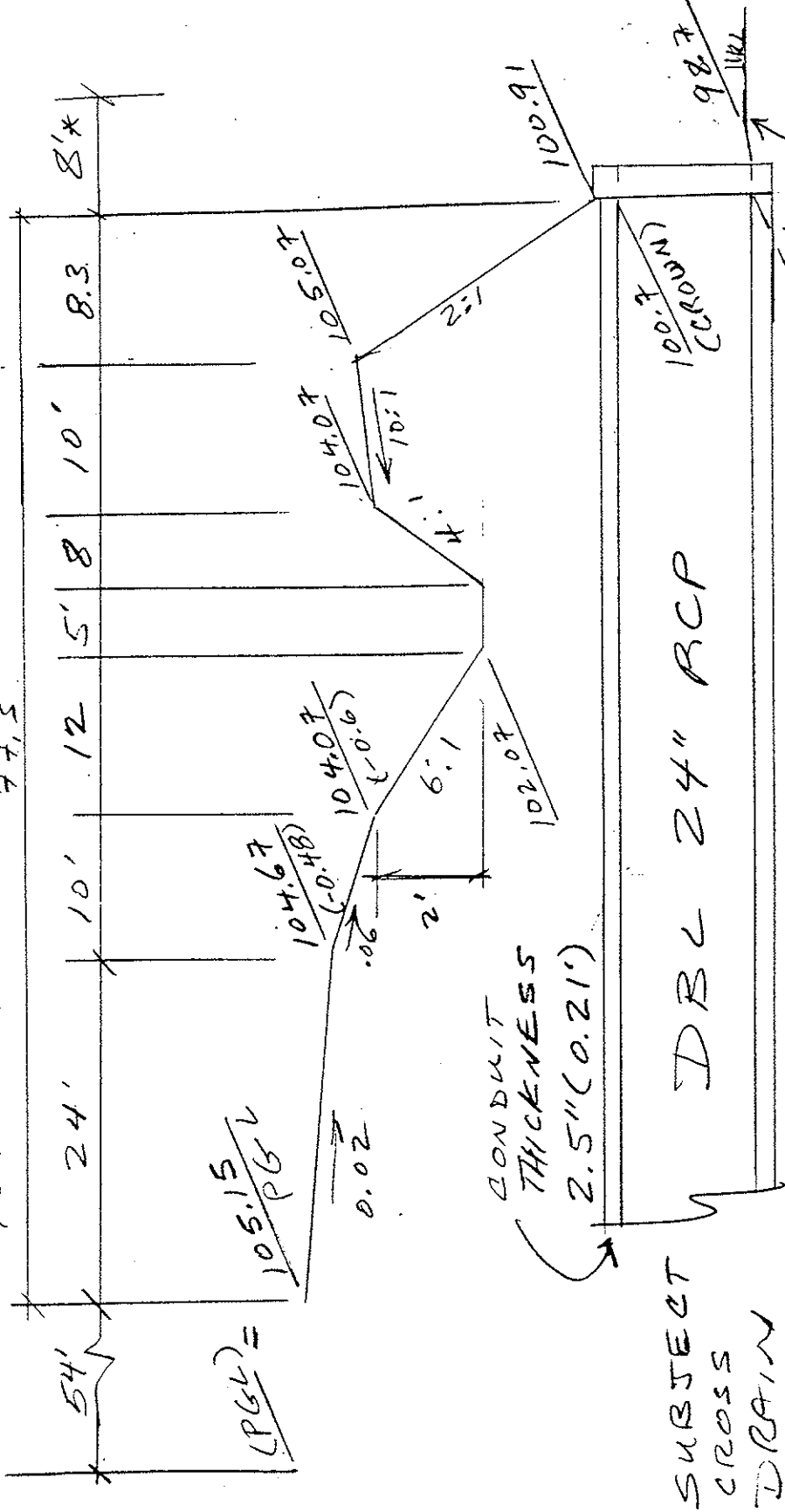
S-R: 39 PROFILE (2)
STA 36+00 - STA 50+00

URS Greiner

JOB Alex. St Bypass / SR 39
 DESCRIPTION AB-3 Length Calc.

SHEET 3 OF 3 PROJ. NO. 000003240.14
 COMPUTED BY Zinner DATE 6-4-99
 CHECKED BY _____ DATE _____

AB-3: Total Length = 54' + 2 x (77.3) + 8' = 216.6
 Station: 48+50cm USC 218



* 8' FOR DBI WITH TRAVELABLE SLOTS TO ACCEPT OFFSITE FLOWS ON UPSTREAM END OF CROSS DRAIN ONLY.

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 7 OF 4 PROJ. NO. C100003240.19
DESCRIPTION: IV.C. 50-YEAR AND 100- COMPUTED BY: Zinner DATE: 5-27-99
YEAR CULVERT CAPACITY ANALYSES CHECKED BY: Pratt DATE: 5-28-99

The capacity of the proposed culvert the proposed culvert AB-3 was analyzed for the 50-year and 100-year storm events using HY-8, software based on the techniques provided in FHWA Hydraulic Design Series # 5. See the enclosed HY-8 output for the analyses.

2/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 17:45:14

FILE DATE: 06-03-1999
FILE NAME: AB3_LC

FHWA CULVERT ANALYSIS
HY-8, VERSION 6.0

C U L V E R T N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	98.70	96.70	218.01	2 RCP	24.00	24.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: AB3_LC DATE: 06-03-1999

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
50 YR -100.60	8.0	8.0	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.1	8.1	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.2	8.2	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.3	8.3	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.4	8.4	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.5	8.5	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.6	8.6	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.7	8.7	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.8	8.8	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	8.9	8.9	0.0	0.0	0.0	0.0	0.0	0.00	1
100.60	9.0	9.0	0.0	0.0	0.0	0.0	0.0	0.00	1
100 YR 105.15	120.8	120.8	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: AB3_LC DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
100.60	0.000	8.00	0.00	0.00
100.60	0.000	8.10	0.00	0.00
100.60	0.000	8.20	0.00	0.00
100.60	0.000	8.30	0.00	0.00
100.60	0.000	8.40	0.00	0.00
100.60	0.000	8.50	0.00	0.00
100.60	0.000	8.60	0.00	0.00
100.60	0.000	8.70	0.00	0.00
100.60	0.000	8.80	0.00	0.00
100.60	0.000	8.90	0.00	0.00
100.60	0.000	9.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010 <2> TOLERANCE (%) = 1.000

3/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 17:45:14

FILE DATE: 06-03-1999
FILE NAME: AB3_LC

PERFORMANCE CURVE FOR CULVERT 1 - 2(24.00 (ft) BY 24.00 (ft)) RCP

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
8.00	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.08	0.00
8.10	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.20	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.30	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.40	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.50	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.60	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.70	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.80	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
8.90	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00
9.00	100.60	1.44	1.90	3-M1t	0.03	0.06	3.80	3.80	0.09	0.00

El. inlet face invert	98.70 ft	El. outlet invert	96.70 ft
El. inlet throat invert	0.00 ft	El. inlet crest	0.00 ft

***** SITE DATA ***** CULVERT INVERT *****

INLET STATION	0.00 ft
INLET ELEVATION	98.70 ft
OUTLET STATION	218.00 ft
OUTLET ELEVATION	96.70 ft
NUMBER OF BARRELS	2
SLOPE (V/H)	0.0092
CULVERT LENGTH ALONG SLOPE	218.01 ft

***** CULVERT DATA SUMMARY *****

BARREL SHAPE	CIRCULAR
BARREL DIAMETER	24.00 ft
BARREL MATERIAL	CONCRETE
BARREL MANNING'S n	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	BEVELED EDGE (1:1)
INLET DEPRESSION	NONE

4/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 17:45:14

FILE DATE: 06-03-1999
FILE NAME: AB3_LC

TAILWATER

CONSTANT WATER SURFACE ELEVATION
100.50

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	192.00 ft
CREST LENGTH	1600.00 ft
OVERTOPPING CREST ELEVATION	105.15 ft

V. PROPOSED CULVERT AB-4

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET / OF 3 PROJ. NO. C100003240.19
DESCRIPTION: V.A. DISCHARGE RATES COMPUTED BY: Zinner DATE: 5-27-99
AND TAILWATER ELEVATIONS CHECKED BY: Pratt DATE: 5-28-99

Discharge rates for culvert AB-4 were calculated using the Rational method. See the enclosed calculations for the peak discharge rates and they are as follows:

<u>Event (year)</u>	<u>Discharge Rate (cfs)</u>	<u>Source</u>
50	84	Rational method
100	93	Rational method

The elevation of the crown of the proposed cross drain and the seasonal high water table (SHWT) elevation was compared, and the higher stage was used for the proposed AB-4 capacity analyses. In this case the SHWT elevation was used. The nearest field verified SHWT elevation was located at the station 55+00 and the SHWT elevation is 103.00 NGVD.

URS Greiner

JOB: SR 39 ALEXANDER ROAD BYPASS	SHEET 2 of 3	PROJ. NO. C100003240.19
DESCRIPTION: Rational C & Q calc.s	COMPUTED BY Jim Zinner	DATE 05-26-99
Drainage Area AB-4	CHECKED BY	DATE

Input/Output = manually input values

Boxes

Explanation = unknown, previously input, or computed output values

Drainage Area = ac

Land Use	Area (ac)	C	C x A (ac)
Pavement	4.3	0.95	4.1
Industrial / Commercial	16.5	0.95	15.7
Pasture, grass, farmlands	123	0.2	24.6
Woodlands	9.2	0.25	2.3
Total =			153
			46.66

C coefficients assumed for sandy soils and flat (0-2%) slopes

composite C = (C x A) / Area = 46.66 / 153 =

TOC = mins = hours (see following worksheet)

Intensities from FDOT Zone IDF Curve

frequency = year

Intensity in / hour

Q = CIA = * * = cfs

frequency = year

Intensity in / hour

Q = CIA = * * = cfs

Project: S.R. 39 Alexander Street Bypass
 Subject: Time of Concentration Calculations Proposed Conditions
 Project No.: C100003240.19

Sheet 2 of 2
 Computed By: JYZ Date: 04-07-99
 Checked By: RWP Date: 5-28-99

Basin #	Sheet Flow						Shallow Concentrated Flow					Channel Flow								Total Time Tc (min)	Total Time Tc (hr)					
	T1 = (0.007*(n*L)^0.8) / (P2^0.5)*(s^0.4) *60min/hr						Avg. Vel (V), Figure 3-1 T2 = (L/V) / 60 sec/min.					V = 1.49 * (r^0.67) * (s^0.5) / n T3 = (L/V) / 60 sec/min.														
	Surface Type	Mannings Coeff. n	Flow Length <=300 ft. L (ft)	2yr-24hr Rainfall P2 (in)	Land Slope s (ft/ft)	Time T1 (min)	Surface Type	Flow Length L (ft)	Water Course Slope s (ft/ft)	Avg. Vel. V (ft/s)	Time T2 (min)	Cross Sectional Flow Area a (ft^2)	Wetted Perimeter Pw (ft)	Hydraulic Radius r = a/Pw (ft)	Channel Slope s (ft/ft)	Mannings Roughness Coeff. n	Vel. V (ft/s)	Flow Length L (ft)	Time T3 (min)							
AB3	Cultivat. >20% cover	0.17	300	4.0	0.006	37.8	unpavd	900	0.014	1.4	10.7															
		Total										37.8	Total					10.7	Total							
AB4	Cultivat. >20% cover	0.17	300	4.0	0.028	20.4	unpavd	1000	0.008	1.4	11.9	18.000	21.300	0.845	0.0004	0.1	0.266	2700	169							
		Total										20.4	Total					11.9	Total							
AB5	Pasture, grass, farmland	0.17	300	4.0	0.004	44.4	unpavd	700	0.004	1.4	8.3															
		Total										44.4	Total					8.3	Total							

- NOTES: (1) Sheet Flow Mannings Roughness Coefficient obtained from Table 3-1 Roughness Coefficients for Sheet Flow, Urban Hydrology for Small Watersheds, TR55 Manual
 (2) Maximum hydraulic length for sheet Flow is 300 ft. (TR 55 Manual)
 (3) Maximum hydraulic length for shallow concentrated flow is 1000 ft.
 (4) 2yr-24hr rainfall amount (P2) was obtained from SWFWMD 2yr-24hr return period rainfall map
 (5) Average Velocity for Paved Surface = 20.3282(s)^0.5 (See Appendix F TR55 Manual)
 (6) Average Velocity for Unpaved Surface = 16.1345(s)^0.5 (See Appendix F TR55 Manual)

3/3

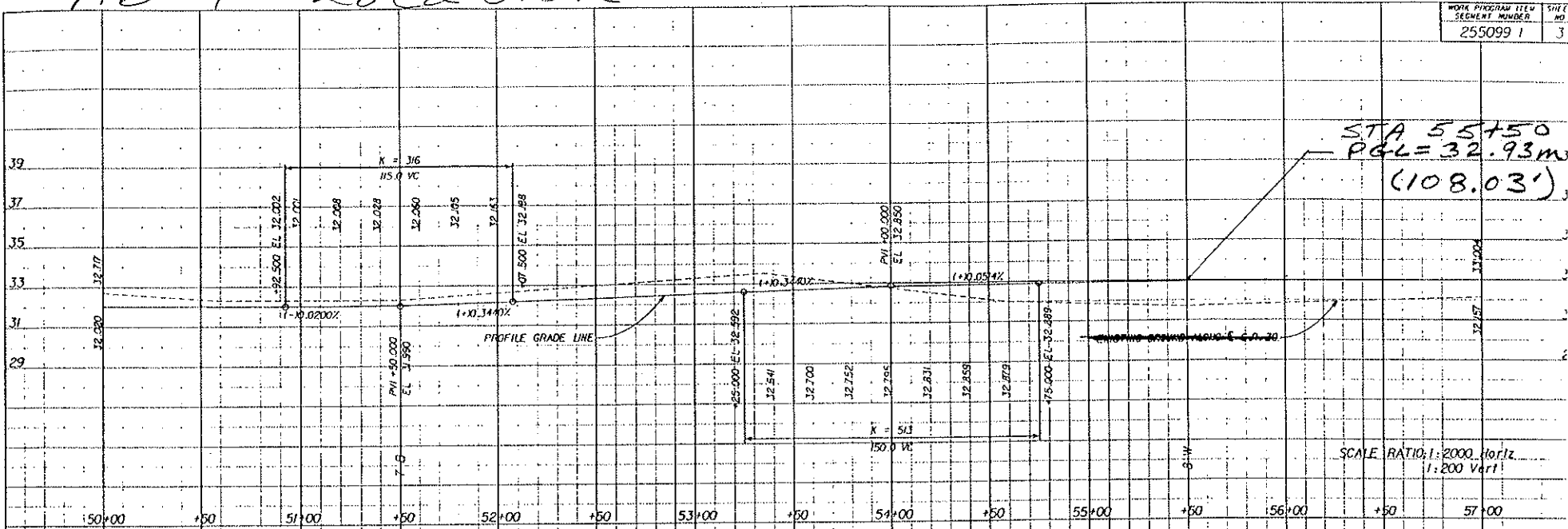
URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 3 PROJ. NO. C100003240.19
DESCRIPTION: V.B. CULVERT LOCATION COMPUTED BY: Zinner DATE: 5-27-99
AND CROSS SECTION CHECKED BY: Pratt DATE: 5-28-99

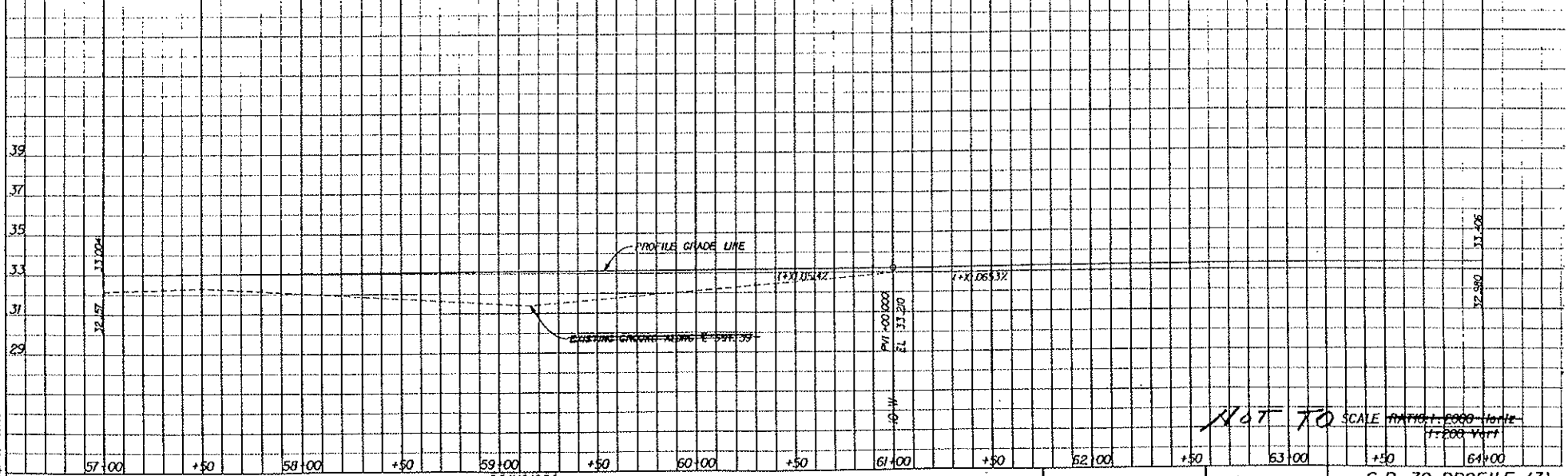
A conceptual vertical profile was developed for this PD&E. See the enclosed portion of the vertical profile and where AB-4 will be located. Also enclosed is a sketch of a half cross section of the proposed cross drain AB-4.

AB-4 Location

WORK PROGRAM ITEM	SHEET
255099 1	3



SCALE RATIO: 1:2000 Horiz
1:200 Vert



NOT TO SCALE RATIO: 1:2000 Horiz
1:200 Vert

C:\p3\sheet3\p3\m31.dwg

DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION

FLORIDA DEPARTMENT OF TRANSPORTATION

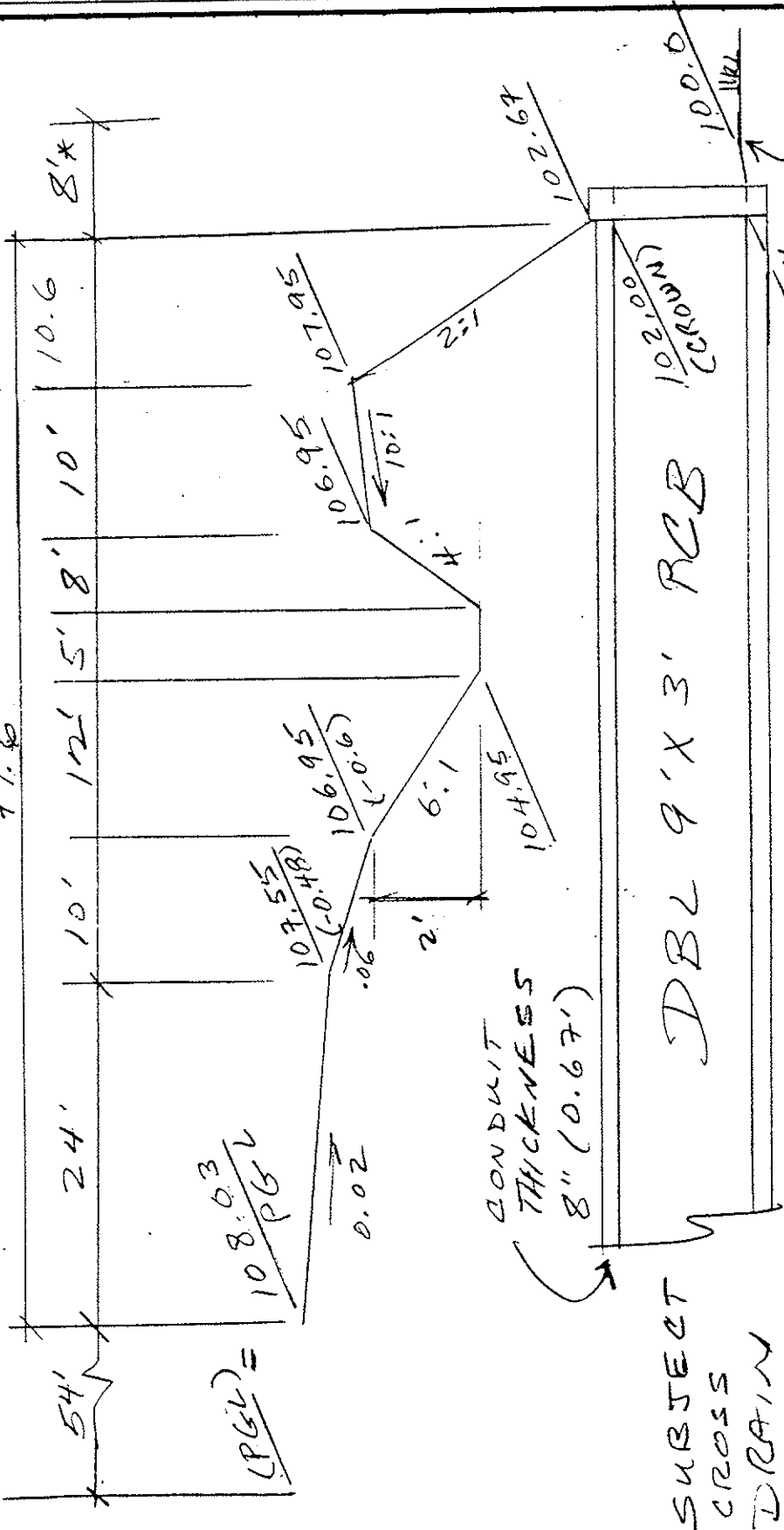
URS Greiner

S.R. 39 PROFILE (3)
STA: 50+00 - STA: 64+00

JOB Alex St. Bypass / SR 39
 DESCRIPTION AB-4 Length Calc.

SHEET 3 OF 3 PROJ. NO. C100003240-17
 COMPUTED BY Zimmer DATE 6-4-99
 CHECKED BY _____ DATE _____

AB-4: Total Length = $54' + 2 \times (79.6) + 8' = 221.2'$
 Station: 79.6 Use 222'



EXIST. GRADE
 100.0
 99.0 ELEV. U/S

* 8' FOR DBI WITH TRAVERSABLE SLOTS TO ACCEPT OFFSITE FLOWS ON UPSTREAM END OF CROSS DRAIN ONLY.

NOT TO SCALE

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 4 PROJ. NO. C100003240.19
DESCRIPTION: V.C. 50-YEAR AND 100- COMPUTED BY: Zinner DATE: 5-27-99
YEAR CULVERT CAPACITY ANALYSES CHECKED BY: Pratt DATE: 5-28-99

The capacity of the proposed culvert AB-4 was analyzed for the 50- and 100-year storm events using HY-8, software based on the techniques provided in FHWA Hydraulic Design Series # 5. See the enclosed HY-8 output for the analyses.

2/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 16:31:02

FILE DATE: 06-03-1999
FILE NAME: AB4_LC

FHWA CULVERT ANALYSIS
HY-8, VERSION 6.0

C U L V E R T N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	99.00	98.00	222.00	2 RCB	9.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: AB4_LC DATE: 06-03-1999

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
50-103.09	84.0	84.0	0.0	0.0	0.0	0.0	0.0	0.00	1
4R 103.09	84.9	84.9	0.0	0.0	0.0	0.0	0.0	0.00	1
103.09	85.8	85.8	0.0	0.0	0.0	0.0	0.0	0.00	1
103.09	86.7	86.7	0.0	0.0	0.0	0.0	0.0	0.00	1
103.09	87.6	87.6	0.0	0.0	0.0	0.0	0.0	0.00	1
103.10	88.5	88.5	0.0	0.0	0.0	0.0	0.0	0.00	1
103.10	89.4	89.4	0.0	0.0	0.0	0.0	0.0	0.00	1
103.10	90.3	90.3	0.0	0.0	0.0	0.0	0.0	0.00	1
103.10	91.2	91.2	0.0	0.0	0.0	0.0	0.0	0.00	1
103.10	92.1	92.1	0.0	0.0	0.0	0.0	0.0	0.00	1
100-103.11	93.0	93.0	0.0	0.0	0.0	0.0	0.0	0.00	1
4R 108.03	641.8	641.8	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: AB4_LC DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
103.09	0.000	84.00	0.00	0.00
103.09	0.000	84.90	0.00	0.00
103.09	0.000	85.80	0.00	0.00
103.09	0.000	86.70	0.00	0.00
103.09	0.000	87.60	0.00	0.00
103.10	0.000	88.50	0.00	0.00
103.10	0.000	89.40	0.00	0.00
103.10	0.000	90.30	0.00	0.00
103.10	0.000	91.20	0.00	0.00
103.10	0.000	92.10	0.00	0.00
103.11	0.000	93.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010 <2> TOLERANCE (%) = 1.000

3/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 16:31:02

FILE DATE: 06-03-1999
FILE NAME: AB4_LC

PERFORMANCE CURVE FOR CULVERT 1 - 2(9.00 (ft) BY 3.00 (ft)) RCB

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
84.00	103.09	1.50	4.09	4-FFt	0.74	0.88	3.00	5.00	1.56	0.00
84.90	103.09	1.51	4.09	4-FFt	0.75	0.89	3.00	5.00	1.57	0.00
85.80	103.09	1.52	4.09	4-FFt	0.75	0.89	3.00	5.00	1.59	0.00
86.70	103.09	1.53	4.09	4-FFt	0.76	0.90	3.00	5.00	1.61	0.00
87.60	103.09	1.54	4.09	4-FFt	0.76	0.90	3.00	5.00	1.62	0.00
88.50	103.10	1.55	4.10	4-FFt	0.77	0.91	3.00	5.00	1.64	0.00
89.40	103.10	1.56	4.10	4-FFt	0.77	0.92	3.00	5.00	1.66	0.00
90.30	103.10	1.57	4.10	4-FFt	0.78	0.92	3.00	5.00	1.67	0.00
91.20	103.10	1.58	4.10	4-FFt	0.79	0.93	3.00	5.00	1.69	0.00
92.10	103.10	1.59	4.10	4-FFt	0.79	0.94	3.00	5.00	1.71	0.00
93.00	103.11	1.60	4.11	4-FFt	0.80	0.94	3.00	5.00	1.72	0.00

El. inlet face invert	99.00 ft	El. outlet invert	98.00 ft
El. inlet throat invert	0.00 ft	El. inlet crest	0.00 ft

***** SITE DATA ***** EMBANKMENT TOE *****

UPSTREAM STATION	0.00 ft
UPSTREAM ELEVATION	99.00 ft
UPSTREAM EMBANKMENT SLOPE (X:1)	0.00
DOWNSTREAM STATION	222.00 ft
DOWNSTREAM ELEVATION	98.00 ft
DOWNSTREAM EMBANKMENT SLOPE (X:1)	0.00

***** CULVERT DATA SUMMARY *****

BARREL SHAPE	BOX
BARREL SPAN	9.00 ft
BARREL RISE	3.00 ft
BARREL MATERIAL	CONCRETE
BARREL MANNING'S n	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE (90-45 DEG.)
INLET DEPRESSION	NONE

4/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 16:31:02

FILE DATE: 06-03-1999
FILE NAME: AB4_LC

TAILWATER

CONSTANT WATER SURFACE ELEVATION
103.00

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	212.00 ft
CREST LENGTH	3000.00 ft
OVERTOPPING CREST ELEVATION	108.03 ft

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 5 PROJ. NO. C100003240.19
DESCRIPTION: V.D. RESULTS COMPUTED BY: Zinner DATE: 5-27-99
CHECKED BY: Pratt DATE: 5-28-99

The cross drain which satisfies the 0.1' rise for the 50-year storm event is a double 9'x3' reinforced concrete box culvert (RCB).

The results of the HY-8 analyses for the proposed culvert AB-4 are shown below:

<u>Event (year)</u>	<u>Existing Headwater/ Tailwater Elevation feet (NGVD)</u>	<u>Proposed Headwater Elevation feet (NGVD)</u>
50	103.00	103.09
100	103.00	103.11

VI. PROPOSED CULVERT AB-5

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 3 PROJ. NO. C100003240.19
 DESCRIPTION: VI.A. DISCHARGE RATES COMPUTED BY: Zinner DATE: 5-27-99
 AND TAILWATER ELEVATIONS CHECKED BY: Pratt DATE: 5-28-99

Discharge rates for culvert AB-5 were calculated using the Rational method. See the enclosed calculations for the peak discharge rates and they are as follows:

Event (Year)	Discharge Rate (cfs)	Source
50	16	Rational method
100	18	Rational method

The elevation of the crown of the proposed cross drain and the seasonal high water table (SHWT) elevation was compared, and the higher stage was used for the proposed AB-5 capacity analyses. In this case the SHWT elevation was used. The nearest field verified SHWT elevation was located at the station 61+00 and the SHWT elevation is 104.00 NGVD.

URS Greiner

JOB: SR 39 ALEXANDER ROAD BYPASS	SHEET 2 of 3	PROJ. NO. C100003240.19
DESCRIPTION: Rational C & Q calc.s	COMPUTED BY Jim Zinner	DATE 05-26-99
Drainage Area AB5	CHECKED BY	DATE

Input/Output = manually input values

Boxes

Explanation = unknown, previously input, or computed output values

Drainage Area = ac

Land Use	Area (ac)	C	C x A (ac)
Pavement	3.1	0.95	2.9
Pasture, grass, farmlands	3.9	0.2	0.8
Total =			<u>7</u> <u>3.7</u>

C coefficients assumed for sandy soils and flat (0-2%) slopes

composite C = (C x A) / Area = 3.7 / 7 =

TOC = mins = hours (see following worksheet)

Intensities from FDOT Zone IDF Curve

frequency = year

Intensity in / hour

Q = CIA = * * = cfs

frequency = year

Intensity in / hour

Q = CIA = * * = cfs

Project: S.R. 39 Alexander Street Bypass
 Subject: Time of Concentration Calculations Proposed Conditions
 Project No.: C100003240.19

Sheet 2 of 2
 Computed By: JYZ Date: 04-07-99
 Checked By: RWP Date: 5-28-99

Basin #	Sheet Flow						Shallow Concentrated Flow					Channel Flow								Total Time	Total Time	
	Surface Type	Mannings Coeff. n	Flow Length <=300 ft. L (ft)	2yr-24hr Rainfall P2 (in)	Land Slope s (ft/ft)	Time T1 (min)	Surface Type	Flow Length L (ft)	Water Course Slope s (ft/ft)	Avg. Vel. V (ft/s)	Time T2 (min)	Cross Sectional Flow Area a (ft^2)	Wetted Perimeter Pw (ft)	Hydraulic Radius r = a/Pw (ft)	Channel Slope s (ft/ft)	Mannings Roughness Coeff. n	Vel. V (ft/s)	Flow Length L (ft)	Time T3 (min)			Tc (min)
AB3	Cultivat. >20% cover	0.17	300	4.0	0.006	37.8	unpavd	900	0.014	1.4	10.7											
												Total					37.8	Total				
AB4	Cultivat. >20% cover	0.17	300	4.0	0.028	20.4	unpavd	1000	0.008	1.4	11.9	18.000	21.300	0.845	0.0004	0.1	0.266	2700	169			
												310.000	320.100	0.968	0.0046	0.1	0.989	650	11	Total		
AB5	Pasture, grass, farmland	0.17	300	4.0	0.004	44.4	unpavd	700	0.004	1.4	8.3											
												Total					44.4	Total				

- NOTES: (1) Sheet Flow Mannings Roughness Coefficient obtained from Table 3-1 Roughness Coefficients for Sheet Flow, Urban Hydrology for Small Watersheds, TR55 Manual
 (2) Maximum hydraulic length for sheet Flow is 300 ft. (TR 55 Manual)
 (3) Maximum hydraulic length for shallow concentrated flow is 1000 ft.
 (4) 2yr-24hr rainfall amount (P2) was obtained from SWFWMD 2yr-24hr return period rainfall map
 (5) Average Velocity for Paved Surface = 20.3282(s)^0.5 (See Appendix F TR55 Manual)
 (6) Average Velocity for Unpaved Surface = 16.1345(s)^0.5 (See Appendix F TR55 Manual)

6/6

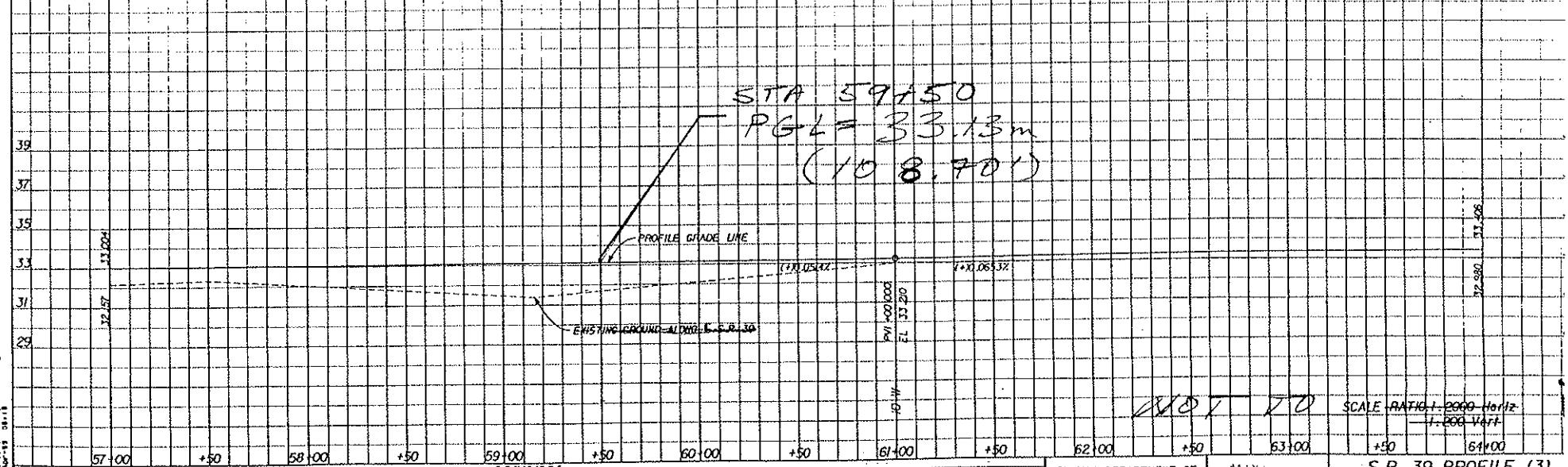
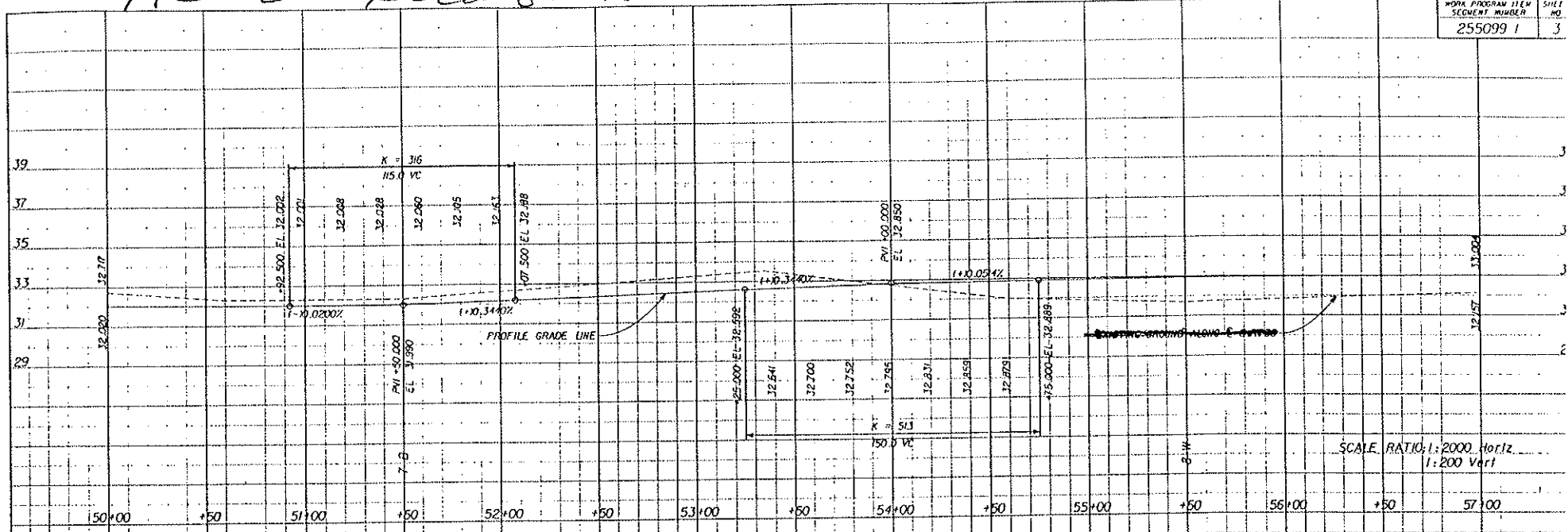
URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 3 PROJ. NO. C100003240.19
DESCRIPTION: VI. B. CULVERT LOCATION COMPUTED BY: Zinner DATE: 5-27-99
AND CROSS SECTION CHECKED BY: Pratt DATE: 5-28-99

A conceptual vertical profile was developed for this PD&E. See the enclosed portion of the vertical profile and where AB-5 will be located. Also enclosed is a sketch of a half cross section of the proposed cross drain AB-5.

AR-5 Location

WORK PROGRAM STEP	SHEET
255099 1	3



STA 59+50
 PGL = 33.13m
 (108.70')

C:\p23\shades\graphical.dwg
 15.04.2015 08:11

DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION

FLORIDA DEPARTMENT OF TRANSPORTATION

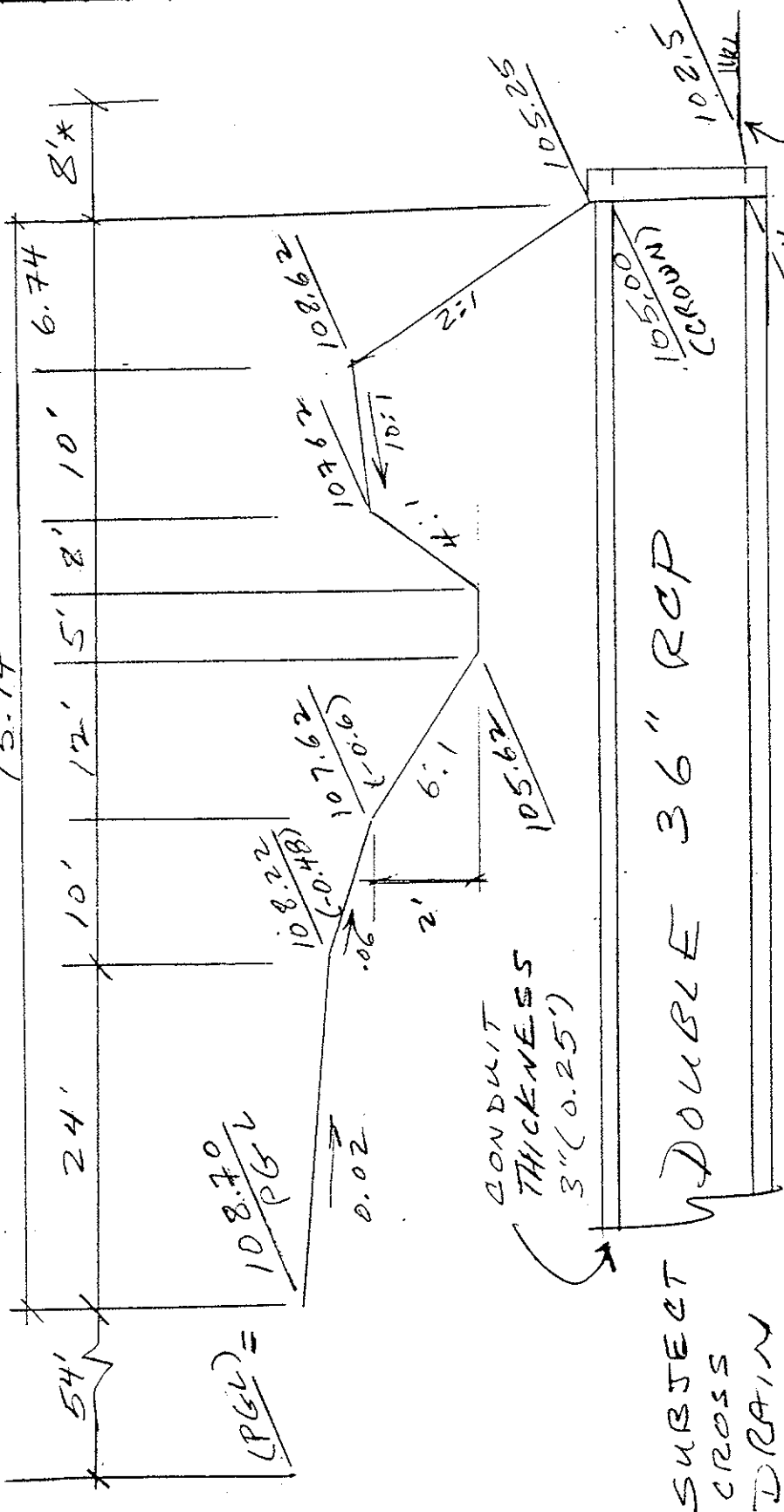
URS Greiner

S.R. 39 PROFILE (3)
 STA 50+00 - STA 64+00

JOB Alex. St. Bypass / SR 39
 DESCRIPTION AB-5 Length Calc.

SHEET 3 OF 3 PROJ. NO. C100003240.19
 COMPUTED BY Zinner DATE 6-4-99
 CHECKED BY _____ DATE _____

AB-5: Total Length = 54' + 2 x (75.74) + 8' = 213.48'
 Station: _____
 USE 215'



EXIST. GRADE

102.0' ELEV.
 102.5' ELEV.

SUBJECT CROSS DRAIN
 DOUBLE 36" RCP
 CONDUIT THICKNESS 3" (0.25')

* 8' FOR DBI WITH TRAVERSABLE SLOTS TO ACCEPT OFFSITE FLOWS ON UPSTREAM END OF CROSS DRAIN ONLY.

NOT TO SCALE

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 4 PROJ. NO. C100003240.19
DESCRIPTION: VI.C. 50-YEAR AND 100- COMPUTED BY: Zinner DATE: 5-27-99
YEAR CULVERT CAPACITY ANALYSES CHECKED BY: Pratt DATE: 5-28-99

The capacity of the proposed culvert AB-5 was analyzed for the 50- and 100-year storm events using HY-8, software based on the techniques provided in FHWA Hydraulic Design Series # 5. See the enclosed HY-8 output for the analyses.

2/4

CURRENT DATE: 06-03-1999
 CURRENT TIME: 18:18:43

FILE DATE: 06-03-1999
 FILE NAME: AB5_LC

FHWA CULVERT ANALYSIS
 HY-8, VERSION 6.0

C U L V E R T N O. 1 2 3 4 5 6	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	102.00	101.00	215.00	2 RCP	3.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: AB5_LC DATE: 06-03-1999

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
50-105.04	16.0	16.0	0.0	0.0	0.0	0.0	0.0	0.00	1
4R 105.04	16.2	16.2	0.0	0.0	0.0	0.0	0.0	0.00	1
105.04	16.4	16.4	0.0	0.0	0.0	0.0	0.0	0.00	1
105.04	16.6	16.6	0.0	0.0	0.0	0.0	0.0	0.00	1
105.04	16.8	16.8	0.0	0.0	0.0	0.0	0.0	0.00	1
105.05	17.0	17.0	0.0	0.0	0.0	0.0	0.0	0.00	1
105.05	17.2	17.2	0.0	0.0	0.0	0.0	0.0	0.00	1
105.05	17.4	17.4	0.0	0.0	0.0	0.0	0.0	0.00	1
105.05	17.6	17.6	0.0	0.0	0.0	0.0	0.0	0.00	1
105.05	17.8	17.8	0.0	0.0	0.0	0.0	0.0	0.00	1
100-105.05	18.0	18.0	0.0	0.0	0.0	0.0	0.0	0.00	1
4R 108.70	162.9	162.9	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: AB5_LC DATE: 06-03-1999

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
105.04	0.000	16.00	0.00	0.00
105.04	0.000	16.20	0.00	0.00
105.04	0.000	16.40	0.00	0.00
105.04	0.000	16.60	0.00	0.00
105.04	0.000	16.80	0.00	0.00
105.05	0.000	17.00	0.00	0.00
105.05	0.000	17.20	0.00	0.00
105.05	0.000	17.40	0.00	0.00
105.05	0.000	17.60	0.00	0.00
105.05	0.000	17.80	0.00	0.00
105.05	0.000	18.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

3/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 18:18:43

FILE DATE: 06-03-1999
FILE NAME: AB5_LC

PERFORMANCE CURVE FOR CULVERT 1 - 2(3.00 (ft) BY 3.00 (ft)) RCP

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
16.00	105.04	1.15	3.04	4-FFt	0.80	0.89	3.00	4.00	1.13	0.00
16.20	105.04	1.16	3.04	4-FFt	0.81	0.90	3.00	4.00	1.15	0.00
16.40	105.04	1.17	3.04	4-FFt	0.82	0.90	3.00	4.00	1.16	0.00
16.60	105.04	1.18	3.04	4-FFt	0.82	0.91	3.00	4.00	1.17	0.00
16.80	105.04	1.19	3.04	4-FFt	0.83	0.91	3.00	4.00	1.19	0.00
17.00	105.05	1.20	3.05	4-FFt	0.83	0.92	3.00	4.00	1.20	0.00
17.20	105.05	1.20	3.05	4-FFt	0.84	0.92	3.00	4.00	1.22	0.00
17.40	105.05	1.21	3.05	4-FFt	0.84	0.93	3.00	4.00	1.23	0.00
17.60	105.05	1.22	3.05	4-FFt	0.85	0.93	3.00	4.00	1.24	0.00
17.80	105.05	1.23	3.05	4-FFt	0.85	0.94	3.00	4.00	1.26	0.00
18.00	105.05	1.24	3.05	4-FFt	0.86	0.94	3.00	4.00	1.27	0.00
El. inlet face invert					102.00 ft	El. outlet invert		101.00 ft		
El. inlet throat invert					0.00 ft	El. inlet crest		0.00 ft		

***** SITE DATA ***** CULVERT INVERT *****

INLET STATION 0.00 ft
 INLET ELEVATION 102.00 ft
 OUTLET STATION 215.00 ft
 OUTLET ELEVATION 101.00 ft
 NUMBER OF BARRELS 2
 SLOPE (V/H) 0.0047
 CULVERT LENGTH ALONG SLOPE 215.00 ft

***** CULVERT DATA SUMMARY *****

BARREL SHAPE CIRCULAR
 BARREL DIAMETER 3.00 ft
 BARREL MATERIAL CONCRETE
 BARREL MANNING'S n 0.012
 INLET TYPE CONVENTIONAL
 INLET EDGE AND WALL BEVELED EDGE (1:1)
 INLET DEPRESSION NONE

4/4

CURRENT DATE: 06-03-1999
CURRENT TIME: 18:18:43

FILE DATE: 06-03-1999
FILE NAME: AB5_LC

TAILWATER

CONSTANT WATER SURFACE ELEVATION
105.00

ROADWAY OVERTOPPING DATA

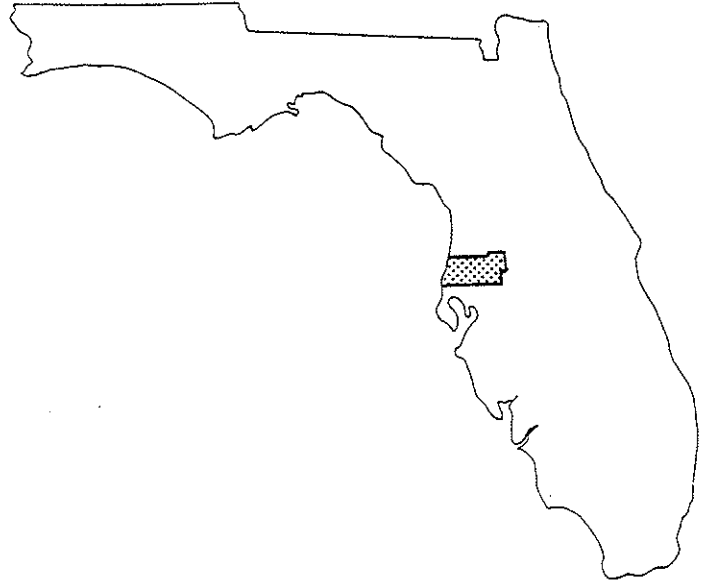
ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	192.00 ft
CREST LENGTH	3000.00 ft
OVERTOPPING CREST ELEVATION	108.70 ft

**VII. HILLSBOROUGH RIVER WSPRO
BACKWATER ANALYSIS**

FLOOD INSURANCE STUDY



PASCO COUNTY,
FLORIDA
UNINCORPORATED AREAS



REVISED:

SEPTEMBER 30, 1992



Federal Emergency Management Agency

COMMUNITY NUMBER -120230

Table 3. Summary of Discharges

<u>Flooding Source and Location</u>	<u>Drainage Area (Square Miles)</u>	<u>Peak Discharges (Cubic Feet per Second)</u>			
		<u>10-Year</u>	<u>50-Year</u>	<u>100-Year</u>	<u>500-Year</u>
Anclote River At State Highway 54	72.5	2,880	5,220	6,420	9,760
Duck Slough At Mouth	2.8	109	200	268	415
Hillsborough River At Confluence With Blackwater Creek	84	2,600	4,130	4,890	6,800
Pithlachascotee River At the City of New Port Richey	182	1,084	2,060	2,600	4,170
Withlacoochee River At Trilby	570	3,880	7,260	9,080	14,400

VII.A. S.R. 39 BRIDGE OVER THE HILLSBOROUGH RIVER REQUIREMENTS

The Hillsborough River is FEMA regulated from the S.R. 39 downstream. Upstream of the bridge the river must meet the Pasco County criteria requiring no increase in head loss above existing conditions.

The cross sections data at the Hillsborough River were obtained from a report entitled "Project Development and Environmental Studies, Location Hydraulics Report For State Road 39 Hillsborough and Pasco Counties" (see Section 10, References, of this report). A total of 19 cross sections were used in the WSPRO model used to analyze the subject bridge crossing. The hydrologic data from the FEMA Flood Insurance Study (FIS) indicates the discharge of the 50- and 100-year storm events at the downstream model cross section are 4130 and 4890 cfs, respectively. The title page and Table 3 from the FIS which the discharge rates were taken are included after this page.

A WSPRO analysis was conducted to evaluate the head loss due to the existing and proposed bridges.

VII.B. EXISTING CONDITIONS

The existing structure was constructed in 1947 and is located at Mile Post 1.585 of S.R. 39. The structure has 21 spans of 15 ft. resulting in the overall structure length of 315.5 ft. The substructure consists of pile bents. Each pile bent has five timber piles spaced at 6 ft., topped by a 1.83-foot square cap. The superstructure is a 13-inch deep flat slab structure. The bridge width is 26 feet between curbs. The low member elevation is 70 ft. NGVD. The bridge opening data were checked. The net horizontal clearance is 280 ft. The difference between the total bridge length and the horizontal clearance is 35.5 ft.

VII.C. PROPOSED CONDITIONS

It is proposed to replace the existing bridge in kind, with a parallel bridge of the same length constructed for the two new lanes. The substructures are proposed to be the same. Without detailed pier dimension, the pier width of the proposed bridge is assumed to be the same as the existing bridge.

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET / OF 3/ PROJ. NO. C100003240.19
DESCRIPTION: VII.D. WSPRO ANALYSIS, COMPUTED BY: Zinner DATE: 5-27-99
EXISTING CONDITIONS CHECKED BY: Pratt DATE: 5-28-99

The WSPRO analyses were conducted considering the case of existing conditions "with the old bridge." This section includes the WSPRO input and output for the analysis of 50- and 100-year storm events for the existing conditions.

EXISTING CONDITIONS 2/31

ANALYSIS INPUT

T1 HILLSBOROUGH RIVER, SR 39
 T2 LOCATION HYDRAULICS STUDY
 T3 50 AND 100 YR. FLOOD
 * J3 1
 Q 4130 4890
 WS 50.75 51.74
 *
 XS B1 3450
 GR 0.0, 60.00 1900, 55.00 3700, 50.00 4200, 45.00 4400, 43.00
 GR 5100, 39.00 5180, 37.00 5195, 33.00 5200, 33.00 5220, 38.00
 GR 5250, 39.00 5270, 40.00 5570, 43.0 6000, 45.00 7900, 50.0
 GR 9500, 55.00 13570, 60.00
 SA 5180 5220
 N 0.25 0.07 0.25
 XS C 7000
 GR 0.0, 60.00 1500, 55.00 2200, 50.00 3300, 45.00 3350, 41.00
 GR 3390, 40.00 3405, 35.00 3410, 35.00 3420, 30.00 3540, 43.00
 GR 4178, 45.00 4720, 50.00 4920, 52.00 6000, 55.00 9000, 60.00
 SA 3390 3420
 N 0.25 0.07 0.25
 *
 XS D 10200
 GR 0.0, 60.00 2300, 55.00 2750, 54.00 2950, 50.00 3380, 45.00
 GR 3400, 44.00 3415, 39.00 3420, 39.00 3440, 44.00 3470, 46.00
 GR 4020, 48.00 4200, 50.00 5500, 55.0 7550, 60.0
 SA 3380 3420
 *
 XS E 13200
 GR 0.0, 60.00 2000, 55.00 2350, 50.00 2600, 45.00 2620, 44.00
 GR 2625, 39.0 2630, 39.00 2640, 44.00 2680, 45.00 3180, 50.00
 GR 3930, 55.00 6000, 60.0
 SA 2620 2640
 *
 XS F 16200
 GR 0.0, 60.00 700, 55.00 1000, 50.00 1079, 48.00 1080, 47.00
 GR 1095, 42.0 1100, 42.00 1110, 47.00 1170, 48.00 1750, 50.00
 GR 2150, 55.00 2900, 60.0
 SA 1080 1110
 *
 XS G 18500
 GR 0.0, 65.00 380, 60.00 900, 55.00 1100, 51.00 1800, 50.00
 GR 1810, 49.00 1960, 48.00 1970, 43.00 1975, 43.00 1990, 48.00
 GR 2240, 49.00 2260, 50.00 2860, 54.0 3360, 55.00 4060, 65.0

SA 1960 1990

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XS H 20500

GR	0.0, 62.50	300, 60.00	700, 55.0	1270, 50.00	1280, 49.00
GR	1300, 48.00	1305, 43.00	1310, 43.00	1320, 48.00	1350, 49.00
GR	1370, 50.00	2100, 55.00	2950, 60.0	5400, 65.00	
SA	1300	1320			

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XS HA 25100

GR	0.0, 65.00	1400, 60.00	1750, 55.00	2250, 54.00	2700, 51.00
GR	2705, 46.00	2710, 46.00	2720, 51.00	3420, 55.00	3720, 60.00
GR	4100, 63.00				
SA	2700	2720			

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XS LOBR 25900

GR	0.0, 65.00	1400, 60.00	1750, 55.00	2250, 54.00	2700, 51.00
GR	2705, 46.00	2710, 46.00	2720, 51.00	3420, 55.00	3720, 60.00
GR	4100, 63.00				
SA	2700	2720			

*

N 0.25 0.07 0.25

*

XS APPR 26980, 0, 0.3, 0.1

GR	0.0, 65.00	1400, 60.00	1750, 56.00	2250, 53.00	3250, 52.00
GR	3260, 47.00	3265, 47.00	3270, 54.00	3470, 55.00	4220, 60.00
GR	6220, 65.00				
SA	3250	3270			

*

N 0.25 0.07 0.25

*

XS I 31180

GR	0.0, 70.00	3800, 65.00	5200, 60.00	5600, 56.00	5620, 51.00
GR	5640, 51.00	5650, 56.00	6100, 59.00	6800, 60.00	7350, 65.00
GR	8750, 70.00				
SA	5600	5650			

*

N 0.25 0.07 0.25

*

XS FULLV 32188

GR	0.0, 73.00	210, 74.30	360, 73.60	540, 73.00	1060, 72.80
GR	1440, 72.60	1860, 72.50	2080, 73.00	2410, 73.60	2440, 70.40
GR	2463, 60.10	2470, 58.60	2590, 55.90	2605, 51.20	2620, 51.40
GR	2628, 52.40	2650, 57.00	2725, 59.10	2755, 70.40	2890, 73.0
GR	3130, 72.00	3350, 71.0	3980, 70.0	5090, 70.00	5160, 71.0
GR	5320, 72.00	5520, 74.00			
SA	2440	2755			

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BR SR39 32188, 70.0, 0.0, 0.5, 0.3
 GR 2410.0, 73.6 2490, 70.40 2500, 66.40 2518, 56.30 2590, 55.90
 GR 2605, 51.20 2620, 51.40 2628, 52.40 2650, 57.00 2664, 57.40
 GR 2680, 65.10 2690, 70.00 2441, 70.00 2410, 73.60
 SA 2518 2664
 N 0.05 0.03 0.05
 CD 3, 105, 2, 69.70
 PD 1 53.2, 1.5, 1 56.4, 3.0, 1 57.8, 4.50, 1

*

XR ROAD 32238, 105, 1
 GR 0.0, 74.30 1860, 72.50 2410, 73.60 2440, 72.00 2755, 72.00

*

AS UP39 32470, 0.0, 0.5, 0.1
 GR 0.0, 70.0 125, 69.00 240, 66.0 420, 66.00 460, 67.00
 GR 640, 67.00 830, 66.00 1040, 66.00 1090, 67.00 1250, 68.00
 GR 1285, 69.00 1325, 69.00 1360, 68.0 1410, 68.00 1470, 69.0
 GR 1640, 69.00 1710, 68.00 2190, 68.00 2290, 64.00 2580, 62.00
 GR 2780, 58.00 2805, 58.00 2830, 59.0 2850, 56.00 2860, 51.4
 GR 2875, 51.40 2880, 56.00 2900, 59.0 3690, 63.00 3750, 65.00
 GR 3830, 66.00 4290, 74.00
 SA .2830 2900
 N 0.25, 0.07, 0.25

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XS L 32765
 GR 0.0, 68.00 180, 65.00 470, 65.00 640, 63.00 940, 63.00
 GR 960, 65.00 1070, 69.00 1100, 69.00 1170, 67.00 1430, 65.00
 GR 1820, 65.00 1840, 68.00 1920, 68.0 2494, 58.30 2533, 57.7
 GR 2539, 56.40 2545, 57.60 2703, 58.2 2726, 52.70 2751, 53.10
 GR 2755, 55.70 2772, 59.10 2780, 55.6 2799, 56.30 2842, 59.2
 GR 2862, 55.80 2881, 58.00 2908, 58.6 2932, 54.90 2960, 60.00
 GR 3020, 61.00 3835, 65.00 4160, 74.00
 SA 2725 2842
 XS UPXS1 33025 * * * 0.0004
 EX
 ER

EXISTING CONDITIONS ANALYSIS OUTPUT

5/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Run Date & Time: 3/ 2/99 4:49 pm Version V050196
Input File: SR39TX1.INP9 Output File: SR39TX1.LST9

-----*
T1 HILLSBOROUGH RIVER, SR 39
T2 LOCATION HYDRAULICS STUDY
T3 50 AND 100 YR. FLOOD
Q 4130 4890

*** Processing Flow Data; Placing Information into Sequence 1 ***

WS 50.75 51.74

6/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record B1 *
-----*

XS	B1 3450				
GR	0.0, 60.00	1900, 55.00	3700, 50.00	4200, 45.00	4400, 43
GR	5100, 39.00	5180, 37.00	5195, 33.00	5200, 33.00	5220, 38.0
GR	5250, 39.00	5270, 40.00	5570, 43.0	6000, 45.00	7900, 50.
GR	9500, 55.00	13570, 60.00			
SA	5180 5220				
N	0.25 0.07 0.25				

*** Completed Reading Data Associated With Header Record B1 ***
*** Storing X-Section Data In Temporary File As Record Number 1 ***

*** Data Summary For Header Record B1 ***
SRD Location: 3450. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (17 pairs)

X	Y	X	Y	X	Y
.000	60.000	1900.000	55.000	3700.000	50.000
4200.000	45.000	4400.000	43.000	5100.000	39.000
5180.000	37.000	5195.000	33.000	5200.000	33.000
5220.000	38.000	5250.000	39.000	5270.000	40.000
5570.000	43.000	6000.000	45.000	7900.000	50.000
9500.000	55.000	13570.000	60.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 13570.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 33.000 (associated X-Station: 5200.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	5180.000
2	.070	---
	---	5220.000
3	.250	---

-----*
* Finished Processing Header Record B1 *
-----*

7/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record C *
-----*

XS C 7000
GR 0.0, 60.00 1500, 55.00 2200, 50.00 3300, 45.00 3350, 41.0
GR 3390, 40.00 3405, 35.00 3410, 35.00 3420, 30.00 3540, 43.0
GR 4178, 45.00 4720, 50.00 4920, 52.00 6000, 55.00 9000, 60.0
SA 3390 3420
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record C ***
*** Storing X-Section Data In Temporary File As Record Number 2 ***

*** Data Summary For Header Record C ***
SRD Location: 7000. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (15 pairs)

X	Y	X	Y	X	Y
.000	60.000	1500.000	55.000	2200.000	50.000
3300.000	45.000	3350.000	41.000	3390.000	40.000
3405.000	35.000	3410.000	35.000	3420.000	30.000
3540.000	43.000	4178.000	45.000	4720.000	50.000
4920.000	52.000	6000.000	55.000	9000.000	60.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 9000.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 30.000 (associated X-Station: 3420.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	3390.000
2	.070	---
	---	3420.000
3	.250	---

-----*
* Finished Processing Header Record C *
-----*

8/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record D *
-----*

XS	D	10200					
GR		0.0, 60.00	2300, 55.00	2750, 54.00	2950, 50.00	3380, 45	
GR		3400, 44.00	3415, 39.00	3420, 39.00	3440, 44.00	3470, 46.0	
GR		4020, 48.00	4200, 50.00	5500, 55.0	7550, 60.0		
SA		3380	3420				

*** Completed Reading Data Associated With Header Record D ***
*** Storing X-Section Data In Temporary File As Record Number 3 ***

*** Data Summary For Header Record D ***
SRD Location: 10200. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
.000	60.000	2300.000	55.000	2750.000	54.000
2950.000	50.000	3380.000	45.000	3400.000	44.000
3415.000	39.000	3420.000	39.000	3440.000	44.000
3470.000	46.000	4020.000	48.000	4200.000	50.000
5500.000	55.000	7550.000	60.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 7550.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 39.000 (associated X-Station: 3420.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	3380.000
2	.070	---
	---	3420.000
3	.250	---

-----*
* Finished Processing Header Record D *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record E *
-----*

XS E 13200
GR 0.0, 60.00 2000, 55.00 2350, 50.00 2600, 45.00 2620, 44
GR 2625, 39.0 2630, 39.00 2640, 44.00 2680, 45.00 3180, 50.
GR 3930, 55.00 6000, 60.0
SA 2620 2640

*** Completed Reading Data Associated With Header Record E ***
*** Storing X-Section Data In Temporary File As Record Number 4 ***

*** Data Summary For Header Record E ***
SRD Location: 13200. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (12 pairs)

X	Y	X	Y	X	Y
.000	60.000	2000.000	55.000	2350.000	50.000
2600.000	45.000	2620.000	44.000	2625.000	39.000
2630.000	39.000	2640.000	44.000	2680.000	45.000
3180.000	50.000	3930.000	55.000	6000.000	60.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 6000.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 39.000 (associated X-Station: 2630.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2620.000
2	.070	---
	---	2640.000
3	.250	---

-----*
* Finished Processing Header Record E *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record F *
-----*

XS F 16200
GR 0.0, 60.00 700, 55.00 1000, 50.00 1079, 48.00 1080, 4
GR 1095, 42.0 1100, 42.00 1110, 47.00 1170, 48.00 1750, 50.
GR 2150, 55.00 2900, 60.0
SA 1080 1110

*** Completed Reading Data Associated With Header Record F ***
*** Storing X-Section Data In Temporary File As Record Number 5 ***

*** Data Summary For Header Record F ***
SRD Location: 16200. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (12 pairs)

X	Y	X	Y	X	Y
.000	60.000	700.000	55.000	1000.000	50.000
1079.000	48.000	1080.000	4.000	1095.000	42.000
1100.000	42.000	1110.000	47.000	1170.000	48.000
1750.000	50.000	2150.000	55.000	2900.000	60.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 2900.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 4.000 (associated X-Station: 1080.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	1080.000
2	.070	---
	---	1110.000
3	.250	---

-----*
* Finished Processing Header Record F *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record G *
-----*

XS	G	18500				
GR		0.0, 65.00	380, 60.00	900, 55.00	1100, 51.00	1800, 50.
GR		1810, 49.00	1960, 48.00	1970, 43.00	1975, 43.00	1990, 48.0
GR		2240, 49.00	2260, 50.00	2860, 54.0	3360, 55.00	4060, 65.0
SA		1960	1990			

*** Completed Reading Data Associated With Header Record G ***
*** Storing X-Section Data In Temporary File As Record Number 6 ***

*** Data Summary For Header Record G ***
SRD Location: 18500. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (15 pairs)

X	Y	X	Y	X	Y
.000	65.000	380.000	60.000	900.000	55.000
1100.000	51.000	1800.000	50.000	1810.000	49.000
1960.000	48.000	1970.000	43.000	1975.000	43.000
1990.000	48.000	2240.000	49.000	2260.000	50.000
2860.000	54.000	3360.000	55.000	4060.000	65.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 4060.000 (associated Y-Elevation: 65.000)
Minimum Y-Elevation: 43.000 (associated X-Station: 1975.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	1960.000
2	.070	---
	---	1990.000
3	.250	---

-----*
* Finished Processing Header Record G *
-----*

12/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
.Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record H *
-----*

XS	H	20500				
GR		0.0, 62.50	300, 60.00	700, 55.0	1270, 50.00	1280, 49
GR		1300, 48.00	1305, 43.00	1310, 43.00	1320, 48.00	1350, 49.0
GR		1370, 50.00	2100, 55.00	2950, 60.0	5400, 65.00	
SA		1300	1320			

*** Completed Reading Data Associated With Header Record H ***
*** Storing X-Section Data In Temporary File As Record Number 7 ***

*** Data Summary For Header Record H ***
SRD Location: 20500. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
.000	62.500	300.000	60.000	700.000	55.000
1270.000	50.000	1280.000	49.000	1300.000	48.000
1305.000	43.000	1310.000	43.000	1320.000	48.000
1350.000	49.000	1370.000	50.000	2100.000	55.000
2950.000	60.000	5400.000	65.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 62.500)
Maximum X-Station: 5400.000 (associated Y-Elevation: 65.000)
Minimum Y-Elevation: 43.000 (associated X-Station: 1310.000)
Maximum Y-Elevation: 65.000 (associated X-Station: 5400.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	1300.000
2	.070	---
	---	1320.000
3	.250	---

-----*
* Finished Processing Header Record H *
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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record HA *
-----*

XS HA 25100
GR 0.0, 65.00 1400, 60.00 1750, 55.00 2250, 54.00 2700, 51
GR 2705, 46.00 2710, 46.00 2720, 51.00 3420, 55.00 3720, 60.0
GR 4100, 63.00
SA 2700 2720

*** Completed Reading Data Associated With Header Record HA ***
*** Storing X-Section Data In Temporary File As Record Number 8 ***

*** Data Summary For Header Record HA ***
SRD Location: 25100. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	65.000	1400.000	60.000	1750.000	55.000
2250.000	54.000	2700.000	51.000	2705.000	46.000
2710.000	46.000	2720.000	51.000	3420.000	55.000
3720.000	60.000	4100.000	63.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 4100.000 (associated Y-Elevation: 63.000)
Minimum Y-Elevation: 46.000 (associated X-Station: 2710.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2700.000
2	.070	---
	---	2720.000
3	.250	---

-----*
* Finished Processing Header Record HA *
-----*

14/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

* Starting To Process Header Record LOBR *

XS LOBR 25900
GR 0.0, 65.00 1400, 60.00 1750, 55.00 2250, 54.00 2700, 51
GR 2705, 46.00 2710, 46.00 2720, 51.00 3420, 55.00 3720, 60.0
GR 4100, 63.00
SA 2700 2720
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record LOBR ***
*** Storing X-Section Data In Temporary File As Record Number 9 ***

*** Data Summary For Header Record LOBR ***
SRD Location: 25900. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	65.000	1400.000	60.000	1750.000	55.000
2250.000	54.000	2700.000	51.000	2705.000	46.000
2710.000	46.000	2720.000	51.000	3420.000	55.000
3720.000	60.000	4100.000	63.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 4100.000 (associated Y-Elevation: 63.000)
Minimum Y-Elevation: 46.000 (associated X-Station: 2710.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2700.000
2	.070	---
	---	2720.000
3	.250	---

* Finished Processing Header Record LOBR *

15/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record APPR *
-----*

XS APPR 26980, 0, 0.3, 0.1
GR 0.0, 65.00 1400, 60.00 1750, 56.00 2250, 53.00 3250, 52
GR 3260, 47.00 3265, 47.00 3270, 54.00 3470, 55.00 4220, 60.0
GR 6220, 65.00
SA 3250 . 3270
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record APPR ***
*** Storing X-Section Data In Temporary File As Record Number 10 ***

*** Data Summary For Header Record APPR ***
SRD Location: 26980. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .30 Contraction: .10

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	65.000	1400.000	60.000	1750.000	56.000
2250.000	53.000	3250.000	52.000	3260.000	47.000
3265.000	47.000	3270.000	54.000	3470.000	55.000
4220.000	60.000	6220.000	65.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 6220.000 (associated Y-Elevation: 65.000)
Minimum Y-Elevation: 47.000 (associated X-Station: 3265.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	3250.000
2	.070	---
	---	3270.000
3	.250	---

-----*
* Finished Processing Header Record APPR *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

-----*
HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record I *
-----*

XS I 31180
GR 0.0, 70.00 3800, 65.00 5200, 60.00 5600, 56.00 5620, 51
GR 5640, 51.00 5650, 56.00 6100, 59.00 6800, 60.00 7350, 65.0
GR 8750, 70.00
SA 5600 5650
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record I ***
*** Storing X-Section Data In Temporary File As Record Number 11 ***

*** Data Summary For Header Record I ***
SRD Location: 31180. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	70.000	3800.000	65.000	5200.000	60.000
5600.000	56.000	5620.000	51.000	5640.000	51.000
5650.000	56.000	6100.000	59.000	6800.000	60.000
7350.000	65.000	8750.000	70.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 70.000)
Maximum X-Station: 8750.000 (associated Y-Elevation: 70.000)
Minimum Y-Elevation: 51.000 (associated X-Station: 5640.000)
Maximum Y-Elevation: 70.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
		5600.000
2	.070	---
		5650.000
3	.250	---

-----*
* Finished Processing Header Record I *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record FULLV *
-----*

XS	FULLV 32188				
GR	0.0, 73.00	210, 74.30	360, 73.60	540, 73.00	1060, 72.80
GR	1440, 72.60	1860, 72.50	2080, 73.00	2410, 73.60	2440, 70.4
GR	2463, 60.10	2470, 58.60	2590, 55.90	2605, 51.20	2620, 51.4
GR	2628, 52.40	2650, 57.00	2725, 59.10	2755, 70.40	2890, 73.0
GR	3130, 72.00	3350, 71.0	3980, 70.0	5090, 70.00	5160, 71.0
GR	5320, 72.00	5520, 74.00			
SA	2440 2755				

*** Completed Reading Data Associated With Header Record FULLV ***
*** Storing X-Section Data In Temporary File As Record Number 12 ***

*** Data Summary For Header Record FULLV ***
SRD Location: 32188. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (27 pairs)

X	Y	X	Y	X	Y
.000	73.000	210.000	74.300	360.000	73.600
540.000	73.000	1060.000	72.800	1440.000	72.600
1860.000	72.500	2080.000	73.000	2410.000	73.600
2440.000	70.400	2463.000	60.100	2470.000	58.600
2590.000	55.900	2605.000	51.200	2620.000	51.400
2628.000	52.400	2650.000	57.000	2725.000	59.100
2755.000	70.400	2890.000	73.000	3130.000	72.000
3350.000	71.000	3980.000	70.000	5090.000	70.000
5160.000	71.000	5320.000	72.000	5520.000	74.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 73.000)
Maximum X-Station: 5520.000 (associated Y-Elevation: 74.000)
Minimum Y-Elevation: 51.200 (associated X-Station: 2605.000)
Maximum Y-Elevation: 74.300 (associated X-Station: 210.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2440.000
2	.070	---
	---	2755.000
3	.250	---

-----*
* Finished Processing Header Record FULLV *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record SR39 *
-----*

BR SR39 32188, 70.0, 0.0, 0.5, 0.3
GR 2410.0, 73.6 2490, 70.40 2500, 66.40 2518, 56.30 2590, 55.9
GR 2605, 51.20 2620, 51.40 2628, 52.40 2650, 57.00 2664, 57.4
GR 2680, 65.10 2690, 70.00 2441, 70.00 2410, 73.60
SA 2518 2664
N 0.05 0.03 0.05
CD 3, 105, 2, 69.70
PD 1 53.2,1.5, 1 56.4, 3.0, 1 57.8, 4.50, 1

*** Completed Reading Data Associated With Header Record SR39 ***
*** Storing Bridge Data In Temporary File As Record Number 13 ***

*** Data Summary For Bridge Record SR39 ***
SRD Location: 32188. Cross-Section Skew: .0 Error Code 0
Valley Slope: ***** Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .30

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
2410.000	73.600	2490.000	70.400	2500.000	66.400
2518.000	56.300	2590.000	55.900	2605.000	51.200
2620.000	51.400	2628.000	52.400	2650.000	57.000
2664.000	57.400	2680.000	65.100	2690.000	70.000
2441.000	70.000	2410.000	73.600		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: 2410.000 (associated Y-Elevation: 73.600)
Maximum X-Station: 2690.000 (associated Y-Elevation: 70.000)
Minimum Y-Elevation: 51.200 (associated X-Station: 2605.000)
Maximum Y-Elevation: 73.600 (associated X-Station: 2410.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.050	---
	---	2518.000
2	.030	---
	---	2664.000
3	.050	---

Discharge coefficient parameters
BRType BRWdth EMBSS EMBElv UserCD
3 105.000 2.00 69.700 *****

Pressure flow elevations
AVBCEL PFElev
***** 70.000

Abutment Parameters

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ABSLPL ABSLPR XTOELT YTOELT XTOERT YTOERT

Pier/Pile Data (3 Group(s))
Code Indicates Bridge Uses Piles

Group	Elevation	Gross Width	Number
1	53.200	1.500	1
2	56.400	3.000	1
3	57.800	4.500	1

* Finished Processing Header Record SR39 *

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

-----*
HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record ROAD *
-----*

XR ROAD 32238, 105, 1
GR 0.0, 74.30 1860, 72.50 2410, 73.60 2440, 72.00 2755, 72.00

*** Completed Reading Data Associated With Header Record ROAD ***
*** Storing Roadway Data In Temporary File As Record Number 14 ***

*** Data Summary For Roadway Record ROAD ***
SRD Location: 32238. Cross-Section Skew: .0 Error Code 0
Roadway Width: 105.000 User-Specified Weir Coefficient: *****
Input Code Indicates Roadway Surface Consists of a Paved Material.

X,Y-coordinates (5 pairs)

X	Y	X	Y	X	Y
.000	74.300	1860.000	72.500	2410.000	73.600
2440.000	72.000	2755.000	72.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 74.300)
Maximum X-Station: 2755.000 (associated Y-Elevation: 72.000)
Minimum Y-Elevation: 72.000 (associated X-Station: 2755.000)
Maximum Y-Elevation: 74.300 (associated X-Station: .000)

Bridge datum projection: XREFLT = *****

-----*
* Finished Processing Header Record ROAD *
-----*

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***** W S P R O *****
 Federal Highway Administration - U. S. Geological Survey
 Model for Water-Surface Profile Computations.
 Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
 LOCATION HYDRAULICS STUDY
 50 AND 100 YR. FLOOD

-----*
 * Starting To Process Header Record UP39 *
 -----*

AS UP39 32470, 0.0, 0.5, 0.1
 +++078 NOTICE: AS Record Replaced With XS Record (See Users Manual).
 GR 0.0, 70.0 125, 69.00 240, 66.0 420, 66.00 640, 67.00
 GR 640, 67.00 830, 66.00 1040, 66.00 1090, 67.00 1250, 68.00
 GR 1285, 69.00 1325, 69.00 1360, 68.0 1410, 68.00 1470, 69.0
 GR 1640, 69.00 1710, 68.00 2190, 68.00 2290, 64.00 2580, 62.0
 GR 2780, 58.00 2805, 58.00 2830, 59.0 2850, 56.00 2860, 51.4
 GR 2875, 51.40 2880, 56.00 2900, 59.0 3690, 63.00 3750, 65.0
 GR 3830, 66.00 4290, 74.00
 SA 2830 2900
 N 0.25, 0.07, 0.25

*** Completed Reading Data Associated With Header Record UP39 ***
 *** Storing X-Section Data In Temporary File As Record Number 15 ***

*** Data Summary For Header Record UP39 ***
 SRD Location: 32470. Cross-Section Skew: .0 Error Code 0
 Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
 Energy Loss Coefficients -> Expansion: .50 Contraction: .10

X,Y-coordinates (32 pairs)					
X	Y	X	Y	X	Y
.000	70.000	125.000	69.000	240.000	66.000
420.000	66.000	460.000	67.000	640.000	67.000
830.000	66.000	1040.000	66.000	1090.000	67.000
1250.000	68.000	1285.000	69.000	1325.000	69.000
1360.000	68.000	1410.000	68.000	1470.000	69.000
1640.000	69.000	1710.000	68.000	2190.000	68.000
2290.000	64.000	2580.000	62.000	2780.000	58.000
2805.000	58.000	2830.000	59.000	2850.000	56.000
2860.000	51.400	2875.000	51.400	2880.000	56.000
2900.000	59.000	3690.000	63.000	3750.000	65.000
3830.000	66.000	4290.000	74.000		

Minimum and Maximum X,Y-coordinates
 Minimum X-Station: .000 (associated Y-Elevation: 70.000)
 Maximum X-Station: 4290.000 (associated Y-Elevation: 74.000)
 Minimum Y-Elevation: 51.400 (associated X-Station: 2875.000)
 Maximum Y-Elevation: 74.000 (associated X-Station: 4290.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2830.000
2	.070	---
	---	2900.000
3	.250	---

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Bridge datum projection(s): XREFLT XREFRT FDSTLT FDSTRT

* Finished Processing Header Record UP39 *

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record L *

XS	L	32765				
GR		0.0, 68.00	180, 65.00	470, 65.00	640, 63.00	940, 63.00
GR		960, 65.00	1070, 69.00	1100, 69.00	1170, 67.00	1430, 65.00
GR		1820, 65.00	1840, 68.00	1920, 68.0	2494, 58.30	2533, 57.7
GR		2539, 56.40	2545, 57.60	2703, 58.2	2726, 52.70	2751, 53.1
GR		2755, 55.70	2772, 59.10	2780, 55.6	2799, 56.30	2842, 59.2
GR		2862, 55.80	2881, 58.00	2908, 58.6	2932, 54.90	2960, 60.0
GR		3020, 61.00	3835, 65.00	4160, 74.00		
SA		2725	2842			

*** Completed Reading Data Associated With Header Record L ***
*** Storing X-Section Data In Temporary File As Record Number 16 ***

*** Data Summary For Header Record L ***
SRD Location: 32765. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (33 pairs)

X	Y	X	Y	X	Y
.000	68.000	180.000	65.000	470.000	65.000
640.000	63.000	940.000	63.000	960.000	65.000
1070.000	69.000	1100.000	69.000	1170.000	67.000
1430.000	65.000	1820.000	65.000	1840.000	68.000
1920.000	68.000	2494.000	58.300	2533.000	57.700
2539.000	56.400	2545.000	57.600	2703.000	58.200
2726.000	52.700	2751.000	53.100	2755.000	55.700
2772.000	59.100	2780.000	55.600	2799.000	56.300
2842.000	59.200	2862.000	55.800	2881.000	58.000
2908.000	58.600	2932.000	54.900	2960.000	60.000
3020.000	61.000	3835.000	65.000	4160.000	74.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 68.000)
Maximum X-Station: 4160.000 (associated Y-Elevation: 74.000)
Minimum Y-Elevation: 52.700 (associated X-Station: 2726.000)
Maximum Y-Elevation: 74.000 (associated X-Station: 4160.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2725.000
2	.070	---
	---	2842.000
3	.250	---

-----*
* Finished Processing Header Record L *

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record UPXS1 *
-----*

XS UPXS1 33025 * * * 0.0004

*** Completed Reading Data Associated With Header Record UPXS1 ***
*** No Roughness Data Input, Propagating From Previous Section ***
*** Storing X-Section Data In Temporary File As Record Number 17 ***

*** Data Summary For Header Record UPXS1 ***
SRD Location: 33025. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00040 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (33 pairs)					
X	Y	X	Y	X	Y
.000	68.104	180.000	65.104	470.000	65.104
640.000	63.104	940.000	63.104	960.000	65.104
1070.000	69.104	1100.000	69.104	1170.000	67.104
1430.000	65.104	1820.000	65.104	1840.000	68.104
1920.000	68.104	2494.000	58.404	2533.000	57.804
2539.000	56.504	2545.000	57.704	2703.000	58.304
2726.000	52.804	2751.000	53.204	2755.000	55.804
2772.000	59.204	2780.000	55.704	2799.000	56.404
2842.000	59.304	2862.000	55.904	2881.000	58.104
2908.000	58.704	2932.000	55.004	2960.000	60.104
3020.000	61.104	3835.000	65.104	4160.000	74.104

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 68.104)
Maximum X-Station: 4160.000 (associated Y-Elevation: 74.104)
Minimum Y-Elevation: 52.804 (associated X-Station: 2726.000)
Maximum Y-Elevation: 74.104 (associated X-Station: 4160.000)

Roughness Data (3 SubAreas)		
SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2725.000
2	.070	---
	---	2842.000
3	.250	---

-----*
* Finished Processing Header Record UPXS1 *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

-----*
HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

EX

* Summary of Boundary Condition Information *

#	Reach Discharge	Water Surface Elevation	Friction Slope	Flow Regime
1	4130.00	50.750	*****	Sub-Critical
2	4890.00	51.740	*****	Sub-Critical

* Beginning 2 Profile Calculation(s) *

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***** W S P R O *****
 Federal Highway Administration - U. S. Geological Survey
 Model for Water-Surface Profile Computations.
 Input Units: English / Output Units: English

-----*
 HILLSBOROUGH RIVER, SR 39
 LOCATION HYDRAULICS STUDY
 50 AND 100 YR. FLOOD

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: B1	50.750	.003	4130.000	24086.250	*****	3430.000
Header Type: XS	50.753	*****	.171	499312.80	*****	8140.000
SRD: 3450.000	41.635	*****	.036	*****	7.229	*****
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " C "						
KRATIO: .59						
Section: C	51.162	.011	4130.000	13811.520	3550.000	2037.283
Header Type: XS	51.173	.413	.299	293342.50	3550.000	4836.227
SRD: 7000.000	39.359	.004	.067	.0001	8.017	.003
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " D "						
KRATIO: .47						
Section: D	52.492	.036	4130.000	7595.759	3200.000	2825.383
Header Type: XS	52.528	1.336	.544	139229.00	3200.000	4848.009
SRD: 10200.000	48.394	.012	.138	.0004	7.835	.006
Section: E	54.696	.023	4130.000	8711.233	3000.000	2021.269
Header Type: XS	54.719	2.178	.474	168761.60	3000.000	3884.423
SRD: 13200.000	48.851	.000	.098	.0007	6.487	.013
Section: F	56.152	.029	4130.000	8695.945	3000.000	538.711
Header Type: XS	56.181	1.453	.475	208668.30	3000.000	2322.810
SRD: 16200.000	34.634	.003	.108	.0005	8.169	.006
Section: G	56.896	.007	4130.000	13638.500	2300.000	702.850
Header Type: XS	56.903	.712	.303	263974.60	2300.000	3492.697
SRD: 18500.000	51.417	.000	.053	.0003	4.884	.010
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " H "						
KRATIO: .59						
Section: H	57.730	.023	4130.000	8695.275	2000.000	481.632
Header Type: XS	57.753	.831	.475	155548.80	2000.000	2564.032
SRD: 20500.000	53.248	.008	.106	.0004	6.641	.011
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "HA "						
KRATIO: 1.58						
Section: HA	59.800	.006	4130.000	12429.960	4600.000	1414.035
Header Type: XS	59.805	2.051	.332	245958.50	4600.000	3707.970
SRD: 25100.000	54.359	.000	.045	.0004	3.258	.001
Section: LOBR	60.019	.005	4130.000	12935.770	800.000	1394.786
Header Type: XS	60.024	.214	.319	259805.70	800.000	3722.358
SRD: 25900.000	54.359	.000	.043	.0003	3.190	.005
Section: APPR	60.270	.003	4130.000	14928.190	1080.000	1324.447
Header Type: XS	60.273	.249	.277	284889.40	1080.000	4327.933
SRD: 26980.000	54.229	.000	.035	.0002	2.546	.000
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "I "						

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KRATIO: .44

Section: I	62.243	.056	4130.000	7218.647	4200.000	4572.097
Header Type: XS	62.299	1.997	.572	125931.30	4200.000	7046.676
SRD: 31180.000	58.740	.027	.196	.0005	*****	.002

Section: FULLV	63.290	.083	4130.000	1786.210	1008.000	2455.876
Header Type: FV	63.374	1.055	2.312	129452.90	1008.000	2736.125
SRD: 32188.000	58.427	.013	.161	.0010	1.000	.007

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "UP39 ".

KRATIO: .67

Section: UP39	63.691	.146	4130.000	3931.946	282.000	2334.862
Header Type: AS	63.836	.429	1.050	86511.63	282.000	3710.718
SRD: 32470.000	60.490	.031	.319	.0015	8.497	.002

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>

<<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: SR39	64.088	.184	4130.000	1425.954	1008.000	2504.121
Header Type: BR	64.271	1.882	2.896	290587.00	1008.000	2677.896
SRD: 32188.000	57.991	.090	.212	*****	1.409	-.012

Specific Bridge Information	C	P/A	PFELEV	BLEN	XLAB	XRAB
Bridge Type 3	Flow Type 1					
Pier/Pile Code	1	.8426	.029	70.000	*****	*****

*** Roadway Section Located at SRD 32238.000 ***

Section: ROAD Header Type: XR
<<< Embankment Is Not Overtopped >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: UP39	64.712	.072	4130.000	5397.853	177.000	2272.204
Header Type: AS	64.784	.487	.765	123400.10	257.524	3741.355
SRD: 32470.000	60.490	.024	.198	.0015	7.889	-.020

Approach Section UP39	Flow	Contraction	Information
M(G)	M(K)	KQ	XLKQ XRKQ OTEL
.876	.416	72560.9	2770.493 2944.315 64.516

<<< End of Bridge Hydraulics Computations >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " L ".

KRATIO: 1.43

Section: L	64.986	.036	4130.000	7611.293	295.000	471.156
Header Type: XS	65.023	.232	.543	176129.40	295.000	3832.230
SRD: 32765.000	59.192	.000	.146	.0008	7.967	.008

* EXISTING
CONDITIONS
BACKWATER
ELEVATION
FOR THE
50-YEAR
STORM
EVENT

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Section: UPXS1	65.134	.045	4130.000	7727.777	260.000	178.223
Header Type: XS	65.179	.153	.534	164729.30	260.000	3836.070
SRD: 33025.000	59.296	.004	.184	.0006	*****	-.001

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***** W S P R O *****
 Federal Highway Administration - U. S. Geological Survey
 Model for Water-Surface Profile Computations.
 Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
 LOCATION HYDRAULICS STUDY
 50 AND 100 YR. FLOOD

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: B1	51.740	.003	4890.000	29082.400	*****	3073.599
Header Type: XS	51.743	*****	.168	609721.80	*****	8456.801
SRD: 3450.000	42.018	*****	.034	*****	6.988	*****
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " C "						
KRATIO: .60						
Section: C	52.119	.010	4890.000	16601.300	3550.000	1903.328
Header Type: XS	52.129	.382	.295	364248.30	3550.000	4962.872
SRD: 7000.000	39.995	.003	.060	.0001	7.314	.000
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " D "						
KRATIO: .49						
Section: D	53.308	.031	4890.000	9348.840	3200.000	2784.596
Header Type: XS	53.340	1.186	.523	177166.00	3200.000	5060.103
SRD: 10200.000	48.643	.011	.124	.0004	7.397	.014
Section: E	55.423	.025	4890.000	10176.030	3000.000	1830.920
Header Type: XS	55.448	2.121	.481	190869.20	3000.000	4104.998
SRD: 13200.000	49.204	.000	.107	.0007	7.089	-.013
Section: F	56.966	.028	4890.000	10243.430	3000.000	424.809
Header Type: XS	56.994	1.541	.477	243964.50	3000.000	2444.847
SRD: 16200.000	36.823	.001	.105	.0005	7.936	.004
Section: G	57.683	.007	4890.000	15888.990	2300.000	620.967
Header Type: XS	57.690	.694	.308	324832.20	2300.000	3547.811
SRD: 18500.000	51.615	.000	.049	.0003	4.420	.002
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " H "						
KRATIO: .59						
Section: H	58.451	.021	4890.000	10262.360	2000.000	423.928
Header Type: XS	58.472	.772	.476	190681.50	2000.000	2686.654
SRD: 20500.000	53.533	.007	.097	.0004	6.018	.003
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "HA "						
KRATIO: 1.49						
Section: HA	60.507	.006	4890.000	14122.200	4600.000	1257.909
Header Type: XS	60.514	2.028	.346	284473.00	4600.000	3784.280
SRD: 25100.000	54.680	.000	.047	.0004	3.249	.014
Section: LOBR	60.734	.006	4890.000	14706.230	800.000	1194.341
Header Type: XS	60.740	.226	.333	296991.90	800.000	3813.036
SRD: 25900.000	54.680	.000	.045	.0003	3.265	.000
Section: APPR	61.001	.003	4890.000	17306.280	1080.000	1119.698
Header Type: XS	61.004	.263	.283	330533.90	1080.000	4620.432
SRD: 26980.000	54.391	.000	.036	.0002	2.630	.001
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "I "						

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KRATIO: .48

Section: I	62.897	.047	4890.000	8921.246	4200.000	4388.893
Header Type: XS	62.944	1.901	.548	159820.10	4200.000	7118.649
SRD: 31180.000	59.003	.022	.170	.0005	*****	.017

Section: FULLV	63.887	.097	4890.000	1954.229	1008.000	2454.544
Header Type: FV	63.984	1.010	2.502	149272.20	1008.000	2737.708
SRD: 32188.000	58.728	.025	.168	.0010	1.000	.005

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

Section: UP39	64.296	.133	4890.000	4791.732	282.000	2282.599
Header Type: AS	64.429	.421	1.021	107231.50	282.000	3728.881
SRD: 32470.000	60.973	.018	.284	.0015	8.227	.006

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>
<<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: SR39	64.684	.233	4890.000	1530.347	1008.000	2503.057
Header Type: BR	64.917	1.832	3.195	323914.70	1008.000	2679.136
SRD: 32188.000	58.346	.140	.231	*****	1.467	-.010

Specific Bridge Information	C	P/A	PFELEV	BLEN	XLAB	XRAB
Bridge Type 3	Flow Type 1					
Pier/Pile Code 1	.8255	.028	70.000	*****	*****	*****

*** Roadway Section Located at SRD 32238.000 ***

Section: ROAD Header Type: XR
<<< Embankment Is Not Overtopped >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: UP39	65.372	.068	4890.000	6382.466	177.000	2255.712
Header Type: AS	65.440	.495	.766	150715.90	257.965	3779.722
SRD: 32470.000	60.973	.027	.181	.0015	7.480	-.016

Approach Section UP39	Flow	Contraction	Information		
M(G)	M(K)	KQ	XLKQ	XRKQ	OTEL
.880	.456	82307.8	2771.269	2947.385	65.187

<<< End of Bridge Hydraulics Computations >>>

Section: L	65.630	.040	4890.000	9535.148	295.000	142.229
Header Type: XS	65.670	.229	.513	204632.90	295.000	3857.732
SRD: 32765.000	59.403	.000	.162	.0008	9.828	.001

Section: UPXS1	65.780	.039	4890.000	9678.994	260.000	139.459
Header Type: XS	65.819	.146	.505	207921.30	260.000	3859.400
SRD: 33025.000	59.507	.000	.158	.0006	9.800	.003

ER

* EXISTING
CONDITIONS
BACKWATER
ELEVATION
FOR 100-
YEAR STORM
EVENT

31/31

***** Normal end of WSPRO execution. *****
***** Elapsed Time: 0 Minutes 4 Seconds *****

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET 1 OF 3 / PROJ. NO. C100003240.19
DESCRIPTION: VII.E. WSPRO ANALYSIS. COMPUTED BY: Zinner DATE: 5-27-99
PROPOSED CONDITIONS CHECKED BY: Pratt DATE: 5-28-99

The WSPRO analyses were conducted considering the case of proposed conditions "with new proposed bridge." This section includes the WSPRO input and output for the analysis of 50- and 100-year storm events for the proposed conditions.

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PROPOSED CONDITIONS

ANALYSIS INPUT

T1 HILLSBOROUGH RIVER, SR 39
T2 LOCATION HYDRAULICS STUDY
T3 50 AND 100 YR. FLOOD
* J3 1
Q 4130 4890
WS 50.75 51.74
*
XS B1 3450
GR 0.0, 60.00 1900, 55.00 3700, 50.00 4200, 45.00 4400, 43.00
GR 5100, 39.00 5180, 37.00 5195, 33.00 5200, 33.00 5220, 38.00
GR 5250, 39.00 5270, 40.00 5570, 43.0 6000, 45.00 7900, 50.0
GR 9500, 55.00 13570, 60.00
SA 5180 5220
N 0.25 0.07 0.25
XS C 7000
GR 0.0, 60.00 1500, 55.00 2200, 50.00 3300, 45.00 3350, 41.00
GR 3390, 40.00 3405, 35.00 3410, 35.00 3420, 30.00 3540, 43.00
GR 4178, 45.00 4720, 50.00 4920, 52.00 6000, 55.00 9000, 60.00
SA 3390 3420
N 0.25 0.07 0.25
*
XS D 10200
GR 0.0, 60.00 2300, 55.00 2750, 54.00 2950, 50.00 3380, 45.00
GR 3400, 44.00 3415, 39.00 3420, 39.00 3440, 44.00 3470, 46.00
GR 4020, 48.00 4200, 50.00 5500, 55.0 7550, 60.0
SA 3380 3420
*
XS E 13200
GR 0.0, 60.00 2000, 55.00 2350, 50.00 2600, 45.00 2620, 44.00
GR 2625, 39.0 2630, 39.00 2640, 44.00 2680, 45.00 3180, 50.00
GR 3930, 55.00 6000, 60.0
SA 2620 2640
*
XS F 16200
GR 0.0, 60.00 700, 55.00 1000, 50.00 1079, 48.00 1080, 47.00
GR 1095, 42.0 1100, 42.00 1110, 47.00 1170, 48.00 1750, 50.00
GR 2150, 55.00 2900, 60.0
SA 1080 1110
*
XS G 18500
GR 0.0, 65.00 380, 60.00 900, 55.00 1100, 51.00 1800, 50.00
GR 1810, 49.00 1960, 48.00 1970, 43.00 1975, 43.00 1990, 48.00
GR 2240, 49.00 2260, 50.00 2860, 54.0 3360, 55.00 4060, 65.0

SA 1960 1990

*

XS H 20500

GR 0.0, 62.50 300, 60.00 700, 55.0 1270, 50.00 1280, 49.00
 GR 1300, 48.00 1305, 43.00 1310, 43.00 1320, 48.00 1350, 49.00
 GR 1370, 50.00 2100, 55.00 2950, 60.0 5400, 65.00
 SA 1300 1320

*

XS HA 25100

GR 0.0, 65.00 1400, 60.00 1750, 55.00 2250, 54.00 2700, 51.00
 GR 2705, 46.00 2710, 46.00 2720, 51.00 3420, 55.00 3720, 60.00
 GR 4100, 63.00
 SA 2700 2720

*

XS LOBR 25900

GR 0.0, 65.00 1400, 60.00 1750, 55.00 2250, 54.00 2700, 51.00
 GR 2705, 46.00 2710, 46.00 2720, 51.00 3420, 55.00 3720, 60.00
 GR 4100, 63.00
 SA 2700 2720

N 0.25 0.07 0.25

*

XS APPR 26980, 0, 0.3, 0.1

GR 0.0, 65.00 1400, 60.00 1750, 56.00 2250, 53.00 3250, 52.00
 GR 3260, 47.00 3265, 47.00 3270, 54.00 3470, 55.00 4220, 60.00
 GR 6220, 65.00
 SA 3250 3270

N 0.25 0.07 0.25

*

XS I 31180

GR 0.0, 70.00 3800, 65.00 5200, 60.00 5600, 56.00 5620, 51.00
 GR 5640, 51.00 5650, 56.00 6100, 59.00 6800, 60.00 7350, 65.00
 GR 8750, 70.00
 SA 5600 5650

N 0.25 0.07 0.25

*

XS FULLV 32188

GR 0.0, 73.00 210, 74.30 360, 73.60 540, 73.00 1060, 72.80
 GR 1440, 72.60 1860, 72.50 2080, 73.00 2410, 73.60 2440, 70.40
 GR 2463, 60.10 2470, 58.60 2590, 55.90 2605, 51.20 2620, 51.40
 GR 2628, 52.40 2650, 57.00 2725, 59.10 2755, 70.40 2890, 73.0

GR 3130, 72.00 3350, 71.0 3980, 70.0 5090, 70.00 5160, 71.0

GR 5320, 72.00 5520, 74.00

SA 2440 2755

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*

BR SR39 32188, 70.0, 0.0, 0.5, 0.3
GR 2410.0, 73.6 2490, 70.40 2500, 66.40 2518, 56.30 2590, 55.90
GR 2605, 51.20 2620, 51.40 2628, 52.40 2650, 57.00 2664, 57.40
GR 2680, 65.10 2690, 70.00 2441, 70.00 2410, 73.60
SA 2518 2664
N 0.05 0.03 0.05
CD 3, 117, 2, 69.70
PD 1 53.2, 1.5, 1 56.4, 3.0, 1 57.8, 4.50, 1

*

XR ROAD 32238, 105, 1
GR 0.0, 74.30 1860, 72.50 2410, 73.60 2440, 72.00 2755, 72.00

*

AS UP39 32470, 0.0, 0.5, 0.1
GR 0.0, 70.0 125, 69.00 240, 66.0 420, 66.00 460, 67.00
GR 640, 67.00 830, 66.00 1040, 66.00 1090, 67.00 1250, 68.00
GR 1285, 69.00 1325, 69.00 1360, 68.0 1410, 68.00 1470, 69.0
GR 1640, 69.00 1710, 68.00 2190, 68.00 2290, 64.00 2580, 62.00
GR 2780, 58.00 2805, 58.00 2830, 59.0 2850, 56.00 2860, 51.4
GR 2875, 51.40 2880, 56.00 2900, 59.0 3690, 63.00 3750, 65.00
GR 3830, 66.00 4290, 74.00
SA 2830 2900
N 0.25, 0.07, 0.25

*

XS L 32765
GR 0.0, 68.00 180, 65.00 470, 65.00 640, 63.00 940, 63.00
GR 960, 65.00 1070, 69.00 1100, 69.00 1170, 67.00 1430, 65.00
GR 1820, 65.00 1840, 68.00 1920, 68.0 2494, 58.30 2533, 57.7
GR 2539, 56.40 2545, 57.60 2703, 58.2 2726, 52.70 2751, 53.10
GR 2755, 55.70 2772, 59.10 2780, 55.6 2799, 56.30 2842, 59.2
GR 2862, 55.80 2881, 58.00 2908, 58.6 2932, 54.90 2960, 60.00
GR 3020, 61.00 3835, 65.00 4160, 74.00
SA 2725 2842
XS UPXS1 33025 * * * 0.0004
EX
ER

PROPOSED CONDITIONS ANALYSIS OUTPUT 5/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Run Date & Time: 3/ 4/99 3:19 pm Version V050196
Input File: sr39tx2.inp9 Output File: sr39tx2.LST9

T1 HILLSBOROUGH RIVER, SR 39
T2 LOCATION HYDRAULICS STUDY
T3 50 AND 100 YR. FLOOD
Q 4130 4890

*** Processing Flow Data; Placing Information into Sequence 1 ***

WS 50.75 51.74

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record B1 *
-----*

XS B1 3450
GR 0.0, 60.00 1900, 55.00 3700, 50.00 4200, 45.00 4400, 43
GR 5100, 39.00 5180, 37.00 5195, 33.00 5200, 33.00 5220, 38.0
GR 5250, 39.00 5270, 40.00 5570, 43.0 6000, 45.00 7900, 50.
GR 9500, 55.00 13570, 60.00
SA 5180 5220
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record B1 ***
*** Storing X-Section Data In Temporary File As Record Number 1 ***

*** Data Summary For Header Record B1 ***
SRD Location: 3450. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (17 pairs)

X	Y	X	Y	X	Y
.000	60.000	1900.000	55.000	3700.000	50.000
4200.000	45.000	4400.000	43.000	5100.000	39.000
5180.000	37.000	5195.000	33.000	5200.000	33.000
5220.000	38.000	5250.000	39.000	5270.000	40.000
5570.000	43.000	6000.000	45.000	7900.000	50.000
9500.000	55.000	13570.000	60.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 13570.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 33.000 (associated X-Station: 5200.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
		5180.000
2	.070	---
		5220.000
3	.250	---

-----*
* Finished Processing Header Record B1 *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record C *
-----*

XS C 7000
GR 0.0, 60.00 1500, 55.00 2200, 50.00 3300, 45.00 3350, 41.0
GR 3390, 40.00 3405, 35.00 3410, 35.00 3420, 30.00 3540, 43.0
GR 4178, 45.00 4720, 50.00 4920, 52.00 6000, 55.00 9000, 60.0
SA 3390 3420
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record C ***
*** Storing X-Section Data In Temporary File As Record Number 2 ***

*** Data Summary For Header Record C ***
SRD Location: 7000. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (15 pairs)

X	Y	X	Y	X	Y
.000	60.000	1500.000	55.000	2200.000	50.000
3300.000	45.000	3350.000	41.000	3390.000	40.000
3405.000	35.000	3410.000	35.000	3420.000	30.000
3540.000	43.000	4178.000	45.000	4720.000	50.000
4920.000	52.000	6000.000	55.000	9000.000	60.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 9000.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 30.000 (associated X-Station: 3420.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	3390.000
2	.070	---
	---	3420.000
3	.250	---

-----*
* Finished Processing Header Record C *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

-----*
HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record D *
-----*

XS D 10200
GR 0.0, 60.00 2300, 55.00 2750, 54.00 2950, 50.00 3380, 45
GR 3400, 44.00 3415, 39.00 3420, 39.00 3440, 44.00 3470, 46.0
GR 4020, 48.00 4200, 50.00 5500, 55.0 7550, 60.0
SA 3380 3420

*** Completed Reading Data Associated With Header Record D ***
*** Storing X-Section Data In Temporary File As Record Number 3 ***

*** Data Summary For Header Record D ***
SRD Location: 10200. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
.000	60.000	2300.000	55.000	2750.000	54.000
2950.000	50.000	3380.000	45.000	3400.000	44.000
3415.000	39.000	3420.000	39.000	3440.000	44.000
3470.000	46.000	4020.000	48.000	4200.000	50.000
5500.000	55.000	7550.000	60.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 7550.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 39.000 (associated X-Station: 3420.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	3380.000
2	.070	---
	---	3420.000
3	.250	---

-----*
* Finished Processing Header Record D *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

-----*
HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record E *
-----*

XS E 13200
GR 0.0, 60.00 2000, 55.00 2350, 50.00 2600, 45.00 2620, 44
GR 2625, 39.0 2630, 39.00 2640, 44.00 2680, 45.00 3180, 50.
GR 3930, 55.00 6000, 60.0
SA 2620 2640

*** Completed Reading Data Associated With Header Record E ***
*** Storing X-Section Data In Temporary File As Record Number 4 ***

*** Data Summary For Header Record E ***
SRD Location: 13200. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (12 pairs)

X	Y	X	Y	X	Y
.000	60.000	2000.000	55.000	2350.000	50.000
2600.000	45.000	2620.000	44.000	2625.000	39.000
2630.000	39.000	2640.000	44.000	2680.000	45.000
3180.000	50.000	3930.000	55.000	6000.000	60.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 6000.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 39.000 (associated X-Station: 2630.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2620.000
2	.070	---
	---	2640.000
3	.250	---

-----*
* Finished Processing Header Record E *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

-----*
HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record F *
-----*

XS F 16200
GR 0.0, 60.00 700, 55.00 1000, 50.00 1079, 48.00 1080, 4
GR 1095, 42.0 1100, 42.00 1110, 47.00 1170, 48.00 1750, 50.
GR 2150, 55.00 2900, 60.0
SA 1080 1110

*** Completed Reading Data Associated With Header Record F ***
*** Storing X-Section Data In Temporary File As Record Number 5 ***

*** Data Summary For Header Record F ***
SRD Location: 16200. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (12 pairs)

X	Y	X	Y	X	Y
.000	60.000	700.000	55.000	1000.000	50.000
1079.000	48.000	1080.000	4.000	1095.000	42.000
1100.000	42.000	1110.000	47.000	1170.000	48.000
1750.000	50.000	2150.000	55.000	2900.000	60.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 60.000)
Maximum X-Station: 2900.000 (associated Y-Elevation: 60.000)
Minimum Y-Elevation: 4.000 (associated X-Station: 1080.000)
Maximum Y-Elevation: 60.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	1080.000
2	.070	---
	---	1110.000
3	.250	---

-----*
* Finished Processing Header Record F *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

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HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record G *
-----*

XS G 18500
GR 0.0, 65.00 380, 60.00 900, 55.00 1100, 51.00 1800, 50.
GR 1810, 49.00 1960, 48.00 1970, 43.00 1975, 43.00 1990, 48.0
GR 2240, 49.00 2260, 50.00 2860, 54.0 3360, 55.00 4060, 65.0
SA 1960 1990

*** Completed Reading Data Associated With Header Record G ***
*** Storing X-Section Data In Temporary File As Record Number 6 ***

*** Data Summary For Header Record G ***
SRD Location: 18500. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (15 pairs)

X	Y	X	Y	X	Y
.000	65.000	380.000	60.000	900.000	55.000
1100.000	51.000	1800.000	50.000	1810.000	49.000
1960.000	48.000	1970.000	43.000	1975.000	43.000
1990.000	48.000	2240.000	49.000	2260.000	50.000
2860.000	54.000	3360.000	55.000	4060.000	65.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 4060.000 (associated Y-Elevation: 65.000)
Minimum Y-Elevation: 43.000 (associated X-Station: 1975.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	1960.000
2	.070	---
	---	1990.000
3	.250	---

-----*
* Finished Processing Header Record G *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record H *
-----*

XS H 20500
GR 0.0, 62.50 300, 60.00 700, 55.0 1270, 50.00 1280, 49
GR 1300, 48.00 1305, 43.00 1310, 43.00 1320, 48.00 1350, 49.0
GR 1370, 50.00 2100, 55.00 2950, 60.0 5400, 65.00
SA 1300 1320

*** Completed Reading Data Associated With Header Record H ***
*** Storing X-Section Data In Temporary File As Record Number 7 ***

*** Data Summary For Header Record H ***
SRD Location: 20500. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
.000	62.500	300.000	60.000	700.000	55.000
1270.000	50.000	1280.000	49.000	1300.000	48.000
1305.000	43.000	1310.000	43.000	1320.000	48.000
1350.000	49.000	1370.000	50.000	2100.000	55.000
2950.000	60.000	5400.000	65.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 62.500)
Maximum X-Station: 5400.000 (associated Y-Elevation: 65.000)
Minimum Y-Elevation: 43.000 (associated X-Station: 1310.000)
Maximum Y-Elevation: 65.000 (associated X-Station: 5400.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	1300.000
2	.070	---
	---	1320.000
3	.250	---

-----*
* Finished Processing Header Record H *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record HA *
-----*

XS HA 25100
GR 0.0, 65.00 1400, 60.00 1750, 55.00 2250, 54.00 2700, 51
GR 2705, 46.00 2710, 46.00 2720, 51.00 3420, 55.00 3720, 60.0
GR 4100, 63.00
SA 2700 2720

*** Completed Reading Data Associated With Header Record HA ***
*** Storing X-Section Data In Temporary File As Record Number 8 ***

*** Data Summary For Header Record HA ***
SRD Location: 25100. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	65.000	1400.000	60.000	1750.000	55.000
2250.000	54.000	2700.000	51.000	2705.000	46.000
2710.000	46.000	2720.000	51.000	3420.000	55.000
3720.000	60.000	4100.000	63.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 4100.000 (associated Y-Elevation: 63.000)
Minimum Y-Elevation: 46.000 (associated X-Station: 2710.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2700.000
2	.070	---
	---	2720.000
3	.250	---

-----*
* Finished Processing Header Record HA *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record LOBR *
-----*

XS LOBR 25900
GR 0.0, 65.00 1400, 60.00 1750, 55.00 2250, 54.00 2700, 51
GR 2705, 46.00 2710, 46.00 2720, 51.00 3420, 55.00 3720, 60.0
GR 4100, 63.00
SA 2700 . 2720
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record LOBR ***
*** Storing X-Section Data In Temporary File As Record Number 9 ***

*** Data Summary For Header Record LOBR ***
SRD Location: 25900. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	65.000	1400.000	60.000	1750.000	55.000
2250.000	54.000	2700.000	51.000	2705.000	46.000
2710.000	46.000	2720.000	51.000	3420.000	55.000
3720.000	60.000	4100.000	63.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 4100.000 (associated Y-Elevation: 63.000)
Minimum Y-Elevation: 46.000 (associated X-Station: 2710.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2700.000
2	.070	---
	---	2720.000
3	.250	---

-----*
* Finished Processing Header Record LOBR *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record APPR *
-----*

XS APPR 26980, 0, 0.3, 0.1
GR 0.0, 65.00 1400, 60.00 1750, 56.00 2250, 53.00 3250, 52
GR 3260, 47.00 3265, 47.00 3270, 54.00 3470, 55.00 4220, 60.0
GR 6220, 65.00
SA 3250 3270
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record APPR ***
*** Storing X-Section Data In Temporary File As Record Number 10 ***

*** Data Summary For Header Record APPR ***
SRD Location: 26980. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .30 Contraction: .10

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	65.000	1400.000	60.000	1750.000	56.000
2250.000	53.000	3250.000	52.000	3260.000	47.000
3265.000	47.000	3270.000	54.000	3470.000	55.000
4220.000	60.000	6220.000	65.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 65.000)
Maximum X-Station: 6220.000 (associated Y-Elevation: 65.000)
Minimum Y-Elevation: 47.000 (associated X-Station: 3265.000)
Maximum Y-Elevation: 65.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
		3250.000
2	.070	---
		3270.000
3	.250	---

-----*
* Finished Processing Header Record APPR *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record I *
-----*

XS I 31180
GR 0.0, 70.00 3800, 65.00 5200, 60.00 5600, 56.00 5620, 51
GR 5640, 51.00 5650, 56.00 6100, 59.00 6800, 60.00 7350, 65.0
GR 8750, 70.00
SA 5600 5650
N 0.25 0.07 0.25

*** Completed Reading Data Associated With Header Record I ***
*** Storing X-Section Data In Temporary File As Record Number 11 ***

*** Data Summary For Header Record I ***
SRD Location: 31180. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (11 pairs)

X	Y	X	Y	X	Y
.000	70.000	3800.000	65.000	5200.000	60.000
5600.000	56.000	5620.000	51.000	5640.000	51.000
5650.000	56.000	6100.000	59.000	6800.000	60.000
7350.000	65.000	8750.000	70.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 70.000)
Maximum X-Station: 8750.000 (associated Y-Elevation: 70.000)
Minimum Y-Elevation: 51.000 (associated X-Station: 5640.000)
Maximum Y-Elevation: 70.000 (associated X-Station: .000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	5600.000
2	.070	---
	---	5650.000
3	.250	---

-----*
* Finished Processing Header Record I *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record FULLV *
-----*

XS	FULLV 32188				
GR	0.0, 73.00	210, 74.30	360, 73.60	540, 73.00	1060, 72.80
GR	1440, 72.60	1860, 72.50	2080, 73.00	2410, 73.60	2440, 70.4
GR	2463, 60.10	2470, 58.60	2590, 55.90	2605, 51.20	2620, 51.4
GR	2628, 52.40	2650, 57.00	2725, 59.10	2755, 70.40	2890, 73.0
GR	3130, 72.00	3350, 71.0	3980, 70.0	5090, 70.00	5160, 71.0
GR	5320, 72.00	5520, 74.00			
SA	2440	2755			

*** Completed Reading Data Associated With Header Record FULLV ***
*** Storing X-Section Data In Temporary File As Record Number 12 ***

*** Data Summary For Header Record FULLV ***
SRD Location: 32188. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (27 pairs)					
X	Y	X	Y	X	Y
.000	73.000	210.000	74.300	360.000	73.600
540.000	73.000	1060.000	72.800	1440.000	72.600
1860.000	72.500	2080.000	73.000	2410.000	73.600
2440.000	70.400	2463.000	60.100	2470.000	58.600
2590.000	55.900	2605.000	51.200	2620.000	51.400
2628.000	52.400	2650.000	57.000	2725.000	59.100
2755.000	70.400	2890.000	73.000	3130.000	72.000
3350.000	71.000	3980.000	70.000	5090.000	70.000
5160.000	71.000	5320.000	72.000	5520.000	74.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 73.000)
Maximum X-Station: 5520.000 (associated Y-Elevation: 74.000)
Minimum Y-Elevation: 51.200 (associated X-Station: 2605.000)
Maximum Y-Elevation: 74.300 (associated X-Station: 210.000)

Roughness Data (3 SubAreas)		
SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2440.000
2	.070	---
	---	2755.000
3	.250	---

-----*
* Finished Processing Header Record FULLV *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record SR39 *
-----*

BR SR39 32188, 70.0, 0.0, 0.5, 0.3
GR 2410.0, 73.6 2490, 70.40 2500, 66.40 2518, 56.30 2590, 55.9
GR 2605, 51.20 2620, 51.40 2628, 52.40 2650, 57.00 2664, 57.4
GR 2680, 65.10 2690, 70.00 2441, 70.00 2410, 73.60
SA 2518 2664
N 0.05 0.03 0.05
CD 3, 117, 2, 69.70
PD 1 53.2,1.5, 1 56.4, 3.0, 1 57.8, 4.50, 1

*** Completed Reading Data Associated With Header Record SR39 ***
*** Storing Bridge Data In Temporary File As Record Number 13 ***

*** Data Summary For Bridge Record SR39 ***
SRD Location: 32188. Cross-Section Skew: .0 Error Code 0
Valley Slope: ***** Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .30

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
2410.000	73.600	2490.000	70.400	2500.000	66.400
2518.000	56.300	2590.000	55.900	2605.000	51.200
2620.000	51.400	2628.000	52.400	2650.000	57.000
2664.000	57.400	2680.000	65.100	2690.000	70.000
2441.000	70.000	2410.000	73.600		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: 2410.000 (associated Y-Elevation: 73.600)
Maximum X-Station: 2690.000 (associated Y-Elevation: 70.000)
Minimum Y-Elevation: 51.200 (associated X-Station: 2605.000)
Maximum Y-Elevation: 73.600 (associated X-Station: 2410.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.050	---
		2518.000
2	.030	---
		2664.000
3	.050	---

Discharge coefficient parameters
BRType BRWdth EMBSS EMBElv UserCD
3 117.000 2.00 69.700 *****

Pressure flow elevations
AVBCEL PFElev
***** 70.000

Abutment Parameters

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ABSLPL ABSLPR XTOELT YTOELT XTOERT YTOERT

Pier/Pile Data (3 Group(s))
Code Indicates Bridge Uses Piles

Group	Elevation	Gross Width	Number
1	53.200	1.500	1
2	56.400	3.000	1
3	57.800	4.500	1

* Finished Processing Header Record SR39 *

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

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HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record ROAD *
-----*

XR ROAD 32238, 105, 1
GR 0.0, 74.30 1860,72.50 2410,73.60 2440, 72.00 2755, 72.00

*** Completed Reading Data Associated With Header Record ROAD ***
*** Storing Roadway Data In Temporary File As Record Number 14 ***

*** Data Summary For Roadway Record ROAD ***
SRD Location: 32238. Cross-Section Skew: .0 Error Code 0
Roadway Width: 105.000 User-Specified Weir Coefficient: *****
Input Code Indicates Roadway Surface Consists of a Paved Material.

X,Y-coordinates (5 pairs)					
X	Y	X	Y	X	Y
.000	74.300	1860.000	72.500	2410.000	73.600
2440.000	72.000	2755.000	72.000		

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 74.300)
Maximum X-Station: 2755.000 (associated Y-Elevation: 72.000)
Minimum Y-Elevation: 72.000 (associated X-Station: 2755.000)
Maximum Y-Elevation: 74.300 (associated X-Station: .000)

Bridge datum projection: XREFLT = *****

-----*
* Finished Processing Header Record ROAD *
-----*

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***** W S P R O *****
 Federal Highway Administration - U. S. Geological Survey
 Model for Water-Surface Profile Computations.
 Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
 LOCATION HYDRAULICS STUDY
 50 AND 100 YR. FLOOD

-----*
 * Starting To Process Header Record UP39 *
 -----*

AS UP39 32470, 0.0, 0.5, 0.1
 +++078 NOTICE: AS Record Replaced With XS Record (See Users Manual).
 GR 0.0, 70.0 125, 69.00 240, 66.0 420, 66.00 460, 67.00
 GR 640, 67.00 830, 66.00 1040, 66.00 1090, 67.00 1250, 68.00
 GR 1285, 69.00 1325, 69.00 1360, 68.0 1410, 68.00 1470, 69.0
 GR 1640, 69.00 1710, 68.00 2190, 68.00 2290, 64.00 2580, 62.0
 GR 2780, 58.00 2805, 58.00 2830, 59.0 2850, 56.00 2860, 51.4
 GR 2875, 51.40 2880, 56.00 2900, 59.0 3690, 63.00 3750, 65.0
 GR 3830, 66.00 4290, 74.00
 SA 2830 2900
 N 0.25, 0.07, 0.25

*** Completed Reading Data Associated With Header Record UP39 ***
 *** Storing X-Section Data In Temporary File As Record Number 15 ***

*** Data Summary For Header Record UP39 ***
 SRD Location: 32470. Cross-Section Skew: .0 Error Code 0
 Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
 Energy Loss Coefficients -> Expansion: .50 Contraction: .10

X,Y-coordinates (32 pairs)

X	Y	X	Y	X	Y
.000	70.000	125.000	69.000	240.000	66.000
420.000	66.000	460.000	67.000	640.000	67.000
830.000	66.000	1040.000	66.000	1090.000	67.000
1250.000	68.000	1285.000	69.000	1325.000	69.000
1360.000	68.000	1410.000	68.000	1470.000	69.000
1640.000	69.000	1710.000	68.000	2190.000	68.000
2290.000	64.000	2580.000	62.000	2780.000	58.000
2805.000	58.000	2830.000	59.000	2850.000	56.000
2860.000	51.400	2875.000	51.400	2880.000	56.000
2900.000	59.000	3690.000	63.000	3750.000	65.000
3830.000	66.000	4290.000	74.000		

Minimum and Maximum X,Y-coordinates
 Minimum X-Station: .000 (associated Y-Elevation: 70.000)
 Maximum X-Station: 4290.000 (associated Y-Elevation: 74.000)
 Minimum Y-Elevation: 51.400 (associated X-Station: 2875.000)
 Maximum Y-Elevation: 74.000 (associated X-Station: 4290.000)

Roughness Data (3 SubAreas)

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2830.000
2	.070	---
	---	2900.000
3	.250	---

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Bridge datum projection(s): XREFLT XREFRT FDSTLT FDSTRT

* Finished Processing Header Record UP39 *

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record L *
-----*

XS	L	32765				
GR		0.0, 68.00	180, 65.00	470, 65.00	640, 63.00	940, 63.00
GR		960, 65.00	1070, 69.00	1100, 69.00	1170, 67.00	1430, 65.00
GR		1820, 65.00	1840, 68.00	1920, 68.00	2494, 58.30	2533, 57.7
GR		2539, 56.40	2545, 57.60	2703, 58.2	2726, 52.70	2751, 53.1
GR		2755, 55.70	2772, 59.10	2780, 55.6	2799, 56.30	2842, 59.2
GR		2862, 55.80	2881, 58.00	2908, 58.6	2932, 54.90	2960, 60.0
GR		3020, 61.00	3835, 65.00	4160, 74.00		
SA		2725	2842			

*** Completed Reading Data Associated With Header Record L ***
*** Storing X-Section Data In Temporary File As Record Number 16 ***

*** Data Summary For Header Record L ***
SRD Location: 32765. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (33 pairs)					
X	Y	X	Y	X	Y
.000	68.000	180.000	65.000	470.000	65.000
640.000	63.000	940.000	63.000	960.000	65.000
1070.000	69.000	1100.000	69.000	1170.000	67.000
1430.000	65.000	1820.000	65.000	1840.000	68.000
1920.000	68.000	2494.000	58.300	2533.000	57.700
2539.000	56.400	2545.000	57.600	2703.000	58.200
2726.000	52.700	2751.000	53.100	2755.000	55.700
2772.000	59.100	2780.000	55.600	2799.000	56.300
2842.000	59.200	2862.000	55.800	2881.000	58.000
2908.000	58.600	2932.000	54.900	2960.000	60.000
3020.000	61.000	3835.000	65.000	4160.000	74.000

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 68.000)
Maximum X-Station: 4160.000 (associated Y-Elevation: 74.000)
Minimum Y-Elevation: 52.700 (associated X-Station: 2726.000)
Maximum Y-Elevation: 74.000 (associated X-Station: 4160.000)

Roughness Data (3 SubAreas)		
SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2725.000
2	.070	---
	---	2842.000
3	.250	---

-----*
* Finished Processing Header Record L *
-----*

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

-----*
* Starting To Process Header Record UPXS1 *
-----*

XS UPXS1 33025 * * * 0.0004

*** Completed Reading Data Associated With Header Record UPXS1 ***
*** No Roughness Data Input, Propagating From Previous Section ***
*** Storing X-Section Data In Temporary File As Record Number 17 ***

*** Data Summary For Header Record UPXS1 ***
SRD Location: 33025. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00040 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (33 pairs)					
X	Y	X	Y	X	Y
.000	68.104	180.000	65.104	470.000	65.104
640.000	63.104	940.000	63.104	960.000	65.104
1070.000	69.104	1100.000	69.104	1170.000	67.104
1430.000	65.104	1820.000	65.104	1840.000	68.104
1920.000	68.104	2494.000	58.404	2533.000	57.804
2539.000	56.504	2545.000	57.704	2703.000	58.304
2726.000	52.804	2751.000	53.204	2755.000	55.804
2772.000	59.204	2780.000	55.704	2799.000	56.404
2842.000	59.304	2862.000	55.904	2881.000	58.104
2908.000	58.704	2932.000	55.004	2960.000	60.104
3020.000	61.104	3835.000	65.104	4160.000	74.104

Minimum and Maximum X,Y-coordinates
Minimum X-Station: .000 (associated Y-Elevation: 68.104)
Maximum X-Station: 4160.000 (associated Y-Elevation: 74.104)
Minimum Y-Elevation: 52.804 (associated X-Station: 2726.000)
Maximum Y-Elevation: 74.104 (associated X-Station: 4160.000)

Roughness Data (3 SubAreas)		
SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.250	---
	---	2725.000
2	.070	---
	---	2842.000
3	.250	---

-----*
* Finished Processing Header Record UPXS1 *
-----*

25/31

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

-----*
HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

EX

* Summary of Boundary Condition Information *

#	Reach Discharge	Water Surface Elevation	Friction Slope	Flow Regime
1	4130.00	50.750	*****	Sub-Critical
2	4890.00	51.740	*****	Sub-Critical

* Beginning 2 Profile Calculation(s) *

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***** W S P R O *****
 Federal Highway Administration - U. S. Geological Survey
 Model for Water-Surface Profile Computations.
 Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
 LOCATION HYDRAULICS STUDY
 50 AND 100 YR. FLOOD

	WSEL EGEL CRWS	VHD HF HO	Q V FR #	AREA K SF	SRDL FLEN ALPHA	LEW REW ERR
Section: B1	50.750	.003	4130.000	24086.250	*****	3430.000
Header Type: XS	50.753	*****	.171	499312.80	*****	8140.000
SRD: 3450.000	41.635	*****	.036	*****	7.229	*****
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " C "						
KRATIO: .59						
Section: C	51.162	.011	4130.000	13811.520	3550.000	2037.283
Header Type: XS	51.173	.413	.299	293342.50	3550.000	4836.227
SRD: 7000.000	39.359	.004	.067	.0001	8.017	.003
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " D "						
KRATIO: .47						
Section: D	52.492	.036	4130.000	7595.759	3200.000	2825.383
Header Type: XS	52.528	1.336	.544	139229.00	3200.000	4848.009
SRD: 10200.000	48.394	.012	.138	.0004	7.835	.006
Section: E	54.696	.023	4130.000	8711.233	3000.000	2021.269
Header Type: XS	54.719	2.178	.474	168761.60	3000.000	3884.423
SRD: 13200.000	48.851	.000	.098	.0007	6.487	.013
Section: F	56.152	.029	4130.000	8695.945	3000.000	538.711
Header Type: XS	56.181	1.453	.475	208668.30	3000.000	2322.810
SRD: 16200.000	34.634	.003	.108	.0005	8.169	.006
Section: G	56.896	.007	4130.000	13638.500	2300.000	702.850
Header Type: XS	56.903	.712	.303	263974.60	2300.000	3492.697
SRD: 18500.000	51.417	.000	.053	.0003	4.884	.010
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " H "						
KRATIO: .59						
Section: H	57.730	.023	4130.000	8695.275	2000.000	481.632
Header Type: XS	57.753	.831	.475	155548.80	2000.000	2564.032
SRD: 20500.000	53.248	.008	.106	.0004	6.641	.011
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "HA "						
KRATIO: 1.58						
Section: HA	59.800	.006	4130.000	12429.960	4600.000	1414.035
Header Type: XS	59.805	2.051	.332	245958.50	4600.000	3707.970
SRD: 25100.000	54.359	.000	.045	.0004	3.258	.001
Section: LOBR	60.019	.005	4130.000	12935.770	800.000	1394.786
Header Type: XS	60.024	.214	.319	259805.70	800.000	3722.358
SRD: 25900.000	54.359	.000	.043	.0003	3.190	.005
Section: APPR	60.270	.003	4130.000	14928.190	1080.000	1324.447
Header Type: XS	60.273	.249	.277	284889.40	1080.000	4327.933
SRD: 26980.000	54.229	.000	.035	.0002	2.546	.000
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "I "						

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KRATIO: .44

Section: I	62.243	.056	4130.000	7218.647	4200.000	4572.097
Header Type: XS	62.299	1.997	.572	125931.30	4200.000	7046.676
SRD: 31180.000	58.740	.027	.196	.0005	*****	.002

Section: FULLV	63.290	.083	4130.000	1786.210	1008.000	2455.876
Header Type: FV	63.374	1.055	2.312	129452.90	1008.000	2736.125
SRD: 32188.000	58.427	.013	.161	.0010	1.000	.007

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

==135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "UP39 "

KRATIO: .67

Section: UP39	63.691	.146	4130.000	3931.946	282.000	2334.862
Header Type: AS	63.836	.429	1.050	86511.63	282.000	3710.718
SRD: 32470.000	60.490	.031	.319	.0015	8.497	.002

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>

<<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: SR39	64.095	.179	4130.000	1427.321	1008.000	2504.107
Header Type: BR	64.274	1.889	2.894	291015.80	1008.000	2677.913
SRD: 32188.000	57.991	.086	.209	*****	1.373	-.012

Specific Bridge Information	C	P/A	PFELEV	BLEN	XLAB	XRAB
Bridge Type 3	Flow Type 1					
Pier/Pile Code 1	.8533	.029	70.000	*****	*****	*****

*** Roadway Section Located at SRD 32238.000 ***

Section: ROAD Header Type: XR
<<< Embankment Is Not Overtopped >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: UP39	64.693	.073	4130.000	5370.445	165.000	2272.671
Header Type: AS	64.766	.464	.769	122649.80	242.821	3740.795
SRD: 32470.000	60.490	.027	.199	.0015	7.904	-.019

Approach Section UP39	Flow	Contraction	Information		
M(G)	M(K)	KQ	XLKQ	XRKQ	OTEL
.876	.414	72290.8	2770.479	2944.332	64.508

<<< End of Bridge Hydraulics Computations >>>

==135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " L "

KRATIO: 1.43

Section: L	64.971	.037	4130.000	7576.733	295.000	472.479
Header Type: XS	65.008	.234	.545	175309.40	295.000	3829.057
SRD: 32765.000	59.192	.000	.147	.0008	7.963	.008

* PROPOSED
CONDITIONS
BACKWATER
ELEVATION
FOR 50-YEAR
STORM EVENT

28/31

Section: UPXS1	65.119	.045	4130.000	7686.177	260.000	179.079
Header Type: XS	65.165	.154	.537	163843.70	260.000	3835.554
SRD: 33025.000	59.296	.004	.185	.0006	*****	-.002

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***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English

HILLSBOROUGH RIVER, SR 39
LOCATION HYDRAULICS STUDY
50 AND 100 YR. FLOOD

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: B1	51.740	.003	4890.000	29082.400	*****	3073.599
Header Type: XS	51.743	*****	.168	609721.80	*****	8456.801
SRD: 3450.000	42.018	*****	.034	*****	6.988	*****
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " C "						
KRATIO: .60						
Section: C	52.119	.010	4890.000	16601.300	3550.000	1903.328
Header Type: XS	52.129	.382	.295	364248.30	3550.000	4962.872
SRD: 7000.000	39.995	.003	.060	.0001	7.314	.000
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " D "						
KRATIO: .49						
Section: D	53.308	.031	4890.000	9348.840	3200.000	2784.596
Header Type: XS	53.340	1.186	.523	177166.00	3200.000	5060.103
SRD: 10200.000	48.643	.011	.124	.0004	7.397	.014
Section: E	55.423	.025	4890.000	10176.030	3000.000	1830.920
Header Type: XS	55.448	2.121	.481	190869.20	3000.000	4104.998
SRD: 13200.000	49.204	.000	.107	.0007	7.089	-.013
Section: F	56.966	.028	4890.000	10243.430	3000.000	424.809
Header Type: XS	56.994	1.541	.477	243964.50	3000.000	2444.847
SRD: 16200.000	36.823	.001	.105	.0005	7.936	.004
Section: G	57.683	.007	4890.000	15888.990	2300.000	620.967
Header Type: XS	57.690	.694	.308	324832.20	2300.000	3547.811
SRD: 18500.000	51.615	.000	.049	.0003	4.420	.002
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID " H "						
KRATIO: .59						
Section: H	58.451	.021	4890.000	10262.360	2000.000	423.928
Header Type: XS	58.472	.772	.476	190681.50	2000.000	2686.654
SRD: 20500.000	53.533	.007	.097	.0004	6.018	.003
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "HA "						
KRATIO: 1.49						
Section: HA	60.507	.006	4890.000	14122.200	4600.000	1257.909
Header Type: XS	60.514	2.028	.346	284473.00	4600.000	3784.280
SRD: 25100.000	54.680	.000	.047	.0004	3.249	.014
Section: LOBR	60.734	.006	4890.000	14706.230	800.000	1194.341
Header Type: XS	60.740	.226	.333	296991.90	800.000	3813.036
SRD: 25900.000	54.680	.000	.045	.0003	3.265	.000
Section: APPR	61.001	.003	4890.000	17306.280	1080.000	1119.698
Header Type: XS	61.004	.263	.283	330533.90	1080.000	4620.432
SRD: 26980.000	54.391	.000	.036	.0002	2.630	.001
===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "I "						

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KRATIO: .48

Section: I	62.897	.047	4890.000	8921.246	4200.000	4388.893
Header Type: XS	62.944	1.901	.548	159820.10	4200.000	7118.649
SRD: 31180.000	59.003	.022	.170	.0005	*****	.017

Section: FULLV	63.887	.097	4890.000	1954.229	1008.000	2454.544
Header Type: FV	63.984	1.010	2.502	149272.20	1008.000	2737.708
SRD: 32188.000	58.728	.025	.168	.0010	1.000	.005

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

Section: UP39	64.296	.133	4890.000	4791.732	282.000	2282.599
Header Type: AS	64.429	.421	1.021	107231.50	282.000	3728.881
SRD: 32470.000	60.973	.018	.284	.0015	8.227	.006

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>
 <<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: SR39	64.692	.227	4890.000	1531.679	1008.000	2503.044
Header Type: BR	64.919	1.839	3.193	324347.40	1008.000	2679.152
SRD: 32188.000	58.346	.135	.228	*****	1.430	-.009

Specific Bridge Information	C	P/A	PFELEV	BLEN	XLAB	XRAB
Bridge Type 3 Flow Type 1						
Pier/Pile Code 1	.8361	.028	70.000	*****	*****	*****

*** Roadway Section Located at SRD 32238.000 ***

Section: ROAD Header Type: XR
 <<< Embankment Is Not Overtopped >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: UP39 *	65.352	.069	4890.000	6352.616	165.000	2256.202
Header Type: AS	65.421	.472	.770	149879.00	243.666	3778.154
SRD: 32470.000	60.973	.030	.182	.0015	7.489	-.015

Approach Section UP39 Flow Contraction Information						
M(G)	M(K)	KQ	XLKQ	XRKQ	OTEL	
.880	.455	82008.8	2771.256	2947.400	65.178	

<<< End of Bridge Hydraulics Computations >>>

Section: L	65.613	.041	4890.000	9483.006	295.000	143.236
Header Type: XS	65.653	.231	.516	203444.80	295.000	3857.126
SRD: 32765.000	59.403	.000	.163	.0008	9.838	.001

Section: UPXS1	65.764	.039	4890.000	9631.521	260.000	140.371
Header Type: XS	65.804	.148	.508	206834.30	260.000	3858.851
SRD: 33025.000	59.507	.000	.160	.0006	9.810	.003

ER

* PROPOSED
 CONDITIONS
 BACKWATER
 ELEVATION
 FOR THE
 100-YEAR
 STORM EVENT.

31/31

***** Normal end of WSPRO execution. *****
***** Elapsed Time: 0 Minutes 4 Seconds *****

URS Greiner

JOB: SR 39 FROM I-4 TO U.S. 301 SHEET / OF 7 PROJ. NO. C100003240.19
DESCRIPTION: VII.F. Results COMPUTED BY: Zinner DATE: 5-27-99
CHECKED BY: Pratt DATE: 5-28-99

The results in the following table indicate the backwater elevations of the proposed conditions are not adversely affected in comparison to the backwater elevations of the existing conditions.

Event	Backwater Elevations (ft, NGVD)	
	Existing Conditions	Proposed Conditions
50-Year	64.7	64.7
100-Year	65.4	65.4

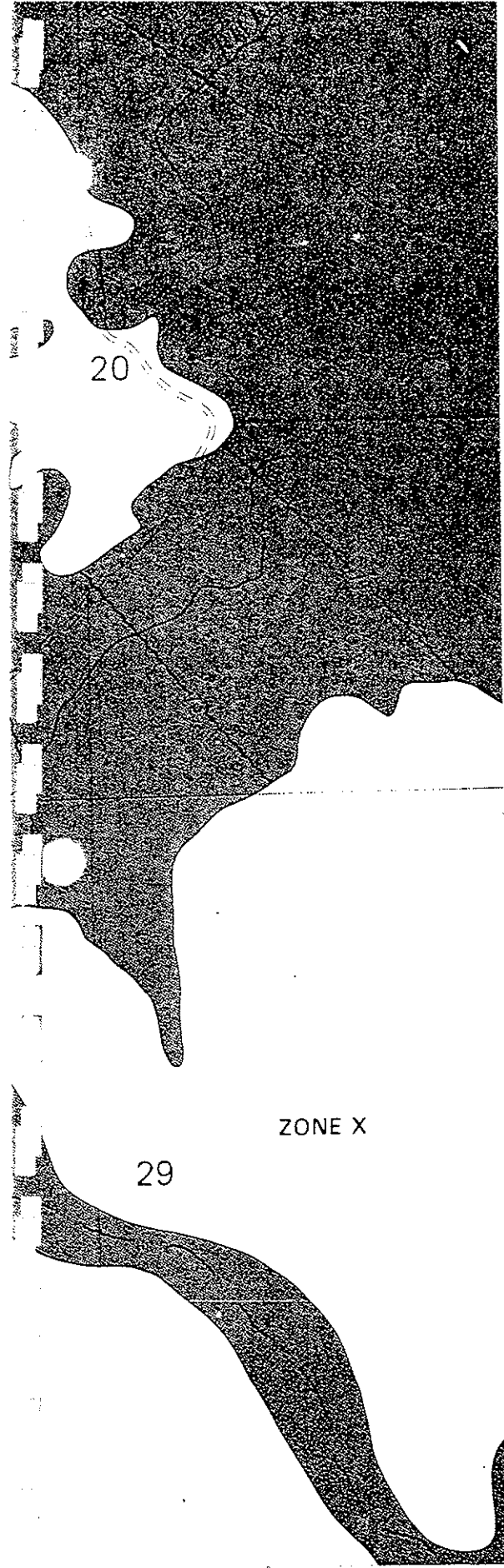
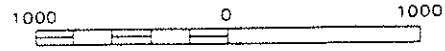
The 100-year stages resulting from WSPRO analysis are approximately equal to those provided on the following FEMA FIRM map.

2/3

To determine if flood insurance is available, contact an insurance agent or call the National Flood Insurance Program at (800) 638-6620.



APPROXIMATE SCALE IN FEET



NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP

PASCO COUNTY,
FLORIDA
(UNINCORPORATED AREAS)

PANEL 460 OF 500
(SEE MAP INDEX FOR PANELS NOT PRINTED)

COMMUNITY—PANEL NUMBER:
120230 0460 D

MAP REVISED:
SEPTEMBER 30, 1992



Federal Emergency Management Agency

- 1 SPREADING OAKS BOULEVARD
- 2 DURON STREET
- 3 CARLISLE STREET
- 4 ARGYLE STREET
- 5 OAK CREST STREET
- 6 OAK HURST STREET
- 7 CRYSTAL SPRINGS ROAD
- 8 JENDHAL AVENUE
- 9 JUSTIN AVENUE
- 10 FUNK STREET
- 11 WOODSIDE LANE
- 12 WOODGATE LANE

ZONE X

ZONE X

ZONE X

STAFFORD DRIVE
MONET DRIVE

WILLOUGHBY DRIVE

ZONE X

← S.R. 39

ZONE X

24

ZONE AE

ZONE A

HILLSBOROUGH RIVER AND FLOODPLAIN

ZONE X

X-SEC. "H"

ZONE X

PATTIE

ROAD

CORVILLA DRIVE

BLIER CORNER DRIVE

26

ZONE X

ZONE X

100-YR
ZONE X
WATER
SURFACE
ELEVATION
= 65

JERRY

ROAD

ZONE X

39

APPENDIX D

**CROSS DRAIN LOCATION
AND
FLOODPLAIN MAPS**

**CROSS DRAIN LOCATION
AND FLOODPLAIN MAP**

**MORICZVILLE TO
ZEPHYRHILLS**

**TABLE 1
EXISTING DRAINAGE STRUCTURES**

STR. NO.	DESCRIPTION	DRAINAGE AREA (AC.)	CATEGORY
D-7	1-4'x4' RCB	183	3
D-8	1-2'x2' RCB w/ 30' RCP Ext.	8.0	3
B-1	167' Steel Girder Bridge w/ Blockwater Cr. (3) 15' Semicircular Arch Relief Bridge	70,400	4
D-9	1-4'x3' RCB	72	3
D-10	1-4'x3' RCB	95	3
D-11	2-8'x3' RCB	215	3
B-2	3-10'x4' RCB	2285	3
B-3	315' Steel Girder Bridge	139,520	4
D-13	1-3'x3' RCB	8.7	3
D-14	1-3'x3' RCB	90	3
D-15	2-30' RCPs	50	3
D-16	1-30' RCP	5.8	3
D-17	2-36' RCPs	6.8	3
D-18	1-18' RCP	20 (rallaf)	3
D-19	2-36' RCP	20 (rallaf)	3
B-3	315' Steel Girder Bridge	139,520	4
D-20	1-36' RCP	18	3
D-21	3-36' RCPs	(equalizer)	3
D-22	1-36' RCP	50	3
D-23	1-24' RCP	9.6	3

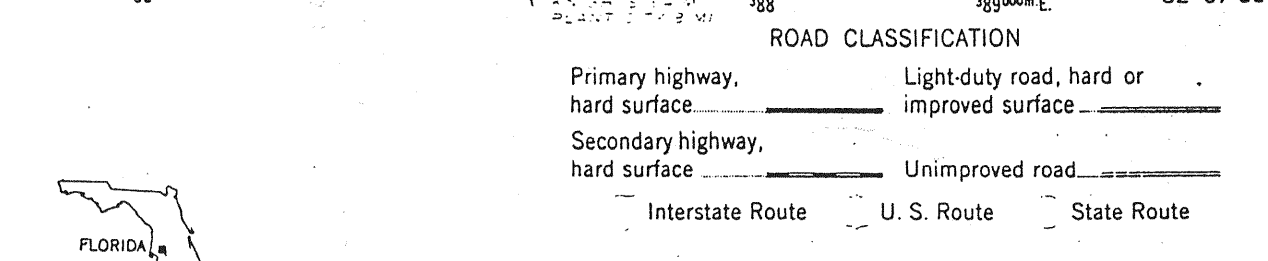
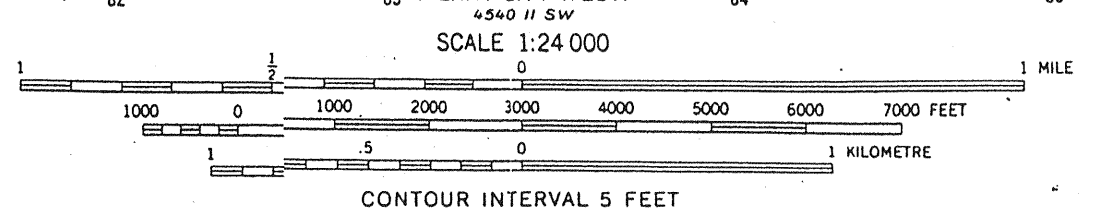
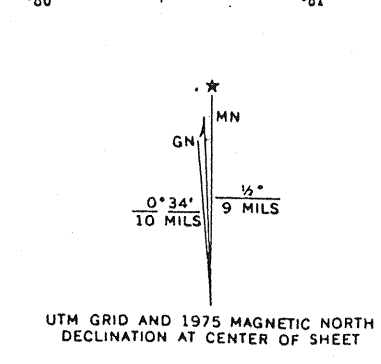
LEGEND

- D - Drainage Structure
- B - Bridge
- Flood Zone Boundary
- - - Drainage Area

SCALE 1" = 2000'

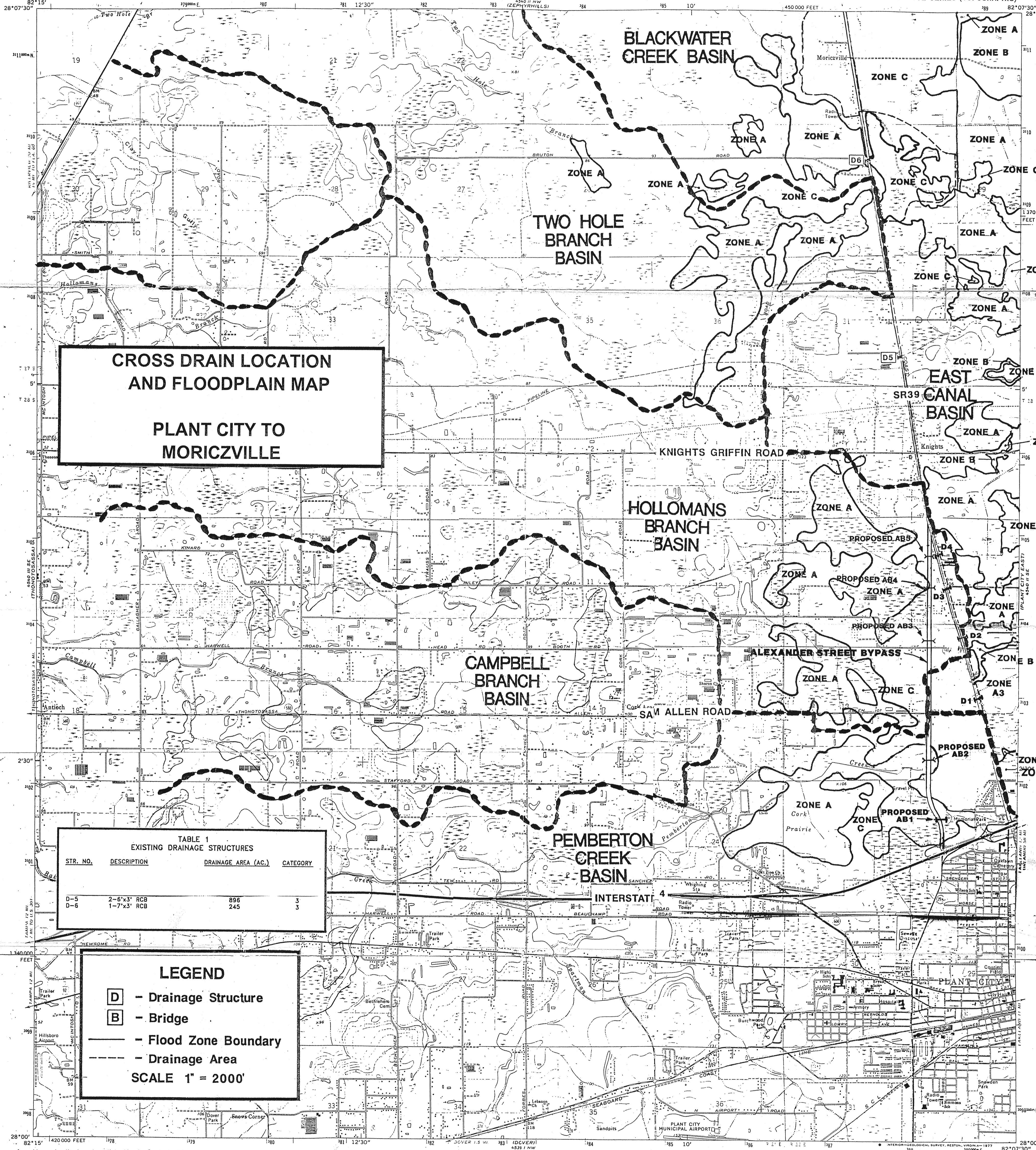


Mapped, edited, and published by the Geological Survey
Control by USGS and NOS/NOAA
Topography by photogrammetric methods from aerial photographs
taken December 1971. Field checked 1975
Supersedes Army Map Service map dated 1947
Projection and 10,000-foot grid ticks: Florida coordinate
system, west zone (transverse Mercator)
1000-metre Universal Transverse Mercator grid ticks,
zone 17, shown in blue. 1927 North American datum
Fine red dashed lines indicate selected fence and field lines where
generally visible on aerial photographs. This information is unchecked
Red tint indicates area in which only landmark buildings are shown



THIS MAP COMPLIES WITH NATIONAL MAP ACCURACY STANDARDS
FOR SALE BY U. S. GEOLOGICAL SURVEY, RESTON, VIRGINIA 22092
A FOLDER DESCRIBING TOPOGRAPHIC MAPS AND SYMBOLS IS AVAILABLE ON REQUEST

ZEPHYRHILLS, FLA.
N2807.5-W8207.5/7.5
1975
AMS 4540 II NW-SERIES V847



**CROSS DRAIN LOCATION
AND FLOODPLAIN MAP
PLANT CITY TO
MORICZVILLE**

**TABLE 1
EXISTING DRAINAGE STRUCTURES**

STR. NO.	DESCRIPTION	DRAINAGE AREA (AC.)	CATEGORY
D-5	2-6"x3' RCB	896	3
D-6	1-7"x3' RCB	245	3

LEGEND

- D - Drainage Structure
- B - Bridge
- Flood Zone Boundary
- - - Drainage Area

SCALE 1" = 2000'

APPENDIX E
COMMUNICATIONS

1/1

URS Greiner Woodward Clyde

RECORD OF CONVERSATION

DATE: 2/15/99

JOB NO: C100003240.19

RECORDED BY: Jim Zinner

OWNER/CLIENT FDOT Dist. 7

TALKED WITH: Larry Boone

OF FDOT Dade City Maintenance

ROUTE TO:

SUBJECT OF CONVERSATION: SR39 in Pasco County

ITEMS DISCUSSED:

Larry said that some side drains on the east side of SR39, just south of Chancey Road, used to flood at some driveways. The flooding problems may have been repaired when Chancey Rd. was constructed, but Larry is not positive this situation has been corrected.

Several sidedrains were constructed when the decel/accel lanes at the Crystal Springs Post Office were constructed during the last resurfacing. The side drains were installed with their flowline elevations at the same elevation as the back slope. It would be desirable if the side drains were lowered and still function properly.

FAX COVER SHEET

cc → J. KIDD / J. GARRISON, HANDLE ORD'S IN HILLS. Co. 2/5

To:	Chuck Williams
Firm:	FDOT - Tampa Maintenance Dept.
Fax #:	813-744-6057
From:	Jim Zinner
Subject:	S.R. 39 from I-4 to U.S. 301

URS Greiner
7650 W. Courtney Campbell Causeway P.O. Box 31646 (33631-3416) Tampa, FL 33607-1462 Telephone: (813) 286-1711, ext. 5355 Fax: (813) 286-6587

Date:	February 5, 1999
Page 1 of 6	

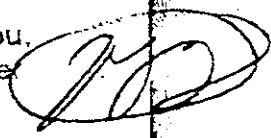
Memo:

Mr. Williams:

We are under FDOT contract to perform a PD&E study on the S.R. 39 corridor from I-4 to U.S. 301. Please see the attached map of the corridor delineated with the approximate locations of the existing cross drains and description.

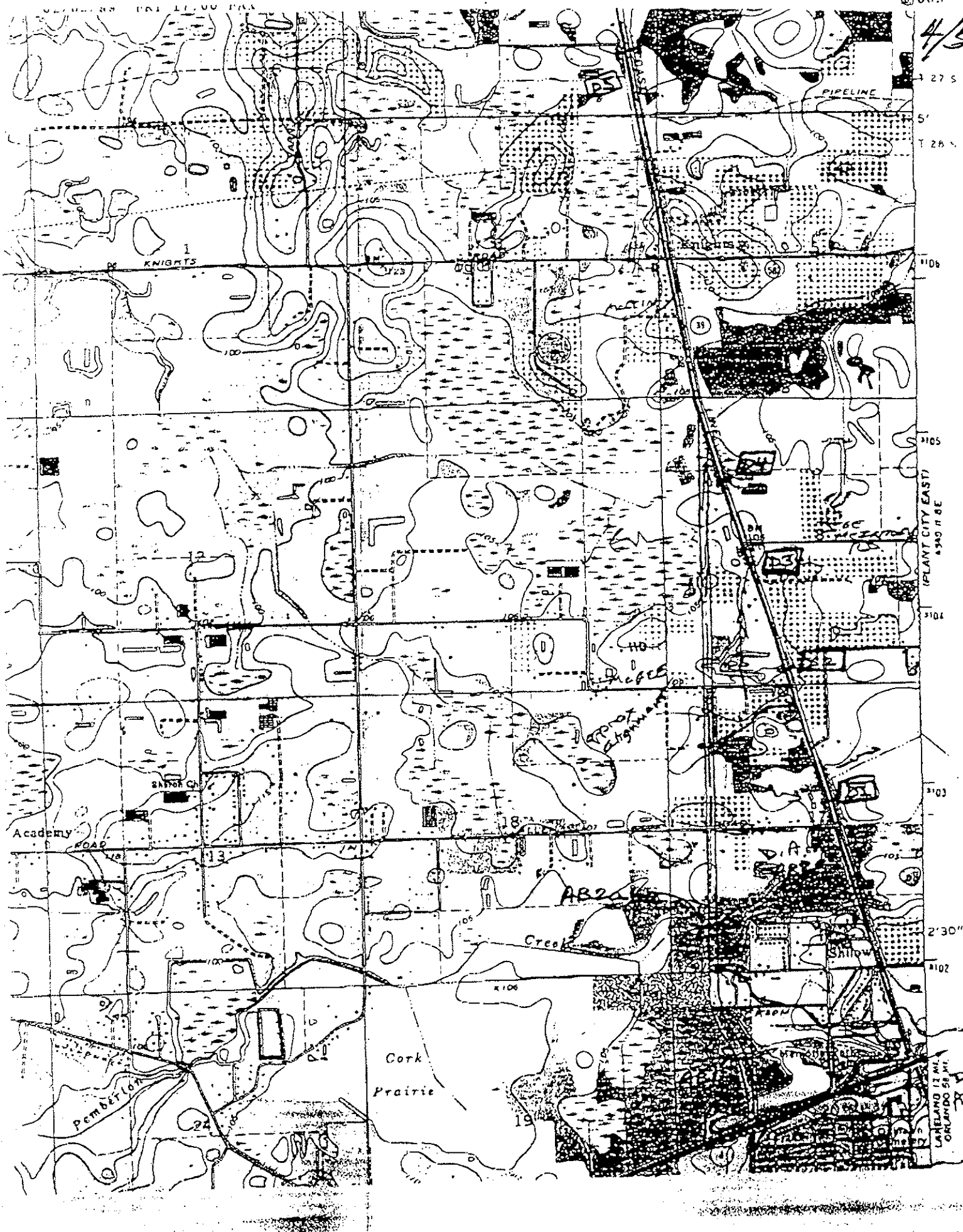
Do any of the subject cross drains have a history of flooding and or scouring? We require this information to determine whether to lengthen or replace the cross drains.

Please call me at 813-286-1711.

Thank you,
Jim Zinner 

cc:	
-----	--

4/5



T 27 S

5'

T 28 S

106

105

(PLANT CITY EAST)
S 940 N BE

104

103

2'30"

102

LARELAND 12 MI.
ORLANDO 58 MI.

2010

1/2

FAX COVER SHEET

To:	Jack Adams
Firm:	Camp Dresser, & McKee
Fax #:	813-288-8787
From:	Jim Zinner
Subject:	Alexander Street Bypass

URS Greiner
7650 W. Courtney Campbell Causeway
P.O. Box 31646 (33631-3416)
Tampa, FL 33607-1462
Telephone: (813) 286-1711, ext. 5355
Fax: (813) 286-6587

Date: February 26, 1999
Page 1 of 2

Memo:

Mr. Adams:

URS Greiner is under FDOT contract to perform a PD&E study on the S.R. 39 corridor from I-4 to U.S. 301 which includes the Alexander Street Bypass.

I apologize in that I did not look over the Plant City Westside Canal study more thoroughly before calling you yesterday. Please see the attached copied portion of Figure 2-1, of the above mentioned study, showing the proposed Alexander Street Bypass alignment. We will need information on all of the nodes that the proposed alignment will become associated with. Specifically nodes; 6410, 6405, 6034, 6035, and 6037.

Can we also obtain the Pistol Range Preliminary Alternative Data Collection Results and Conceptual Report and/or the Pistol Range Preliminary Design Report. URS Greiner and the FDOT should be cognizant of what Plant City has planned in the subject area.

We require this information for our Pond Siting Report.

If you have any questions please call me.

Thank you,
Jim Zinner

cc:

April 14, 1999

FLORIDA #AA C000901
FLORIDA #LC C000234

1/9

Mr. Carlos Lopez, P.E.
District Drainage Engineer
FDOT District Seven
1120 N. McKinley Drive
Tampa, FL 33612

Re: **SR39 and Alexander Street Bypass PD&E Study**
WPI Segment No. 254552, FAP No. F-321-1 (4)
Hillsborough and Pasco Counties, Florida

Dear Mr. Lopez:

This letter presents the conclusions of our meeting held on April 9, 1999 concerning the roadway grade control elevations discussed for the referenced project along with some background information for clarification. We discussed the seasonal high water table (SHWT) and design high water (DHW) elevations for the portion of the referenced project from I-4 to Knights-Griffin Road and an additional pond site.

The SHWT, used for vertical control elevations, was estimated by Mark Brown of FDOT at predetermined locations using wetland and soil boring indicators. The normal pool (NP) and flood elevations were also estimated at most of the wetland locations. Some the control elevations, as well as the NP and flood estimates, were field surveyed at locations where it appeared the grade elevation may not be reflected accurately on the Southwest Florida Water Management (SWFWMD) contoured aerials due to development, vegetative cover, etc. Mark Brown presented his findings in the attached memorandums. An error in the field reduction for the SHWT at site 13B was discovered and confirmed with Mark (see correction in 3-26-99 memorandum).

The nominal DHW elevation was typically assumed to be one-half of the 0.46 m (1.5 ft) maximum treatment depth (SWFWMD criteria) or 0.23 m (0.75 ft) above the SHWT. Although it was not specifically discussed, the profile grade line (PGL) can be generated from the DHW for use by Roadway Design. If the DHW was above natural grade, the minimum PGL was determined at the control elevation locations by adding 1.18m (3.87 ft) to the DHW. This 1.18 m (3.87 ft) distance is the sum of 0.61m (2 ft) base clearance, 0.42 m (1.39 ft) of pavement thickness, and 0.15 m (0.48 ft) for the cross slope. If the calculated minimum PGL elevation occurred below natural grade, the minimum PGL was assumed to be set at natural grade at that station.

The first basin that the ASB traverses is an upper reach of Pemberton Creek just north of I-4. The SHWT in the area of station 25+00 (meters) was estimated at grade, approximately 32.31 m (106.0 ft) NGVD at location 1W. This portion of Pemberton Creek is a FEMA designated floodplain but has no designated 100-year base flood elevation. This reach was recently modeled by CDM for the Westside Canal Study (for the City of Plant City) and according to their study the 100-year flood stage is 32.74 m (107.4 ft) NGVD. Mr. Lopez suggested we obtain the Pemberton Creek Study recently performed by Hillsborough County to confirm the elevations computed by CDM.

The second basin traversed by the ASB is part of another reach of Pemberton Creek farther north of the aforementioned reach. The SHWT and flood elevations were estimated and surveyed at 31.72 m (104.08 ft) NGVD and 31.98 m (104.92 ft) NGVD, respectively, near station 34+00 (location 3W). The base flood elevation in the area of this control elevation was calculated to be 32.25 m (105.8 ft) NGVD according to the CDM study, approximately 0.3 m (1 ft) above the wetland flood elevation delineated by Mark Brown.

A control elevation south of McGee Road was estimated using a soil boring at an existing high point in the proposed alignment near station 44+00 (location 5B). This control elevation was not field surveyed and therefore SWFWMD topographic information was used for estimating the SHWT at 31.62 m (103.75 ft) NGVD. In this case, the control elevation was estimated lower than the existing grade (approximately 33.53m [110.0 ft]).

McGee Road will be crossed by the ASB at approximately station 47+50. McGee Road does not appear to have flooding problems and its existing grade at 32.16 m (105.5 ft) should be maintained with the proposed vertical profile as much as possible.

The ASB crosses an agriculture irrigation and drainage (man-made) ditch system, associated with adjacent farming activities north of McGee Road, near station 48+00 (location 6W). The break-over elevation downstream of this drainage system is approximately 29.72 m (97.5 ft). It was estimated that the SHWT in this system is 2 to 3 feet above this break-over elevation, thus setting the SHWT at 30.63 m (100.5 ft) NGVD.

A control elevation was estimated using a soil boring between McGee and Joe McIntosh Roads at an existing high point near station 51+50 (location 7B). This control elevation was field surveyed and the SHWT is at 31.63m (103.76 ft) NGVD, which is lower than the existing grade (32.31m [106.01 ft]).

Part of the aforementioned man-made irrigation and drainage system drains to an existing ditch which travels west from the existing SR39 alignment, near Joe McIntosh Road. The ASB crosses this ditch at approximately 55+00 (location 8W). The SHWT at this location is estimated at 31.39 m (103.0 ft) NGVD using an adjacent wetland boundary elevation noted on the SWFWMD aerial.

FDOT Technical Memorandum

RECEIVED PD & E

5/9

1999 MAR 30 AM 10:13

To: Gabor Farkasfalvy, Carlos Lopez
 cc: Dennis Jent, John Kubler
 From: Mark Brown
 Subject: SR 39/Alexander Street Extension
 PD&E Study (FTN 255099-1, SPN 10200-1508)
 Date: March 26, 1999

The following table lists the water elevations associated with the sites requested for evaluation. I have attached a copy of my original memorandum with approximate elevations that are within close range of the surveyed elevations. If I receive additional data from the survey crew, I will pass that information along. If you have any questions, please call (ext. 27989) or e-mail (RI0744MB). Thanks again for all your help. Mark

State Road 39 - Wetland/Upland Surface & Ground Water Elevations

SITE	Grade Elev.	Normal Pool	Seasonal High	Flood Elev.
3W	103.62 ft.	103.62 ft.	104.08 ft.	104.92 ft.
7B	106.01 ft.	-----	103.76 ft.	-----
11B	110.24 ft.	-----	105.4 ft.	-----
12W	100.2 ft.	100.71 ft.	101.37 ft.	102.19 ft.
13B	105.41 ft.	-----	106.8 ft. 101.49	-----
14W	100.7 ft.	101.19 ft.	101.99 ft.	-----
15W	97.42 ft.	97.42 ft.	98.41 ft.	-----
16W	95.65 ft.	-----	95.65 ft.	-----
19W	72.23 ft.	72.8 ft.	73.54 ft.	-----
20W	70.34 ft.	70.74 ft.	71.59 ft.	-----

Note. The sites are designated "W" for wetland elevations using above-grade biological indicators for hydrological estimations. Sites designated as "B" are wetlands and uplands using soil borings for hydrological evaluations. Site 4W/B was not surveyed since it is part of the same wetland associated with Site 3W. A few wetlands have grade elevations that match either normal pool or seasonal high water elevations

Post-It Fax Note 7671

Date	3/30/99	# of pages	5
To	Kevin Doyle	From	Gabor Farkasfalvy
Co/Dept	URS Greiner	Co	FDOT
Phone #		Phone #	975-6455
Fax #	286-6587	Fax #	

7/9

Franklin Street until the road ends. Turn right on a private drive, when the driveway turns back to the east, you will see a series of locator flags leading north to the maple tree on the north side of a fence line.

Site 4B/W (Sheet 2) - This site is actually a tailwater recovery pond used for the adjacent strawberry fields. It would be good to know how deep the pond is since it will have to be filled for the roadway. The table lists the elevation for 35+46 as 104.0 ft. and 37+13 as 109.0 ft. Since the latter elevation is representative of the surrounding strawberry fields, I can't tell if the 104.0 elevation is at the pond toe-of-slope or somewhere else. In any case, I put a stake with pink ribbon at the northeast pond boundary to mark the grade elevation (SHWT) of the pond and surrounding fields. The water levels are controlled for berry production but on the average, the SHWT appears to be at least two feet below grade through the fields. **Location:** Take SR 39 north then west on Sam Allen Road until you see strawberry fields (south) across from the citrus groves (north) (Refer to Sheet 3). There is a dirt road approximately located down the proposed road right-of-way.

Site 5B (Sheet 4) - In the soil survey, this area is mapped as Fort Meade which matches the soil characteristics I found in the soil boring. The SHWT is greater than 75 inches below grade. The grade elevation at Station 44+45 is listed as 109.0 ft. **Location:** Take SR 39 north then west on McGee Road until you reach the proposed roadway centerline. Take private dirt road south until almost the end of the driveway. There is pink flag on a tree where the boring was conducted.

Site 6W (Sheet 4) - This area is a series of canals and ponds dredged within historic wetlands. Water levels within this ponded area substantially vary due to the influence of the surrounding strawberry fields. The closest station (Station 48+72) is listed as 105.0 ft. which may be close to the SHWT/Flood Elev. nailed in a willow tree, followed with a nail at the NP elev. The next station (Station 49+94) is listed as 92.4 ft. which appears to be a real questionable elevation. **Location:** There is a gate along McGee Road north of the proposed R/W. If it is closed, there is another entrance north along Jerry Red Road. There are dirt roads through the strawberry fields that run along the proposed roadway centerline.

Site 7B (Sheet 5) - There is a discrepancy between the soil conditions and what is depicted in the NRCS soil survey. Additional borings within the area found the same soil characteristics as a soil mapped just south of the proposed R/W. The soil is Seffner which has a SHWT 20-40 inches below grade. The borings conducted found a SHWT approximately 27 inches below grade. The grade elevation is difficult to determine at Station 51+50 (Station 50+70 is 105.0 ft. and Station 54+97 is 110.0 ft.). **Location:** You can either take the crop roads from Site 6W or take the private driveway from SR 39 across from Joe McIntosh Road.

Sites 8W and 9B (Sheet 5) - These sites were included as one since the soil conditions are anticipated to be the same. Both sites are mapped on the NRCS soil survey as Myakka which has a SHWT approximately 12 inches below grade. A soil boring at 8W found a SHWT at 14 inches below

Gabor Farkasfalvy, Dennis Jent, Carlos Lopez

Page 4

March 15, 1999

9/9

Site 17B (Sheet 16) - I conducted a soil boring adjacent to the roadway that indicated the SHWT is approximately 20 inches below. The roadway and adjacent natural grade elevation at that location (Station 135+18) is listed as 85 ft. which would estimate the SHWT at approximately 83.5 ft. There is a large, deep drainage swale along the R/W that probably maintains that lower water level. In addition, approximately 6 inches of fill is located adjacent to the roadway.

Site 18W (Sheet 17) - This is the Blackwater Creek crossing area. I did not set any water level indicators but refer to the specific hydrologic modeling conducted by Megan Arasteh in preparation of the Blackwater Creek Bridge replacement.

Site 19W (Sheet 21) - I set two nails (SHWT, NP) within a cypress tree along the proposed R/W limits. The nearest grade elevation (Station 168+87) is listed as 73.0 with the road grade elevation at 77.7. The SHWT elevation is 1-1.5 ft. above natural grade.

Site 20W (Sheet 23) - I set two nails (SHWT, NP) within a cypress tree. There is an old road grade berm located along the edge of the proposed R/W through this swamp. That berm acts to impound surface water between the existing SR 39 embankment and the old berm, resulting in some rather high water level indicators. The closest station (Station 185+03) has a road grade elevation of 74.5 ft. and natural grade elevation of 70.0 ft. The wetland SHWT is probably around 72.0 ft.

Site 21W (Sheet 29) - This area is listed as both a wetland and within the 100-Year Flood Zone. It is not a wetland area and have real doubts about the accuracy of the FEMA map if it is in a flood zone. The NRCS soil survey depicts the area as a Tavares soil which has a SHWT between 40 to 60 inches below grade. A soil boring within the proposed alignment verified that the soil is Tavares and a SHWT is estimated at 52 inches below grade.

If you should have any questions, please my e-mail is RD744MB and extension is 27989. Thanks-MB