

US 41 (SR 45)

From Kracker Avenue to South of SR 676 (Causeway Boulevard)
Project Development and Environment (PD&E) Study



Final Pond Sizing Report





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Work Program Item Segment No. 430056-1 ETDM Project No. 5180 Hillsborough County

Prepared for:

Florida Department of Transportation District Seven



Prepared by:

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EXECUTIVE SUMMARY

The Florida Department of Transportation (FDOT) conducted a Project Development and Environment (PD&E) Study to evaluate alternative improvements for US 41 (SR 45) from Kracker Avenue (milepoint 15.784) to south of SR 676 (Causeway Boulevard – milepoint 22.791) in Hillsborough County (Figure 1-1), a distance of approximately 7.0 miles. Study objectives included: determine proposed typical sections and develop preliminary conceptual design plans for proposed improvements, while minimizing impacts to the environment; consider agency and public comments; and ensure project compliance with all applicable federal and state laws. Improvement alternatives were identified which will improve safety and satisfy future transportation demand. A State Environmental Impact Report (SEIR) was prepared for this study and approved on January 12, 2017.

In accordance with the FDOT's PD&E Manual, a Pond Sizing Report (PSR) was prepared for this PD&E Study. The information presented in this document is subject to change until the final Phase of the project. This Pond Sizing Report is preliminary and used as an engineering tool to identify potential stormwater management and floodplain encroachments as a result of the conceptual improvements. The calculations presented in this report are preliminary and help in estimating the preliminary size of the pond site facilities for each basin. The size requirements are preliminary based upon many assumptions and judgments. Conceptual calculations are attached in **Appendix A**.

The evaluation finds that a combination of dry retention and wet detention ponds are recommended for meeting the stormwater management requirements for the proposed roadway improvements. A preliminary right of way (ROW) cost for stormwater management facilities (ponds, etc.) and floodplain compensation sites is approximately \$17 million.

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SECTION 1 INTRODUCTION

1.1 PD&E STUDY PURPOSE

The objective of this Project Development and Environment (PD&E) study was to assist the Florida Department of Transportation (FDOT) in reaching a decision on the type, location, and conceptual design of the proposed improvements for widening US 41 (SR 45) from Kracker Avenue to south of Causeway Boulevard (SR 676). The PD&E study satisfied all applicable requirements in order for this project to qualify for state funding of subsequent project development phases (design, right of way [ROW] acquisition, and construction).

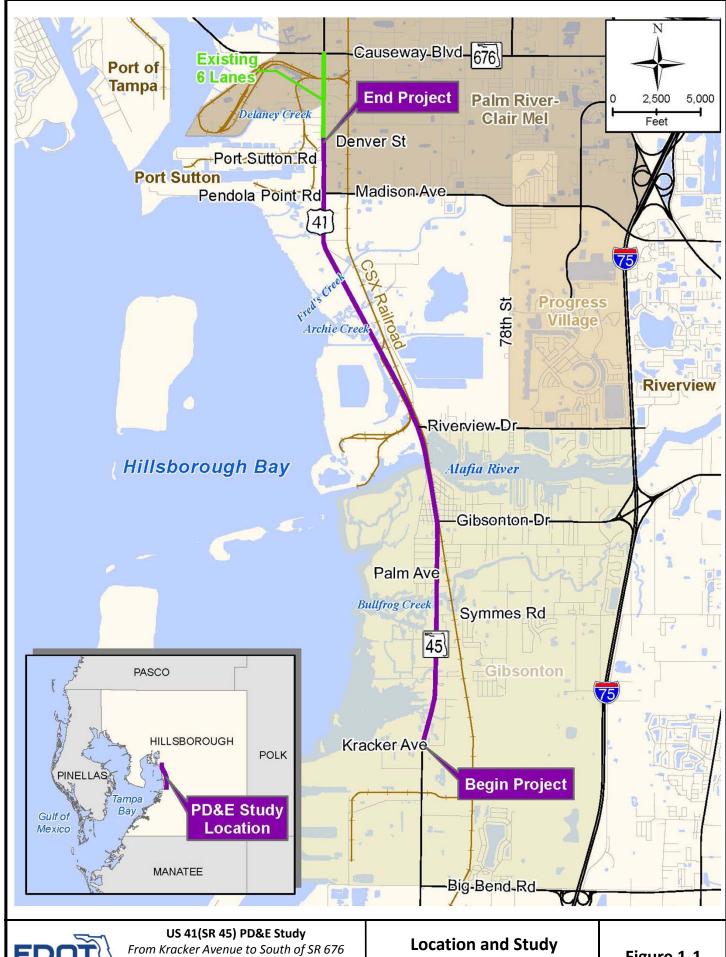
US 41 is a major north-south arterial of regional significance that parallels Interstate 75 (I-75) and US 301 in Hillsborough County. This project was screened through FDOT's Efficient Transportation Decision Making (ETDM) process as Project #5180. A *Final Programming Screen Summary Report* was published on April 10, 2013. A *State Environmental Impact Report* (SEIR) was prepared as part of this study and approved on January 12, 2017.

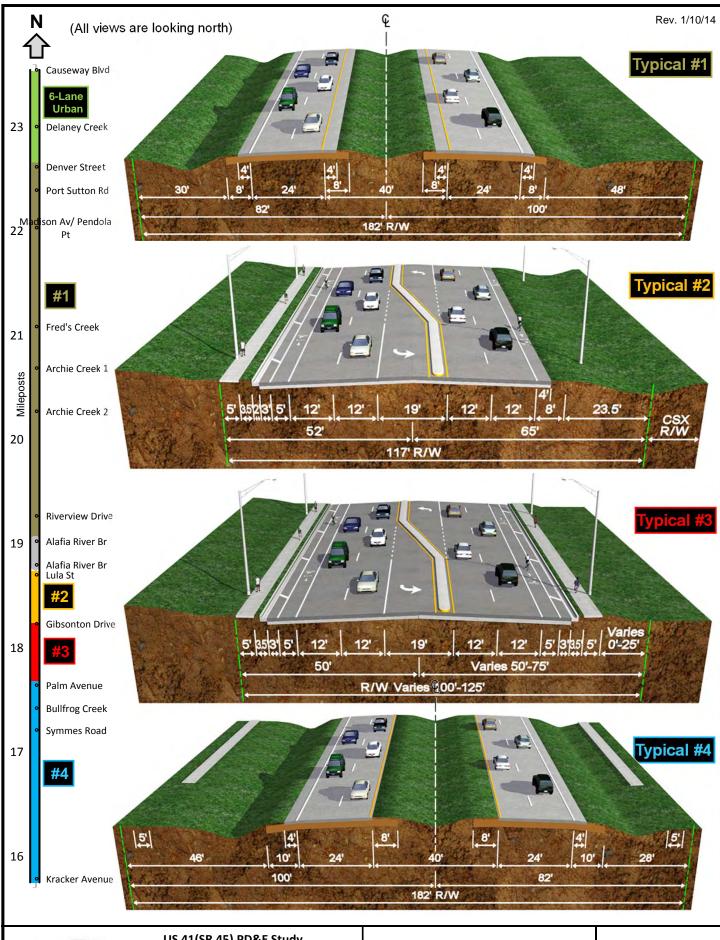
1.2 PROJECT DESCRIPTION

The FDOT conducted a PD&E study to evaluate alternative capacity and operational improvements to US 41 from Kracker Avenue (milepoint 15.784) to south of Causeway Boulevard (milepoint 22.791) in Hillsborough County (**Figure 1-1**), a distance of approximately 7.0 miles. The highway is to be improved from an existing, four-lane divided rural and urban facility to a six-lane divided facility. Bridges over Bullfrog Creek and the Alafia River are planned to be replaced. The planned improvements will include construction of stormwater management and floodplain compensation facilities and various intersection improvements, in addition to multimodal facilities (trail, pedestrian, bicycle and transit accommodations). However, the PD&E study for the proposed project did not evaluate specific stormwater management facilities and floodplain compensation sites as these locations will be identified during the proposed project's future design phase.

1.3 EXISTING FACILITY AND PLANNED IMPROVEMENTS

US 41 currently has both four-lane divided rural and urban typical sections (**Figure 1-2**). In addition, a 0.9-mile segment near the north end, between Denver Street and SR 676, was previously widened to a six-lane urban section. Existing lane widths vary from 11 to 12 feet and median widths vary from 19 to 40 feet. The rural typical section areas include 4-foot paved shoulders. The posted speed limit is 50 miles per hour (mph) in the north Gibsonton area and 55 mph in the areas to the south and north. The existing right of way width varies from 100 feet in north Gibsonton to 182 feet in the areas to the south and north. Existing bridge typical sections are shown in **Figure 1-3**.





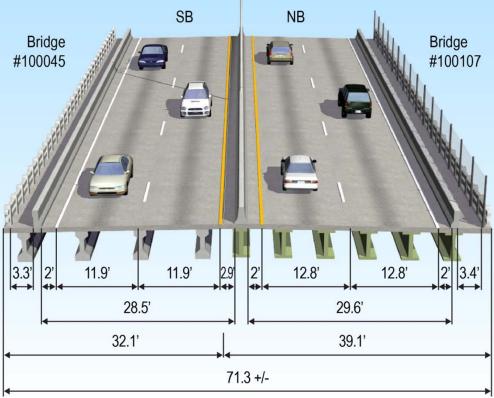


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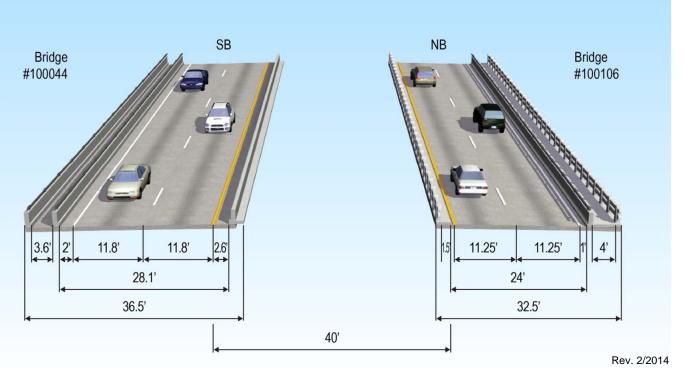
From Kracker Avenue to South of SR 676 (Causeway Blvd) WPI Segment No. 430056 1 - Hillsborough County **Existing Roadway Typical Sections**

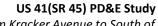
Figure 1-2

Existing Bridges over the Alafia River (Looking North) SB NB



Existing Bridges over Bullfrog Creek (Looking North)





Planned improvements include widening to six lanes as well as intersection improvements, construction of stormwater management and floodplain compensation facilities and multimodal facilities. Planned typical sections include both suburban and urban typical sections. Additional right of way will be required in the north Gibsonton area for the planned improvements. Alternatives to replace the bridges at Bullfrog Creek and the Alafia River were evaluated. Planned typical sections are shown in **Figures 1-4**, **1-5** and **1-6**. A "No-Build" Alternative was also evaluated. No future phases for this proposed project are included in FDOT's current adopted 5-year work program (Fiscal Years 16/17 through 20/21).

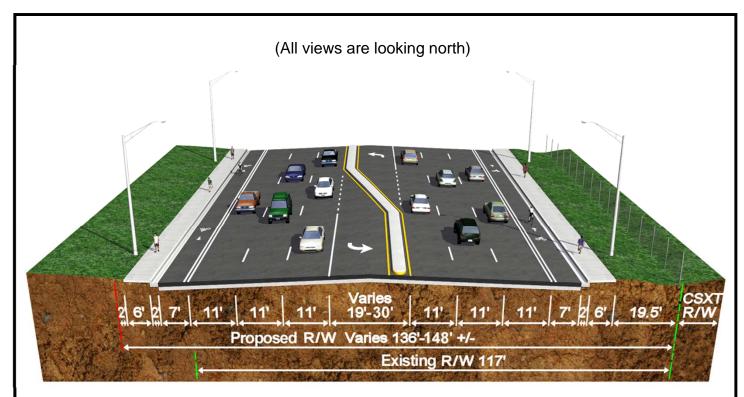
1.4 PROJECT PURPOSE AND NEED

US 41 within the study area plays a significant role in connecting southern Hillsborough County to the Tampa Bay region. The purpose of the proposed project is to accommodate future traffic demands on US 41 due to growth within the project limits and surrounding areas. Segments within this corridor are projected to operate at level of service (LOS) F in the design year (2040) if no increase in capacity is provided. Additional factors which support the need for the project include:

Regional Connectivity - US 41 is a major north-south regional arterial that parallels I-75 and US 301 and connects south Hillsborough County to the Tampa Bay region. It provides connectivity between the communities of Apollo Beach, Riverview, and Gibsonton. US 41 is a "regional road" according to the West Central Florida Metropolitan Planning Organization's (MPO's) Chairs Coordinating Committee (CCC). US 41 also provides highway access to the Port of Tampa facilities at Pendola Point and Port Sutton.

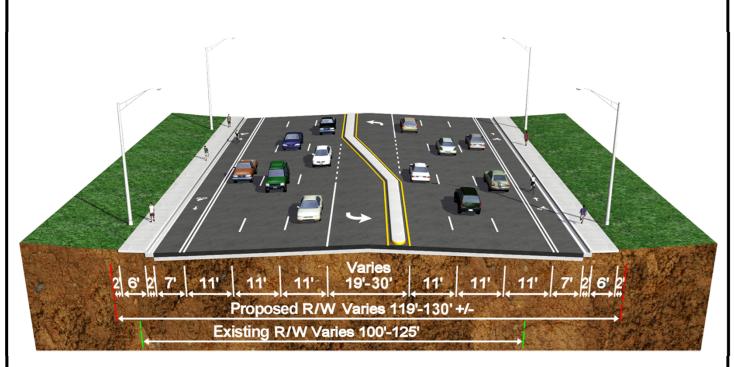
Safety - With the additional capacity provided in the corridor by the widening of US 41 from four to six lanes, roadway congestion will be reduced, which will decrease potential conflicts with other vehicles and potentially increase safety. An analysis of traffic crash data for years 2008 thru 2012 revealed that the overall average crash rate within the study limits was lower than the statewide average crash rate for similar type facilities. While not structurally deficient, the bridges over both Bullfrog Creek and the Alafia River are classified as *functionally obsolete* due to substandard-width shoulders. In addition, the sidewalks on the bridges are very narrow and there are no dedicated bicycle facilities.

Plan Consistency - This project is consistent with the Comprehensive Plan for Unincorporated Hillsborough County. The Hillsborough County *Imagine 2040 Long-Range Transportation Plan (LRTP)* indicates a need to widen US 41 to 6-lanes from 19th Avenue to north of Madison Avenue, "beyond 2040". In addition, a short segment between Madison Avenue and Causeway Boulevard is shown as 6 lanes in the Cost Feasible FDOT Strategic Intermodal System Projects, with design after year 2026.



From Gibsonton Drive to Lula Street

Design Speed = 45 mph



From Palm Avenue to Gibsonton Drive

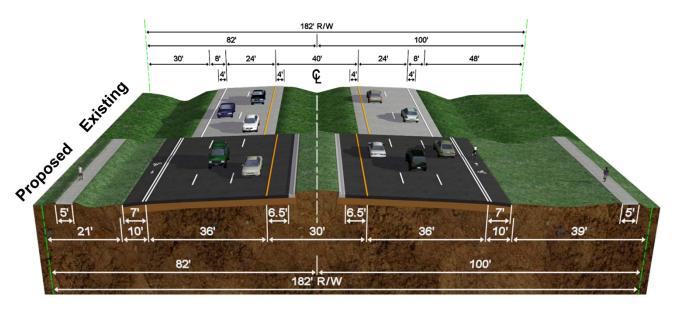
Design Speed = 45 mph

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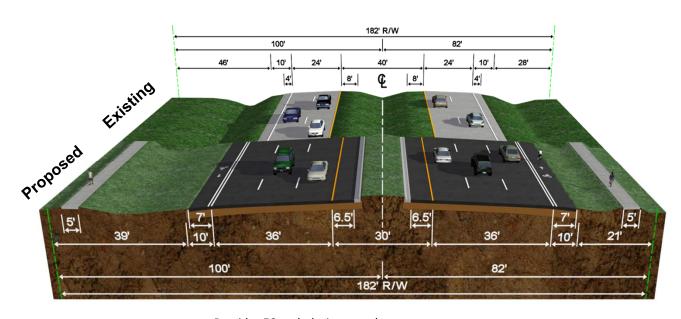
US 41(SR 45) PD&E Study

Suburban Alternatives Utilizing the Existing Pavement



- Provides 50 mph design speed (required for SIS Connector Segment north of Pendola Point)
- Design variation for border width required
- No additional ROW required

Between Alafia River Bridge & Denver Street (Near the North End of the Project)



- Provides 50 mph design speed
- Design variation for border width required
- No additional ROW required

Between Kracker Ave. & Palm Ave. (Near the South End of the Project)

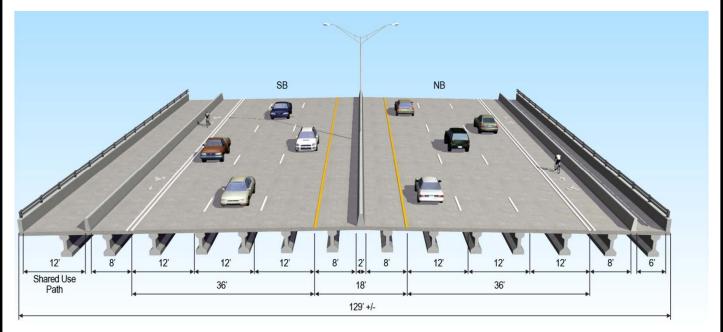
(All views are looking north)

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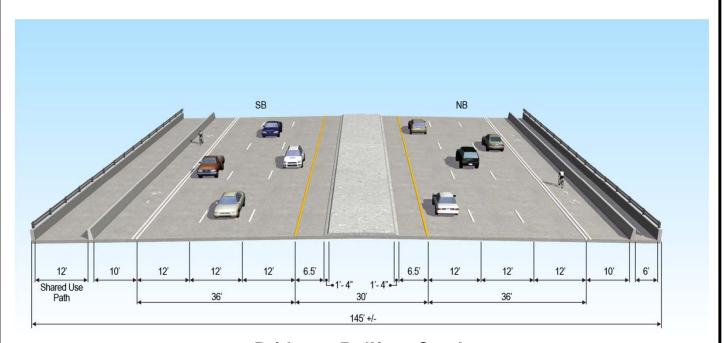
US 41(SR 45) PD&E Study

(All views are looking north)



Bridge at Alafia River

Design Speed = 50 mph



Bridge at Bullfrog Creek

Design Speed = 50 mph

Rev. 10/12/16



US 41(SR 45) PD&E Study

Emergency Evacuation - US 41 is listed as an evacuation route by the Hillsborough County Emergency Management and shown on the Florida Division of Emergency Management's evacuation route network. US 41 provides access to I-75 via interchanges with east-west connections on Gibsonton Drive, Big Bend Road (CR 672) and SR 60 in close proximity to the study limits.

Current and Future Transportation Demand - Traffic in the corridor is expected to increase due to projected population and employment growth along the corridor. In 2013, the Annual Average Daily Traffic (AADT) ranged between 23,400 vehicles per day (VPD) (Level of Service [LOS] B) and 36,400 VPD (LOS B) within the study area according to the *Traffic Technical Memorandum*. With a maximum AADT of 32,350 VPD over the four lane section, US 41 is at 88 percent capacity for the adopted level of service standard of D. In 2040, AADTs are expected to range between 38,800 VPD and 61,000 VPD. The existing four lane cross section would result in a LOS F in some segments with the future projected traffic volumes. The widening of this facility is also intended to provide relief to parallel facilities such as I-75 and US 301.

Modal Interrelationships – Expansion of the existing roadway would help improve mobility for the Hillsborough Area Regional Transit (HART) Authority local bus route 31 within the corridor. Bicycle and pedestrian accommodations will also be considered as part of the proposed improvements.

US 41 is part of the highway network that provides access to regional intermodal facilities such as the Port of Tampa and Port Manatee. The segment of US 41 between Madison Avenue/Pendola Point Road and SR 676 is designated as a Strategic Intermodal System (SIS) *connector*. The SIS is a statewide network of highways, railways, waterways, and transportation hubs that handle the bulk of Florida's passenger and freight traffic. Improvements to US 41 would enhance access to activity centers in the area and would improve movement for goods and freight in the Tampa Bay region and across the State.

1.5 REPORT PURPOSE

This *Pond Sizing Report* is one of several documents prepared as part of this PD&E study. This report documents a preliminary estimate of stormwater management pond sizes required to meet current drainage design standards. The calculations presented in this report are preliminary and will help in estimating the preliminary size of the pond site facilities for each basin.

SECTION 2 HYDROLOGIC FEATURES

The study limits of the US 41 corridor are within the three watersheds: Delaney Creek, Alafia River, and Bullfrog Creek. The proposed drainage areas are divided into 13 sub-basins. The basin limits and areas are presented in **Appendix A**.

2.1 NUTRIENT LOADING

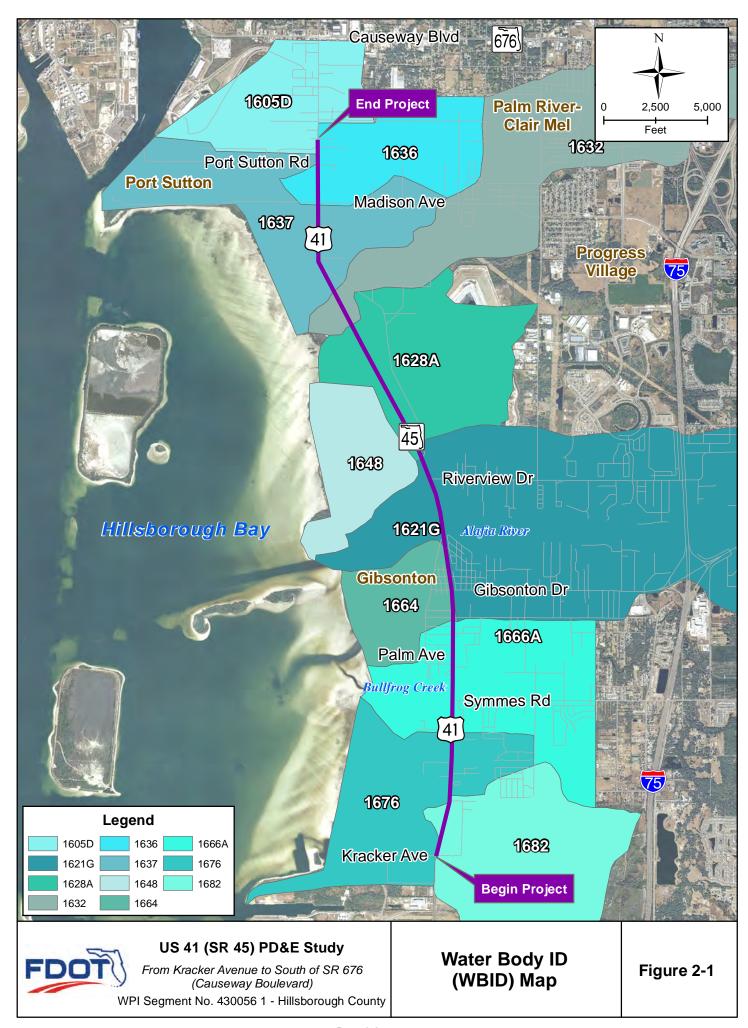
The following **Table 2-1** summarizes verified Impaired Water Body Identification (WBID) System based on Department of Environmental Protection (DEP) Geographic Information System (GIS) and **Figure 2-1** is the WBID Map.

Table 2-1 Impaired WBIDs

| Regional Basins | Project Basin No. | WBID | Impairments | | | | |
|----------------------|-------------------------|-------|---|--|--|--|--|
| Kitchen Branch | 1 | 1682 | Fecal Coliform, Nutrients (Chlorophyll-a), | | | | |
| Ritchell branch | 2 | 1002 | Dissolved Oxygen (Nutrients and BOD) | | | | |
| Direct Runoff to Bay | 3 | 1676 | Fecal Coliform, Nutrients (Chlorophyll-a), | | | | |
| | | | Dissolved Oxygen (Nutrients and BOD) | | | | |
| Pullfrog Crook | 4 | 1666A | Dissolved Oxygen, Nutrients (Chlorophyll-a and | | | | |
| Bullfrog Creek | 5 | 1000A | Historic Chlorophyll-a) | | | | |
| Direct Runoff to Bay | 6 | 1664 | (1) | | | | |
| North Prong Alafia R | 7 | 1621G | Mercury (in fish tissue), Nutrients (Chlorophyll- | | | | |
| | | | a), Dissolved Oxygen | | | | |
| Archie Creek | 8 | 1628A | Fecal Coliform (2) | | | | |
| Unnamed Canal | 9 | 1632 | Focal Caliform (2) | | | | |
| Unnamed Canal | 10 | 1032 | Fecal Coliform (2) | | | | |
| Black Point Channel | 11 | 1637 | (2) | | | | |
| Black Point Drain | 12 | 1636 | Fecal Coliform, Dissolved Oxygen (Nutrients | | | | |
| DIACK PUITE DIAIT | 13 | 1030 | and BOD) | | | | |

⁽¹⁾ Per discussion with SWFWMD this basin requires pre vs. post nutrient loading analysis since it drains directly to the bay

⁽²⁾ Per discussion with SWFWMD these basins do not require pre vs. post nutrient loading analysis



2.2 SOIL CHARACTERISTICS

Based on a review of the U.S. Department of Agriculture (USDA) and the Natural Resources Conservation Service (NRCS) Soil Survey for Hillsborough County, Florida, the predominant soils within the study limits consist of Myakka fine sand, Malabar fine sand, Pinellas fine sand, and St. Johns fine sand. For the purpose of estimating the SCS runoff Curve Numbers, the Hydrologic Soil Group was retrieved from the South West Florida Water Management District (SWFWMD) Information System website. See **Table 2-2** for USDA soils and **Figure 2-2** for soils map.

Table 2-2 USDA Soils

| Map# | Soil Name | Hydrologic Group | Depth to High Water Table (ft) | Soil Type | Description |
|------|--|---------------------|--------------------------------------|----------------------|---|
| 5 | Basinger Fine Sand, Holopaw Sand, Samsula muck | D | +2-1.0 | Sandy and loamy soil | Very poorly drained soil in depressions, slopes 0-2% |
| 15 | Felda Fine Sand | B/D | 0-1.0 | Sandy and loamy soil | Very poorly drained soil in depressions, slopes 0-1% |
| 17 | Floridana Sand | B/D | 0-1.0 | Sandy and loamy soil | Very poorly drained soil in depressions, slopes 0-1% |
| 24 | Kesson Muck | D | 0-0.5 | Sandy soil | Very poorly drained soil in tidal swamps, slopes 0-1% |
| 27 | Malabar Sand | B/D | 0-1.0 | Sandy and loamy soil | Very poorly drained soil in depressions, slopes 0-2% |
| 29 | Myakka Sand | B/D | 0-1.0 | Sandy soil | Very poorly drained soil in flatwoods, slopes 0-8% |
| 30 | Myakka Sand, frequently flooded | B/D | 0-1.0 | Sandy soil | Very poorly drained soil in flatwoods, slopes 0-8% |
| 38 | Pinellas Fine Sand | B/D | 0-1.0 | Sandy and loamy soil | Very poorly drained soil in depressions, slopes 0-2% |
| 44 | St. Augustine Fine Sand | С | 1.5-3.0 | Sandy and loamy soil | Very poorly drained soil in depressions, slopes 0-5% |
| 46 | St. Johns Sand | B/D | 0-1.0 | Sandy soil | Very poorly drained soil in broad areas, slopes 0-5% |
| 57 | Wabasso Fine Sand | B/D | 0-1.0 | Sandy and loamy soil | Very poorly drained soil in flatwoods, slopes 0-2% |





2.3 HISTORY OF FLOODING

Based on correspondence with District 7 Drainage Office and District 7 Maintenance Office there are three flood investigation sites and several locations of maintenance concern within the project limits. No history of roadway flooding was identified. See **Figure 2-3** for the FEMA floodplain map.

Flood investigation sites include flood investigation Nos. 1001032008834, 1005262005805, and 1006222010925. The flood investigation inventory sheets have been included within **Appendix B**.

Maintenance related issues identified include:

- US 41 at Palm Ave M.P. 17.642 southbound complaints related to ponding issue at roadside.
- At Florence St. MP. 16.862 there is a low area that retains water during wet season due to minimal outflow.
- At Dover St. MP.21.828 there is a low area that holds water during wet season. The outfall is
 to a creek flowing west to Tampa Bay. The outfall ditch needs clearing. This may be a County
 drainage easement and may be County maintained.
- At Bullfrog Creek, MP. 17.406 the utility strip leaches water over the sidewalk area for several blocks to the north.
- At Raleigh St.MP. 23.018 the old Chloride Battery Facility site has contaminated soil and is a Superfund site. Special attention needed in this area.

These current maintenance related issues have been taken into consideration in regards to the widening of US 41.

2.4 BASE FLOODPLAIN

The FEMA FIRMs dated August 28, 2008: 12057C0484H, 12057C0482H, 12057C0369H and 12057C0367H indicate that the study limits are within Flood Zone AE (El 11.0 ft) from approx. Station 831+00 to approx. Station 840+00 and Zone AE (10.0 ft) for the remainder of the study limits. FEMA Maps are provided in **Appendix B**. Per SWFWMD the FEMA elevations are based on storm surge conditions and base floodplain impacts will be assessed based on the lower riverine floodplain elevations.

Hillsborough County provided the following studies that establish the base floodplain for the project limits:

- Bullfrog Creek/ Wolf Branch Watershed Management Plan, dated October 2000
- Countywide Masterplan Update for the Alafia River Watershed, dated November 2010
- Delany Creek Area Stormwater Master Plan Update, dated April 2007

Hillsborough County provided GIS data along with the reports that identifies model node locations as well as other information. A nodal diagram is provided in **Appendix C** along with excerpts from these reports. Floodplain elevations for each project basin are identified in **Table 2-3**. Bullfrog Creek

elevations are provided in NGVD 29, however these elevations have been converted to NAVD 88 based on a conversion factor of -0.9.

The project's drainage design will be consistent with local FEMA, FDOT, and Southwest Florida Water Management District (SWFWMD) design guidelines, which state that no net encroachment into the floodplain, up to that encompassed by the 100-year event, which will adversely affect conveyance, storage, water quality or adjacent lands will be allowed., and that any required compensating storage shall be equivalently provided. Therefore, no significant changes in base flood elevations or limits will occur.

Table 2-3 Preliminary Floodplain Encroachment Summary

| Regional Basins | Project Basin No. | Project Basin Boundaries | Model Node ID | Zone AE- Hillsborough County 100 yr flood EL (ft – NAVD 88) |
|------------------------|-------------------------|--------------------------|---------------|---|
| Kitchen Branch | 1 | Sta 831+00 to Sta 848+90 | 822100 | 2.8 |
| KILCHEH BIAHCH | 2 | Sta 848+90 to Sta 869+91 | 822000 | 1.1 |
| Kracker Ave | 3 | Sta 869+91 to Sta 892+40 | 821200 | 5.0 |
| D. Ilfor - Corol | 4 | Sta 892+40 to Sta 917+37 | 810020,810110 | 5.1 |
| Bullfrog Creek | 5 | Sta 917+37 to Sta 946+99 | 810100 | 5.6 |
| Gibsonton | 6 | Sta 946+99 to Sta 995+51 | 700050 | 1.8 |
| North Prong Alafia R | 7 | Sta 995+51 to Sta 96+75 | 280015 | 3.9 |
| Archie Creek | 8 | Sta 96+75 to Sta 118+66 | 260040 | 4.5 |
| Dalma Divian Clain Mal | 9 | Sta 118+66 to Sta 139+67 | 240040 | 4.9 |
| Palm River-Clair Mel | 10 | Sta 139+67 to Sta 160+58 | 200305 | 7.4 |
| Black Point Channel | 11 | Sta 160+58 to Sta 189+78 | 200300,200340 | 5.1 |
| Dlack Daint Drain | 12 | Sta 189+78 to Sta 208+79 | 200025 | 7.6 |
| Black Point Drain | 13 | Sta 208+79 to Sta 220+62 | 200080 | 5.5 |

⁽¹⁾ The estimated 100-year elevations are taken from Bullfrog Creek/Wolf Branch Watershed Management Plan, Countywide Masterplan Update for the Alafia River Watershed, and the Delany Creek Area Stormwater Master Plan Update.

2.5 CURVE NUMBERS

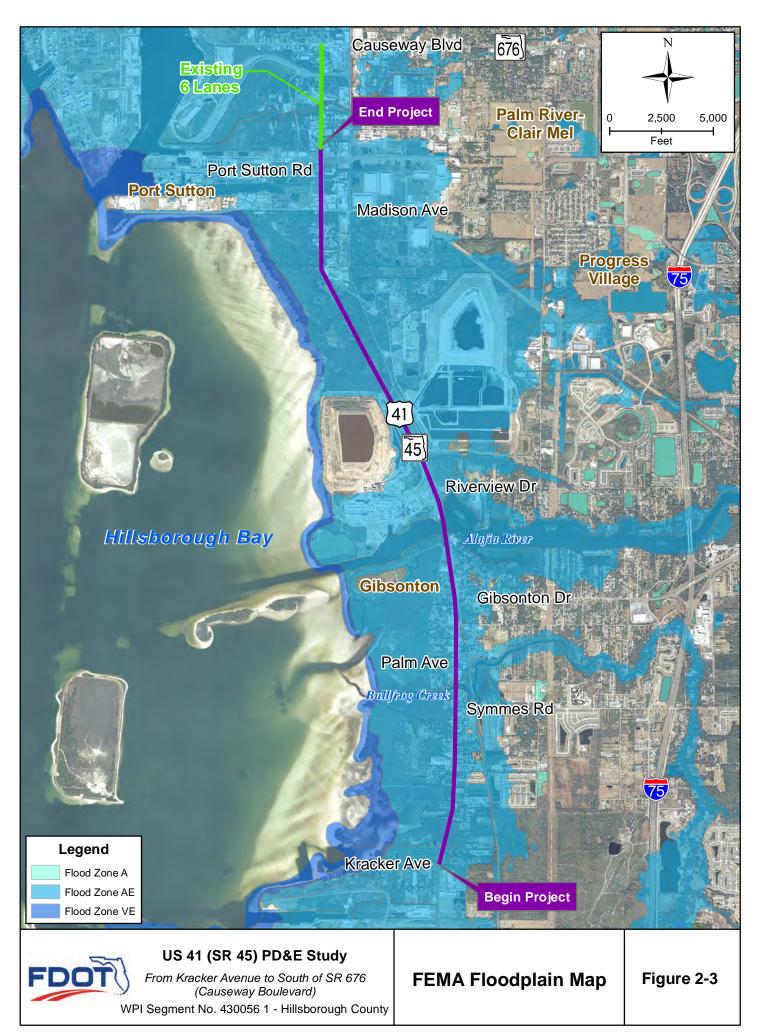
The runoff Curve Numbers (CN) were determined from Table T-7 of the FDOT Hydrology Handbook (dated February 2012) using the Hydrologic Soil Group BD.

2.6 SOIL STORAGE

The Soil storage capacity was determined using its relationship to the Curve Number using the SCS methodology.

2.7 RAINFALL INTENSITY

Rainfall intensity data were obtained from the SWFWMD's Return Period Rainfall Maps.



2.8 EXISTING DRAINAGE CONDITIONS

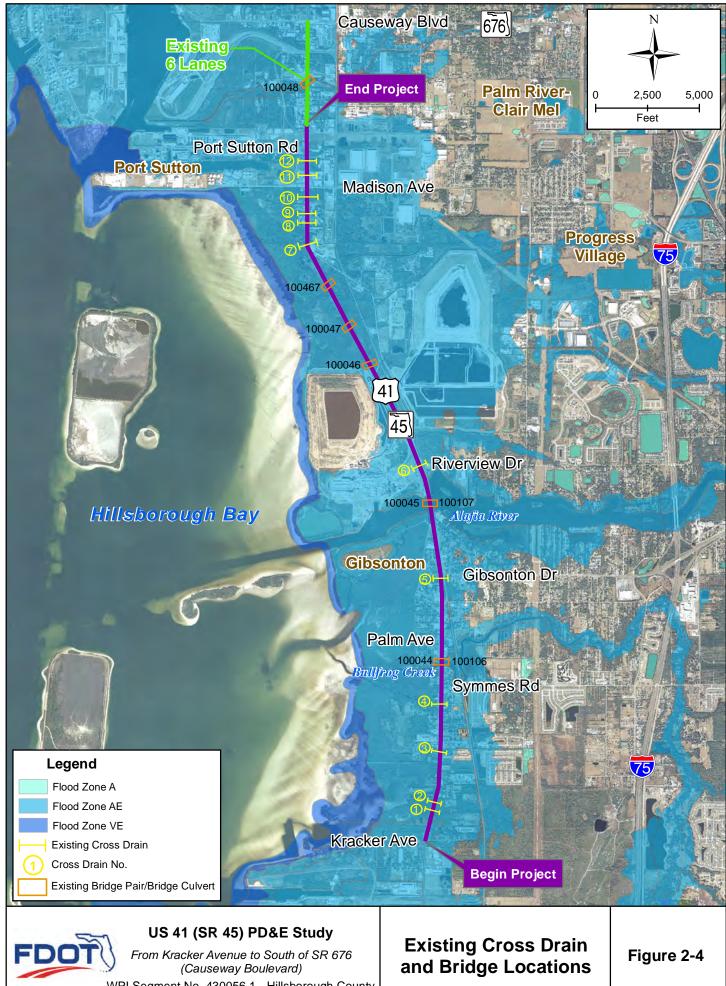
The study limits of the US 41 corridor traverses 10 regional basins with ultimate discharge to Tampa Bay. There are 12 cross drains and 6 bridge pair/bridge culverts within the study limits. See **Tables 2-4 & 2-5** for cross drain and bridge locations.

Table 2-4 Existing Cross Drains

| Cross Drain No. | Mile Post | Description |
|--------------------|-----------|-------------|
| 1 | 16.038 | 10'x5' CBC |
| 2 | 16.123 | 10'x5' CBC |
| 3 | 16.620 | 10'x8' CBC |
| 4 | 16.989 | 36" CC |
| 5 | 18.160 | 2-36" CC |
| 6 | 19.211 | 30" CC |
| 7 | 21.423 | 15" CC |
| 8 | 21.727 | 36" CC |
| 9 | 21.779 | 2-36" CC |
| 10 | 21.968 | 2-36" CC |
| 11 | 22.166 | 15" CC |
| 12 | 22.313 | 10'x7' CBC |

Table 2-5 Existing Bridge Pair/Bridge Culvert

| Bridge No. | Mile Post | Pipe Size/Type & Water Body |
|---------------|-------------|------------------------------------|
| 100044 | 17.422 (SB) | Bridge Pair (Bullfrog Creek) |
| 100106 | 17.422 (NB) | Bridge Pair (Bullfrog Creek) |
| 100045 | 18.914 (SB) | Bridge Pair (Alafia River) |
| 100107 | 18.914 (NB) | Bridge Pair (Alafia River) |
| 100046 | 20.271 | 36' Bridge Culvert (Archie Creek) |
| 100047 | 20.686 | 31' Bridge Culvert (Archie Creek) |
| 100467 | 21.084 | 26' Bridge Culvert (Fred's Creek) |
| 100048 | 23.003 | 36' Bridge Culvert (Delaney Creek) |



WPI Segment No. 430056 1 - Hillsborough County

SECTION 3 SMF DESIGN CRITERIA AND METHODOLOGY

3.1 DISCHARGE ATTENUATION

For basins with a positive outfall, and that do not discharge to an infinite basin, SWFWMD will require the proposed discharge rate from the basin be less than or equal to the existing discharge rate for the 25-yr/24-hr SWFWMD storm event. Additionally, FDOT Criteria requires Florida Administrative Code 14-86 evaluation for closed basins or basins with historical flooding.

The majority of the basins are considered to meet the infinite basin criteria based on conceptual pond outfall locations, as discussed with SWFWMD August 19, 2015, and are not anticipated to require any discharge attenuation. The project basins within Black Point Drain will require pre vs. post discharge attenuation. See notes provided with Pond Sizing Calculations and meeting minutes.

3.2 WATER QUALITY

- 1. A wet detention treatment system shall treat one inch of runoff from the contributing area.
- 2. A manmade wet detention system shall include a minimum of 35 percent littoral zone, concentrated at the outfall, for biological assimilation of pollutants. The treatment volume shall be no greater than 18 inches above the control elevation (orifice elevation/SHWL).
- 3. The wet detention system's treatment volume shall be discharged in no less than 120 hours (5 days) with no more than one-half the total volume being discharged within the first 60 hours (2.5 days).

Criterion 1 was utilized to estimate the required water quality for the wet pond. Criteria 2 and 3 will be implemented in final design. Dry retention pond is provided as well for the following reason:

Due to the impaired status for many of the receiving water bodies it is necessary to demonstrate that the project will not contribute to the impairment through demonstration of no net increase in nutrient loading from the project (pre vs. post nutrient loading comparison). Based on the Nutrient Loading calculations, shown in **Appendix A**, a wet pond would not be capable of meeting requirements for nutrient loading for some basins, therefore dry detention ponds have being considered in the estimation of pond sizing requirements.

3.3 DRAINAGE AREAS

The impervious drainage areas for each basin were determined as the basin length multiply by a typical impervious width. The pervious drainage areas were subtracted from the total drainage areas calculated as the basin length multiply by a typical Right of Way width of 182 feet. The calculations presented in this report are preliminary and help in estimating the preliminary size of the pond site facilities for each basin. The size requirements are preliminary based upon many assumptions and judgments. The results are tabulated on **Table 4-1**. The drainage basin map and conceptual calculations are shown in **Appendix A**. Historical drainage maps from District 7 have been included in **Appendix D**.

3.4 FLOODPLAIN INVOLVEMENT

The project limits have been evaluated to determine potential impacts to the base floodplain. Cup for cup compensation has been programed for any fill placed within the riverine floodplain. Alternatively, per discussion with SWFWMD, modeling and documentation could be provided to demonstrate that the fill placed within the riverine floodplain will not adversely affect conveyance, storage, water quality or adjacent lands. Therefore, it is anticipated that much of the floodplain mitigation provisions identified by this evaluation could be eliminated or reduced through more detailed analysis and modeling. Floodplain compensation site requirements are identified separately and are estimated based on estimated floodplain encroachment area, estimated floodplain encroachment volume, and estimated floodplain compensation (FPC) site area. These are summarized in **Table 4-2.**

SECTION 4 SUMMARY & RECOMMENDATIONS

The evaluation finds that a combination of dry retention and wet detention ponds are recommended for providing stormwater management to serve the proposed US 41 (SR 45) improvements. **Table 4-1** classifies the SMF size requirements per basin. **Table 4-2** shows the estimated floodplain encroachment area, estimated floodplain encroachment volume, and estimated floodplain compensation (FPC) site area.

Table 4-1 Pond Sizing Areas

| Regional Basins | Project Basin No. | Project Basin Boundaries | Project Basin Acreage (ac) | SMF Total Area (ac) |
|----------------------|-------------------------|--------------------------|-------------------------------------|------------------------|
| Kitchen Branch | 1 | Sta 831+00 to Sta 848+90 | 7.48 | 1.2 |
| KILCHEH DI dHCH | 2 | Sta 848+90 to Sta 869+91 | 8.78 | 1.5 |
| Direct Runoff to Bay | 3 | Sta 869+91 to Sta 892+40 | 9.40 | 1.6 |
| Pullfrog Crook | 4 | Sta 892+40 to Sta 917+37 | 10.43 | 1.7 |
| Bullfrog Creek | 5 | Sta 917+37 to Sta 946+99 | 12.38 | 2.1 |
| Direct Runoff to Bay | 6 | Sta 946+99 to Sta 995+51 | 20.27 | 3.4 |
| North Prong Alafia R | 7 | Sta 995+51 to Sta 96+75 | 30.21 | 5.0 |
| Archie Creek | 8 | Sta 96+75 to Sta 118+66 | 9.15 | 1.5 |
| Unnamed Canal | 9 | Sta 118+66 to Sta 139+67 | 8.78 | 1.5 |
| Offinallieu Cariai | 10 | Sta 139+67 to Sta 160+58 | 8.74 | 1.5 |
| Black Point Channel | 11 | Sta 160+58 to Sta 189+78 | 12.20 | 2.0 |
| Black Point Drain | 12 | Sta 189+78 to Sta 208+79 | 7.94 | 2.0 |
| DIACK PUHIL DI AITI | 13 | Sta 208+79 to Sta 220+62 | 4.94 | 1.3 |
| | | Total | 150.69 | 26.3 |

Table 4-2 Floodplain Encroachment and Compensation Summary

| Basin #/FPC Site No. | Project Basin Boundaries | Estimated Floodplain Encroachment Area (ac) | Estimated Floodplain Encroachment Volume (ac-ft) | Estimated Floodplain Compensation (FPC) site Area (ac) |
|-------------------------------|---|--|---|--|
| 1 | Sta. 831+00.00 to Sta 848+90.00 | Abo | ove 100 yr floodp | lain |
| 2 | Sta 848+90.00 to Sta. 869+91.00 | Abo | ove 100 yr floodp | lain |
| 3 | Sta. 869+91.00 to Sta. 892+40.00 | 2.74 | 1.37 | 1.71 |
| 4 | Sta. 892+40.00 to Sta. 917+37.00 | 0.56 | 0.28 | 0.35 |
| 5 | Sta. 917+37.00 to Sta. 946+99.00 | Abo | ove 100 yr floodp | lain |
| 6 | Sta. 946+99.00 to Sta. 995+51.00 | Abo | ove 100 yr floodp | lain |
| 7 | Sta. 995+51.00 to Sta. 1034+11.00 Sta. 63+05.00 to Sta. 96+75.00 | Abo | ove 100 yr floodp | lain |
| 8 | Sta. 96+75.00 to Sta. 118+66.00 | Abo | ove 100 yr floodp | lain |
| 9 | Sta. 118+66.00 to Sta. 139+67.00 | Abo | ove 100 yr floodp | lain |
| 10 | Sta. 139+67.00 to Sta. 160+58.00 | 2.54 | 5.08 | 6.35 |
| 11 | Sta. 160+58.00 to Sta. 189+78.00 | 3.13 | 1.57 | 1.96 |
| 12 | Sta. 189+78.00 to Sta. 208+79.00 | 2.31 | 2.31 | 2.89 |
| 13 | Sta. 208+79.00 to Sta. 220+62.00 | 1.44 | 0.72 | 0.90 |

¹⁾ The estimated floodplain encroachment area is based on a 26.5 ft width per the length of encroachment per side.

Cost Estimates

An earlier conceptual SMF/FPC Area of 67.66 acres was based on attenuation and water quality for sizing pond areas. After meeting with SWFWMD staff on August 19, 2015 (see **Appendix E**), it was determined that attenuation would not be required for most areas where a direct connection to the Bay is possible, allowing the pond sizing to decrease. FDOT's ROW staff previously provided a ROW total cost estimate of \$20,502,400 for pond sites, based on 67.66 acres. Based on the new conceptual area of 55.97 acres and a factor of \$303,020.99/acre, the new total estimated cost is approximately \$17,000,000.

②An estimated fill depth based on contour data and the average depth was estimated per basin.

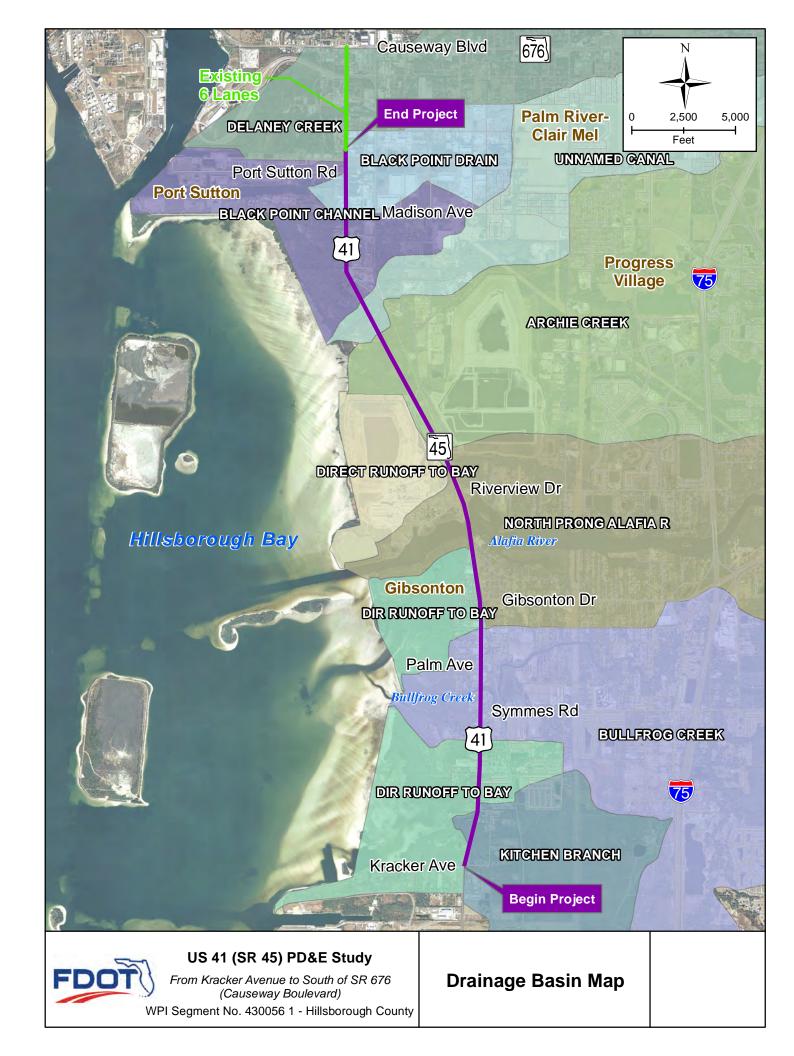
⁽³⁾ An estimated of 1.25 determined the FPC site area.

⁽⁴⁾ See Appendix C (Floodplain Encroachment and Compensation Calculation Summary) for Calculations.

APPENDIX A

Calculations

Drainage Basin Map



| | EXISTING LAND USE | | | | | | | | | | | | |
|-------|-----------------------|------------------------|----------------|---------------------------------|----------------------------------|---------------------------------|------------------------------|-----------------------|-----------------------|--------------------|--------------|--|--|
| Basin | Sta. From | Sta. To | Length (ft) | Typical R/W Width (ft) | Typical Imp. Width (ft) | Typical Imp. Area (ac) | Add 10% Imp. Area (ac) | Imp. Total (ac) | Pervious Area (ac) | Total Area (ac) | Exist. CN | | |
| 1 | 831+00.00 | 848+90.00 | 1790 | 182 | 56 | 2.30 | 0.23 | 2.53 | 4.95 | 7.48 | 79 | | |
| 2 | 848+90.00 | 869+91.00 | 2101 | 182 | 56 | 2.70 | 0.27 | 2.97 | 5.81 | 8.78 | 79 | | |
| 3 | 869+91.00 | 892+40.00 | 2249 | 182 | 56 | 2.89 | 0.29 | 3.18 | 6.22 | 9.40 | 79 | | |
| 4 | 892+40.00 | 917+37.00 | 2497 | 182 | 56 | 3.21 | 0.32 | 3.53 | 6.90 | 10.43 | 79 | | |
| 5 | 917+37.00 | 946+99.00 | 2962 | 182 | 56 | 3.81 | 0.38 | 4.19 | 8.19 | 12.38 | 79 | | |
| 6 | 946+99.00 | 995+51.00 | 4852 | 182 | 56 | 6.24 | 0.62 | 6.86 | 13.41 | 20.27 | 79 | | |
| 7 | 995+51.00 63+05.00 | 1034+11.00 96+75.00 | 7230 | 182 | 64 | 10.62 | 1.06 | 11.68 | 18.52 | 30.21 | 80 | | |
| 8 | 96+75.00 | 118+66.00 | 2191 | 182 | 56 | 2.82 | 0.28 | 3.10 | 6.06 | 9.15 | 79 | | |
| 9 | 118+66.00 | 139+67.00 | 2101 | 182 | 56 | 2.70 | 0.27 | 2.97 | 5.81 | 8.78 | 79 | | |
| 10 | 139+67.00 | 160+58.00 | 2091 | 182 | 56 | 2.69 | 0.27 | 2.96 | 5.78 | 8.74 | 79 | | |
| 11 | 160+58.00 | 189+78.00 | 2920 | 182 | 56 | 3.75 | 0.38 | 4.13 | 8.07 | 12.20 | 79 | | |
| 12 | 189+78.00 | 208+79.00 | 1901 | 182 | 56 | 2.44 | 0.24 | 2.69 | 5.25 | 7.94 | 79 | | |
| 13 | 208+79.00 | 220+62.00 | 1183 | 182 | 56 | 1.52 | 0.15 | 1.67 | 3.27 | 4.94 | 79 | | |

Note: The CN value used for pervious area in the calculation is 69.

| | PROPOSED LAND USE | | | | | | | | | | | | |
|-------|-----------------------|------------------------|----------------|---------------------------------|----------------------------------|---------------------------------|------------------------------|-----------------------|-----------------------|--------------------|-------------|--|--|
| Basin | Sta. From | Sta. To | Length (ft) | Typical R/W Width (ft) | Typical Imp. Width (ft) | Typical Imp. Area (ac) | Add 15% Imp. Area (ac) | Imp. Total (ac) | Pervious Area (ac) | Total Area (ac) | Prop. CN | | |
| 1 | 831+00.00 | 848+90.00 | 1790 | 182 | 109 | 4.48 | 0.67 | 5.15 | 2.33 | 7.48 | 89 | | |
| 2 | 848+90.00 | 869+91.00 | 2101 | 182 | 109 | 5.26 | 0.79 | 6.05 | 2.73 | 8.78 | 89 | | |
| 3 | 869+91.00 | 892+40.00 | 2249 | 182 | 109 | 5.63 | 0.84 | 6.47 | 2.92 | 9.40 | 89 | | |
| 4 | 892+40.00 | 917+37.00 | 2497 | 182 | 109 | 6.25 | 0.94 | 7.19 | 3.25 | 10.43 | 89 | | |
| 5 | 917+37.00 | 946+99.00 | 2962 | 182 | 109 | 7.41 | 1.11 | 8.52 | 3.85 | 12.38 | 89 | | |
| 6 | 946+99.00 | 995+51.00 | 4852 | 182 | 109 | 12.14 | 1.82 | 13.96 | 6.31 | 20.27 | 89 | | |
| 7 | 995+51.00 63+05.00 | 1034+11.00 96+75.00 | 7230 | 182 | 109 | 18.09 | 2.71 | 20.81 | 9.40 | 30.21 | 89 | | |
| 8 | 96+75.00 | 118+66.00 | 2191 | 182 | 109 | 5.48 | 0.82 | 6.30 | 2.85 | 9.15 | 89 | | |
| 9 | 118+66.00 | 139+67.00 | 2101 | 182 | 109 | 5.26 | 0.79 | 6.05 | 2.73 | 8.78 | 89 | | |
| 10 | 139+67.00 | 160+58.00 | 2091 | 182 | 109 | 5.23 | 0.78 | 6.02 | 2.72 | 8.74 | 89 | | |
| 11 | 160+58.00 | 189+78.00 | 2920 | 182 | 109 | 7.31 | 1.10 | 8.40 | 3.80 | 12.20 | 89 | | |
| 12 | 189+78.00 | 208+79.00 | 1901 | 182 | 109 | 4.76 | 0.71 | 5.47 | 2.47 | 7.94 | 89 | | |
| 13 | 208+79.00 | 220+62.00 | 1183 | 182 | 109 | 2.96 | 0.44 | 3.40 | 1.54 | 4.94 | 89 | | |

Note: The CN value used for pervious area in the calculation is 69.

| | POND SIZING CALCULATIONS | | | | | | | | | | | | |
|-------|--------------------------|--------------|------------------|---------------------------------------|-------------|-----------------|--------------------------------------|------------------------------|----------------------------|-------------------------------|-------------------------------|-------------------------------|--|
| Basin | Basin Area | Exist. CN | Exist. S (in) | Exist. 25-yr 24-hr vol. (ac-ft) | Prop. CN | Prop. S (in) | Prop. 25-yr 24-hr vol. (ac-ft) | Req. Att. Vol. (ac-ft) | Req. WQ Vol. (ac-ft) | Dry Retention Pond (ac) | Wet Retention Pond (ac) | Total Pond Area (ac) | |
| 1 | 7.48 | 79 | 3 | 4.02 | 89 | 1 | 4.78 | 0.00 | 0.62 | 1.2 | 0.0 | 1.2 | |
| 2 | 8.78 | 79 | 3 | 4.71 | 89 | 1 | 5.61 | 0.00 | 0.73 | 1.5 | 0.0 | 1.5 | |
| 3 | 9.40 | 79 | 3 | 5.05 | 89 | 1 | 6.01 | 0.00 | 0.78 | 1.6 | 0.0 | 1.6 | |
| 4 | 10.43 | 79 | 3 | 5.60 | 89 | 1 | 6.67 | 0.00 | 0.87 | 1.7 | 0.0 | 1.7 | |
| 5 | 12.38 | 79 | 3 | 6.65 | 89 | 1 | 7.91 | 0.00 | 1.03 | 2.1 | 0.0 | 2.1 | |
| 6 | 20.27 | 79 | 3 | 10.89 | 89 | 1 | 12.96 | 0.00 | 1.69 | 3.4 | 0.0 | 3.4 | |
| 7 | 30.21 | 80 | 3 | 16.53 | 89 | 1 | 19.31 | 0.00 | 2.52 | 5.0 | 0.0 | 5.0 | |
| 8 | 9.15 | 79 | 3 | 4.92 | 89 | 1 | 5.85 | 0.00 | 0.76 | 1.5 | 0.0 | 1.5 | |
| 9 | 8.78 | 79 | 3 | 4.71 | 89 | 1 | 5.61 | 0.00 | 0.73 | 1.5 | 0.0 | 1.5 | |
| 10 | 8.74 | 79 | 3 | 4.69 | 89 | 1 | 5.58 | 0.00 | 0.73 | 1.5 | 0.0 | 1.5 | |
| 11 | 12.20 | 79 | 3 | 6.55 | 89 | 1 | 7.80 | 0.00 | 1.02 | 2.0 | 0.0 | 2.0 | |
| 12 | 7.94 | 79 | 3 | 4.27 | 89 | 1 | 5.08 | 0.81 | 0.66 | 1.3 | 0.7 | 2.0 | |
| 13 | 4.94 | 79 | 3 | 2.65 | 89 | 1 | 3.16 | 0.50 | 0.41 | 0.8 | 0.5 | 1.3 | |

Nutrient Loading Calcs

Representative Area Calculation for **Nutrient Loading Concerns**

 $AP := 51.50 \frac{\text{in}}{}$

Annual Mass Loading for Highway Areas

TNhwy := $1.64 \frac{\text{mg}}{1}$

Annual Precipitation Depth

TPhwy := $0.220 \frac{\text{mg}}{1}$

Annual C values

Meteorological Zone 4

Existing loading calculation

Existing roadway DCIA = 35%

NDCIA(CN) = 65

From Appendix E, FDEP Stormwater Quality Handbook (2010)

Annual curve number $CA_e := 0.323$

 $CA_{e} = 0.32$

Existing annual runoff $QA_e := CA_e \cdot AP \cdot 1$ acre

 $QA_e = 1.39ft \cdot \frac{acre}{yr}$

Project: US 41 (SR 45) PD&E

Project No.: 5127041

FPID No. 430056-1-22-01 Hillsborough County

Existing annual loading

Nitrogen loading $NA_e := TNhwy \cdot QA_e$ $NA_e = 2.80 \frac{kg}{yr}$

Posphorus loading $PA_e := TPhwy \cdot QA_e$

 $PA_e = 0.38 \frac{kg}{vr}$

Proposed loading calculation

Proposed roadway DCIA = 70%

NDCIA(CN) = 65

From Appendix E, FDEP Stormwater Quality Handbook (2010)

Annual curve number $CA_n := 0.592$

Existing annual runoff $QA_p := CA_p \cdot AP \cdot 1$ acre

 $QA_p = 2.54 \text{ft} \cdot \frac{\text{acre}}{\text{yr}}$

Existing annual loading

Nitrogen loading

 $NA_p := TNhwy \cdot QA_p$ $NA_p = 5.14 \frac{kg}{yr}$

Phosphorus loading

 $PA_p := TPhwy \cdot QA_p$ $PA_p = 0.69 \frac{kg}{vr}$

Required removal efficiency calculations

Required N removal efficiency

 $NRe := 1 - \frac{NA_e}{NA_p} \qquad \qquad NRe = 45.4 \cdot \%$

Required Premoval efficiency

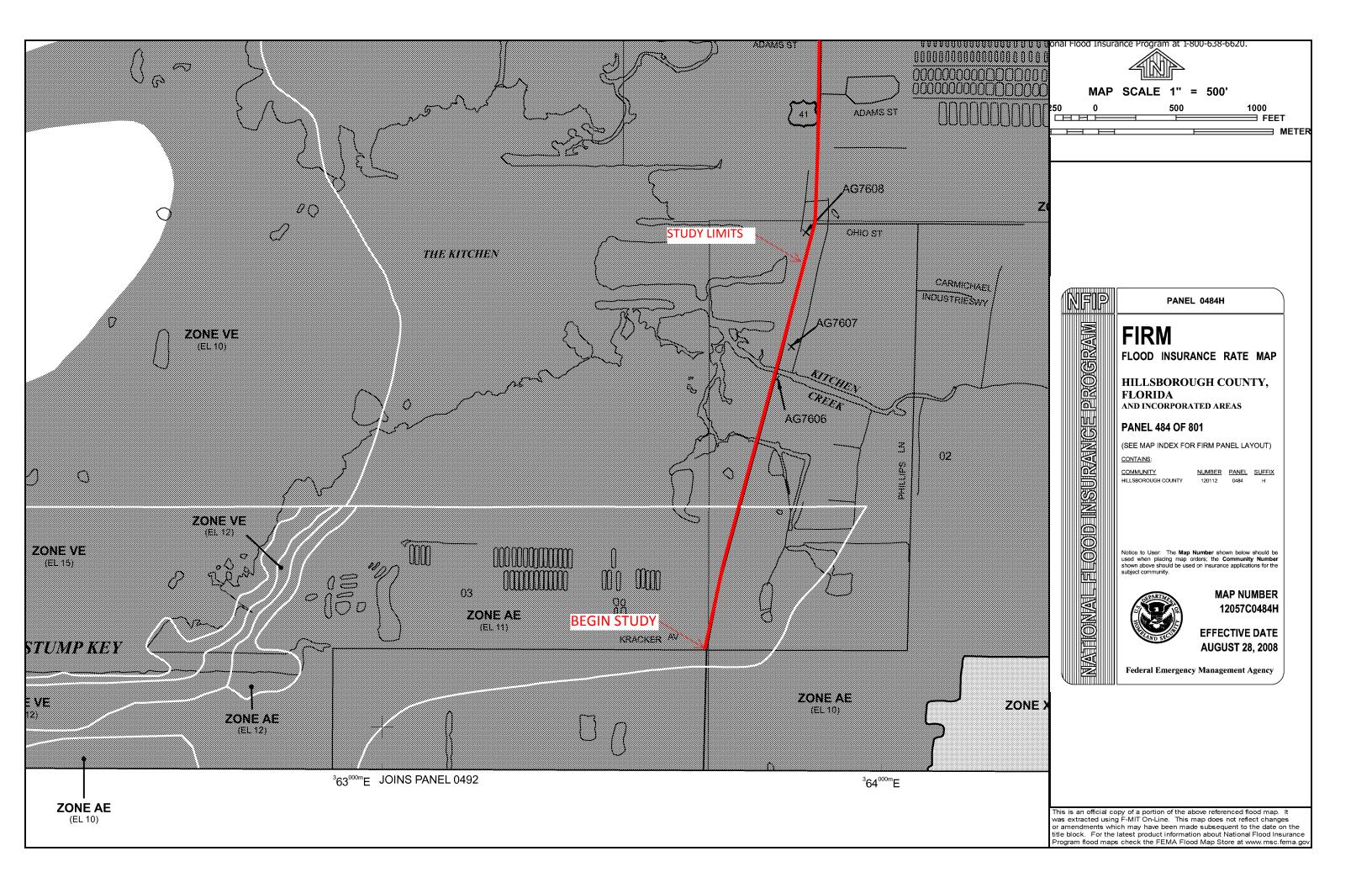
 $PRe := 1 - \frac{PA_e}{PA_p}$

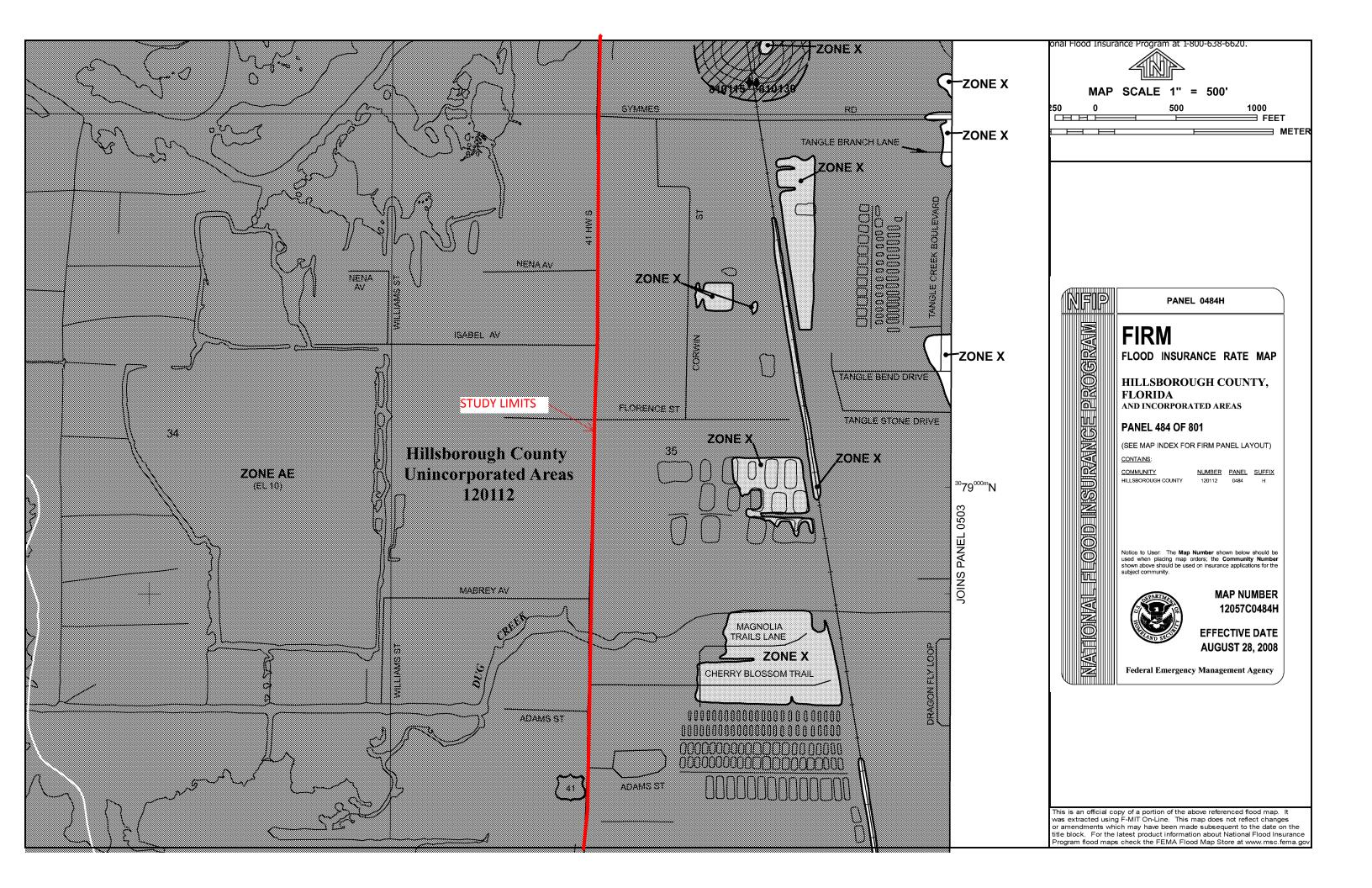
 $PRe = 45.4 \cdot \%$

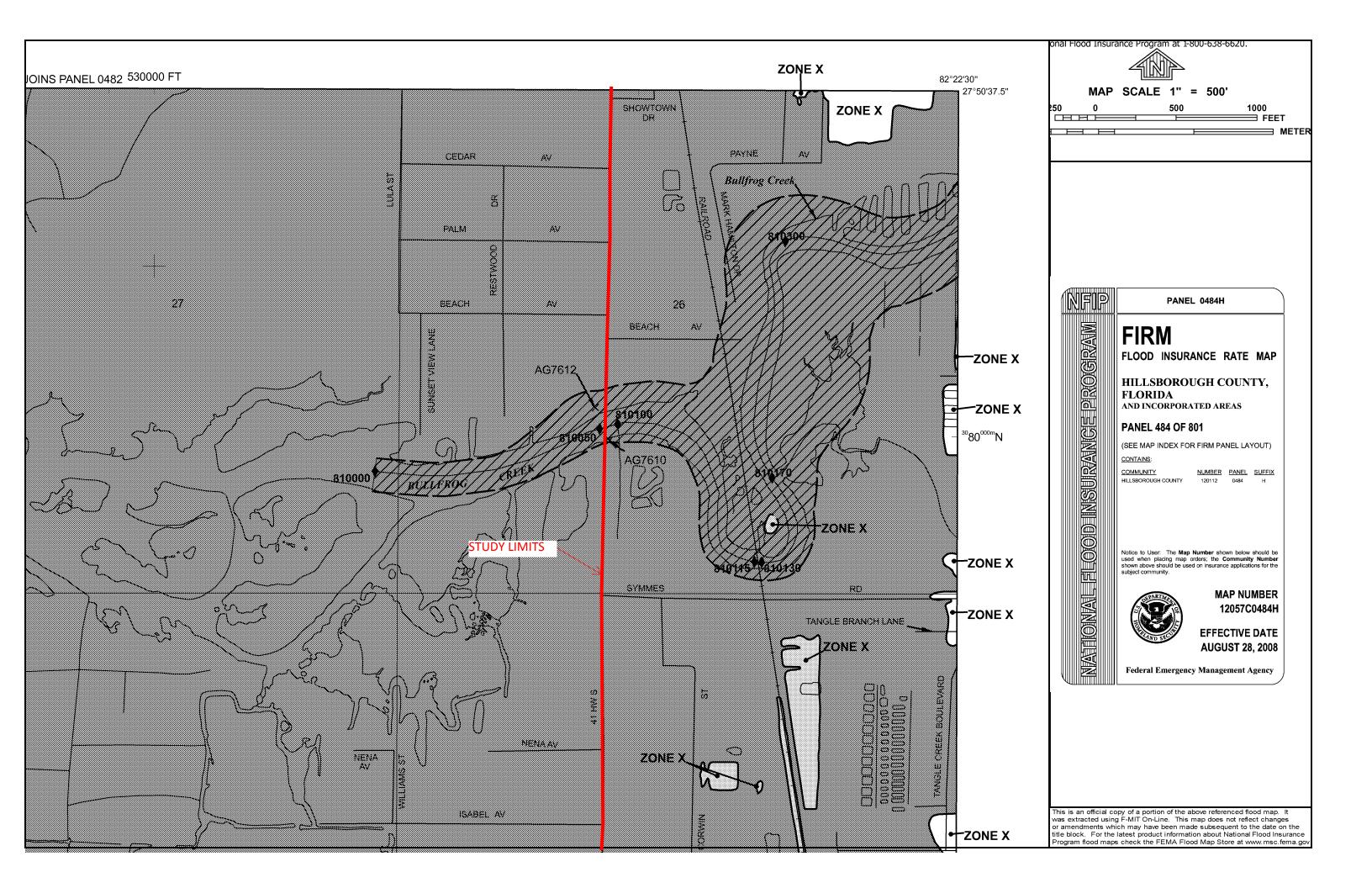
Based on above calculations, a wet pond would not be capable of meeting requirements for nutrient loading, since the removal efficiency of a wet pond is limited at or below 45%, therefore dry detention followed by wet detention is required.

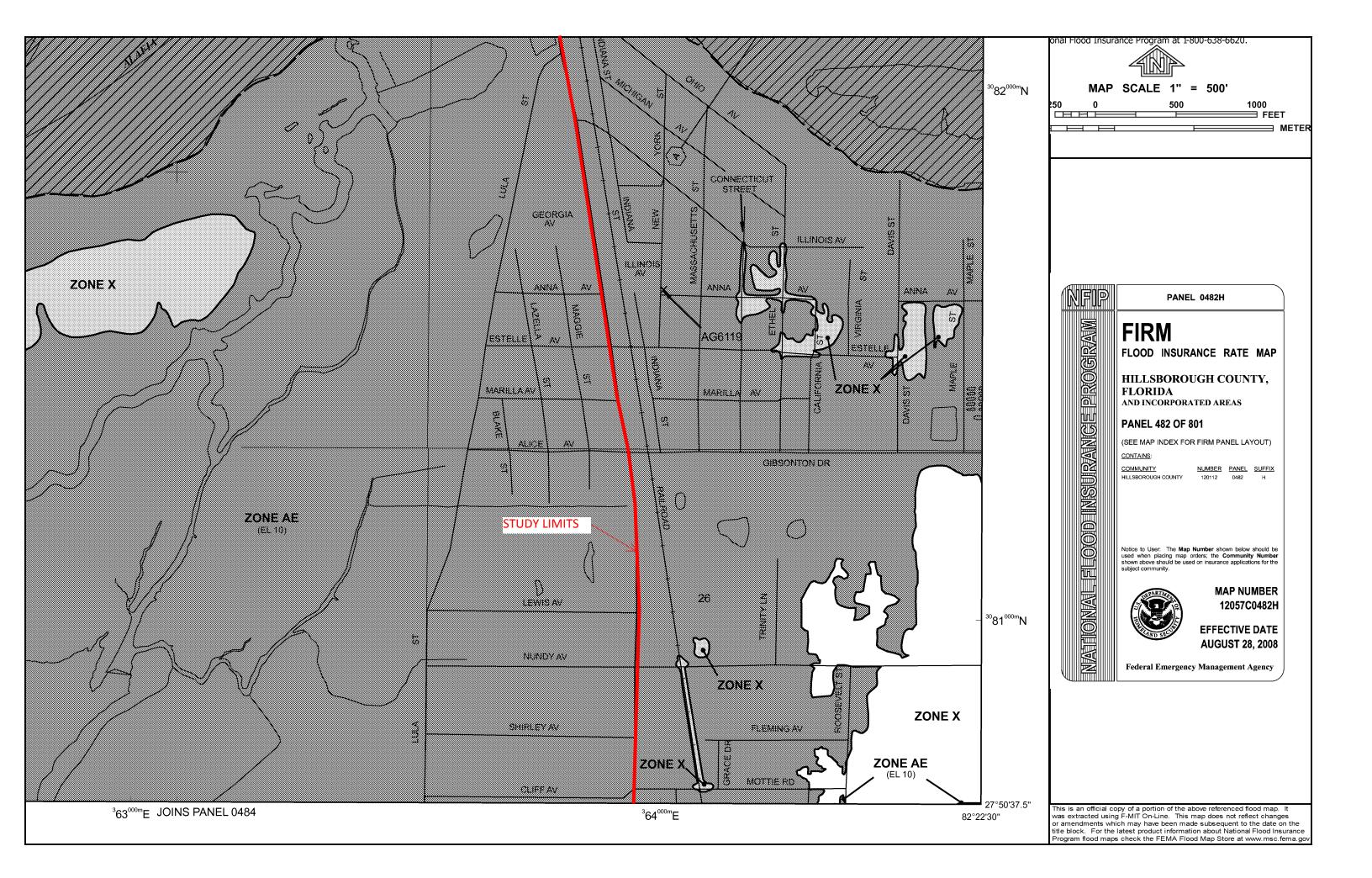
APPENDIX B

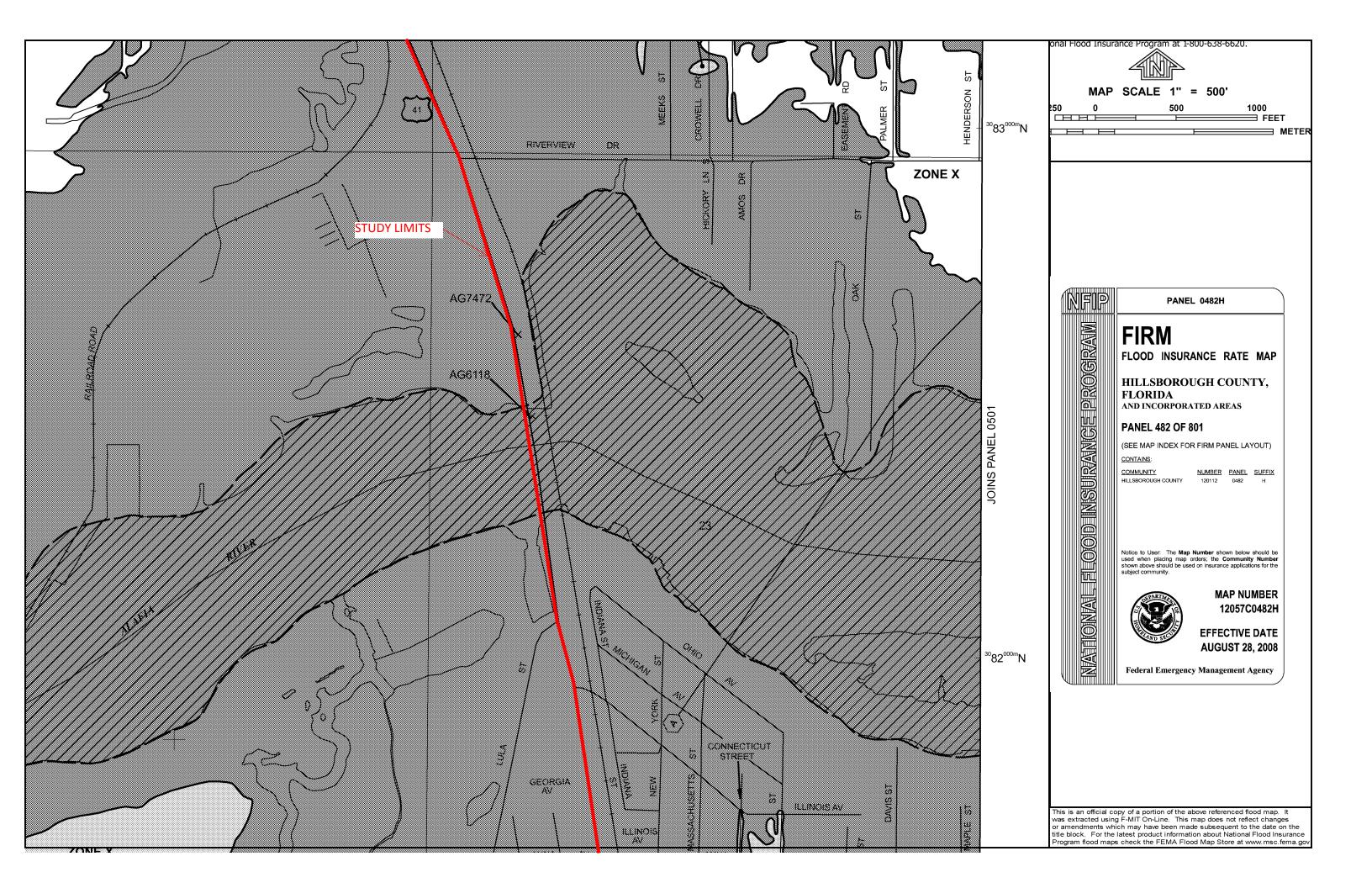
FEMA Mapping/Flood Investigation Documentation

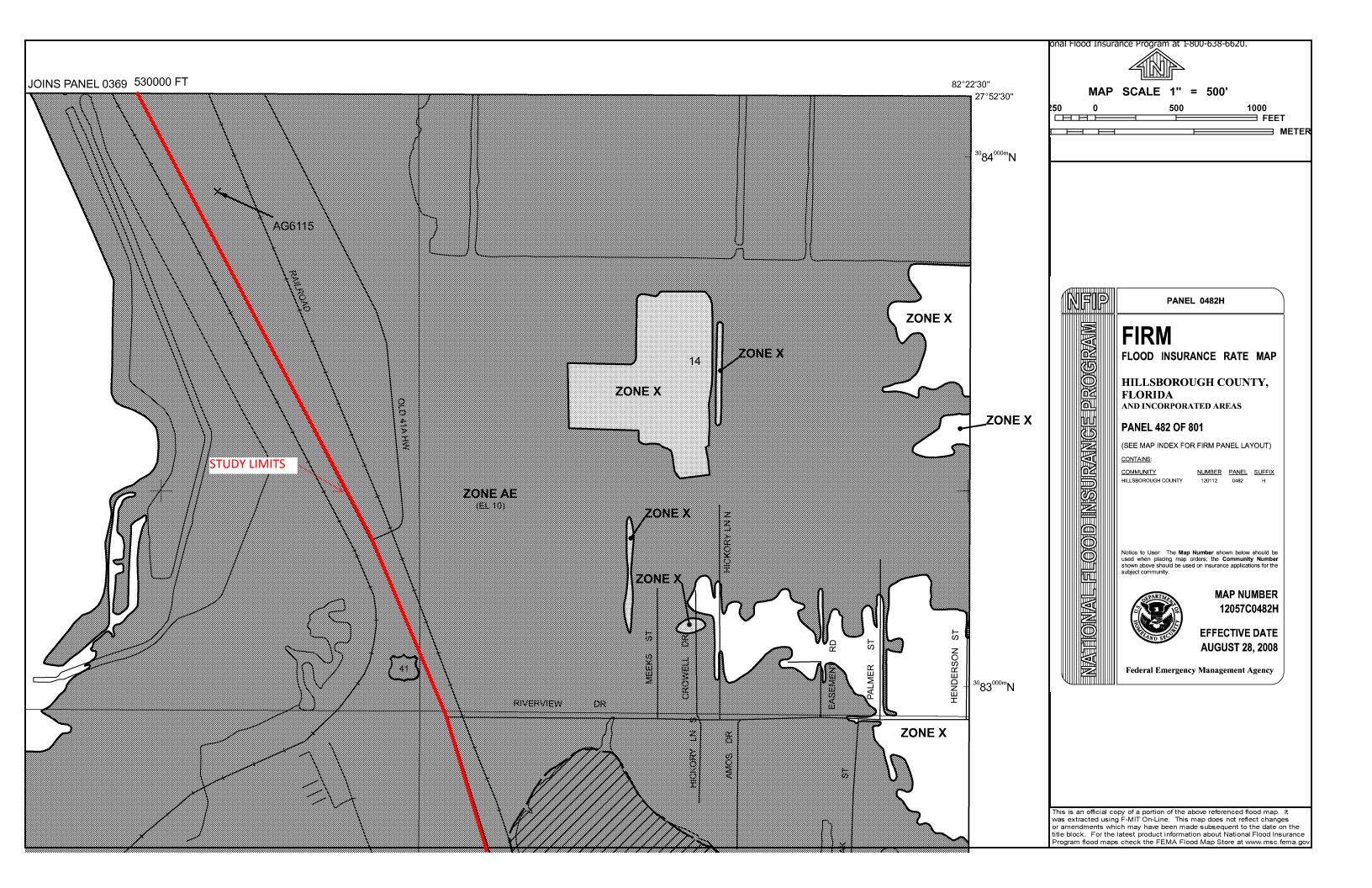


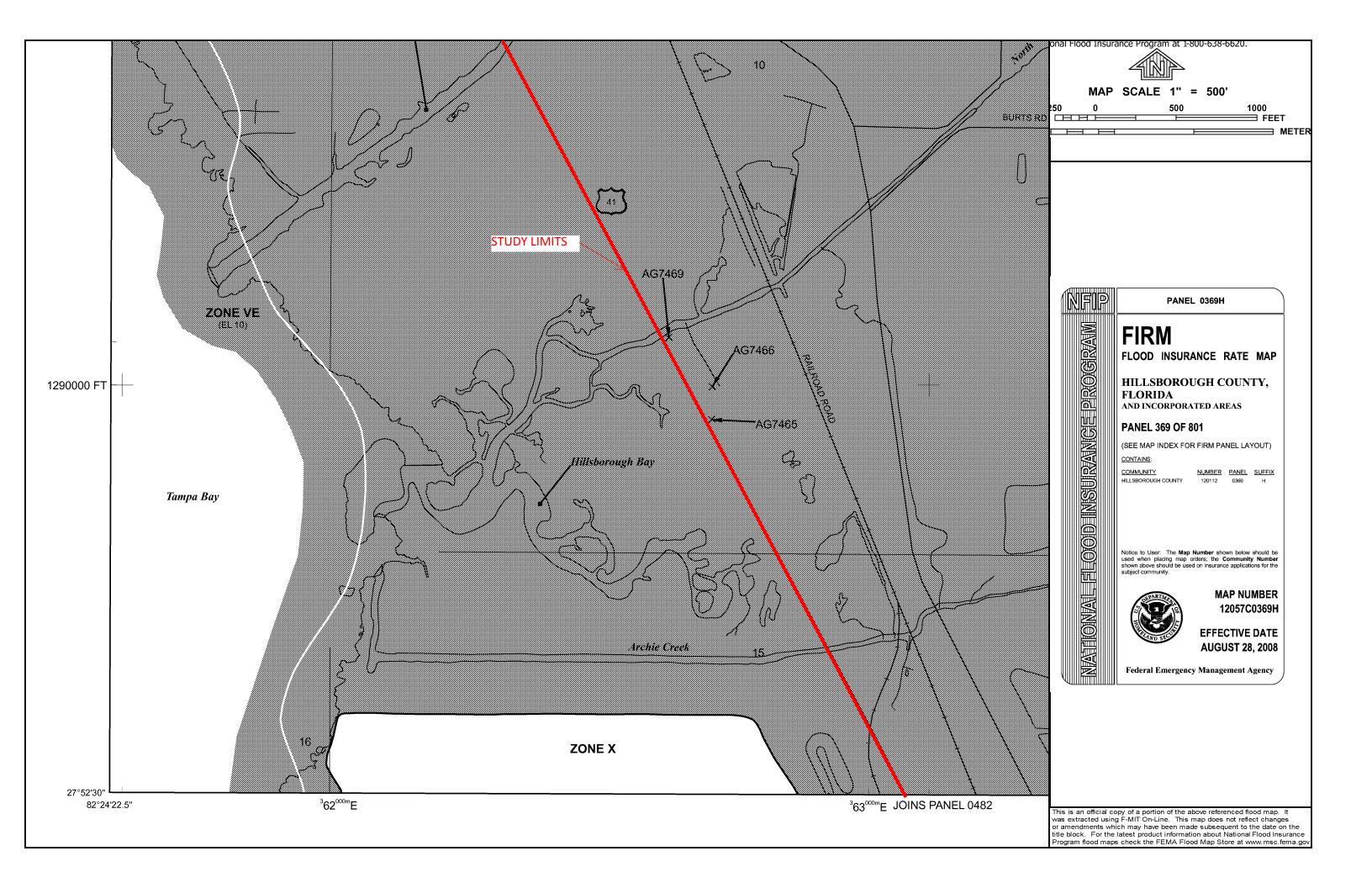


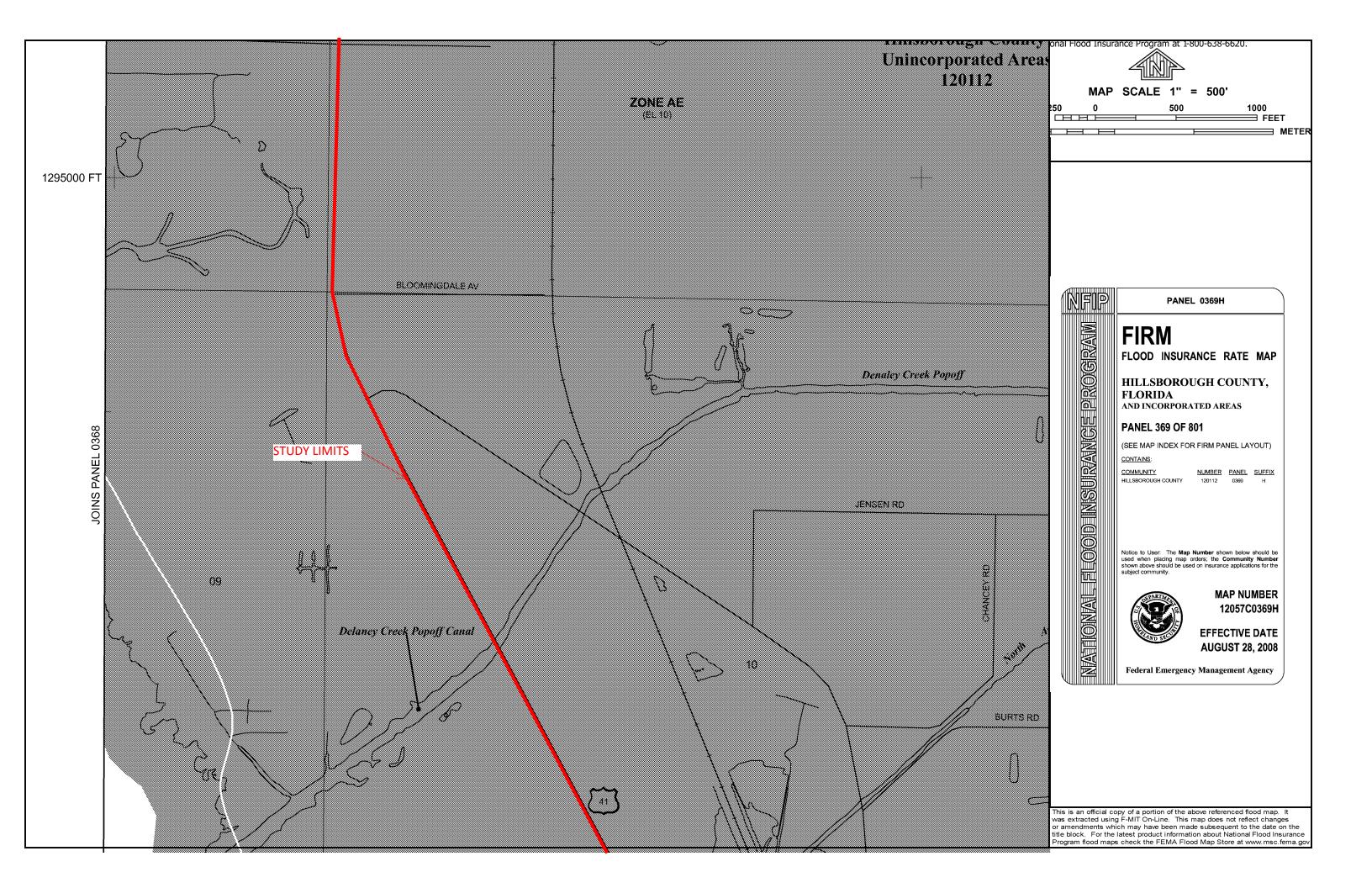


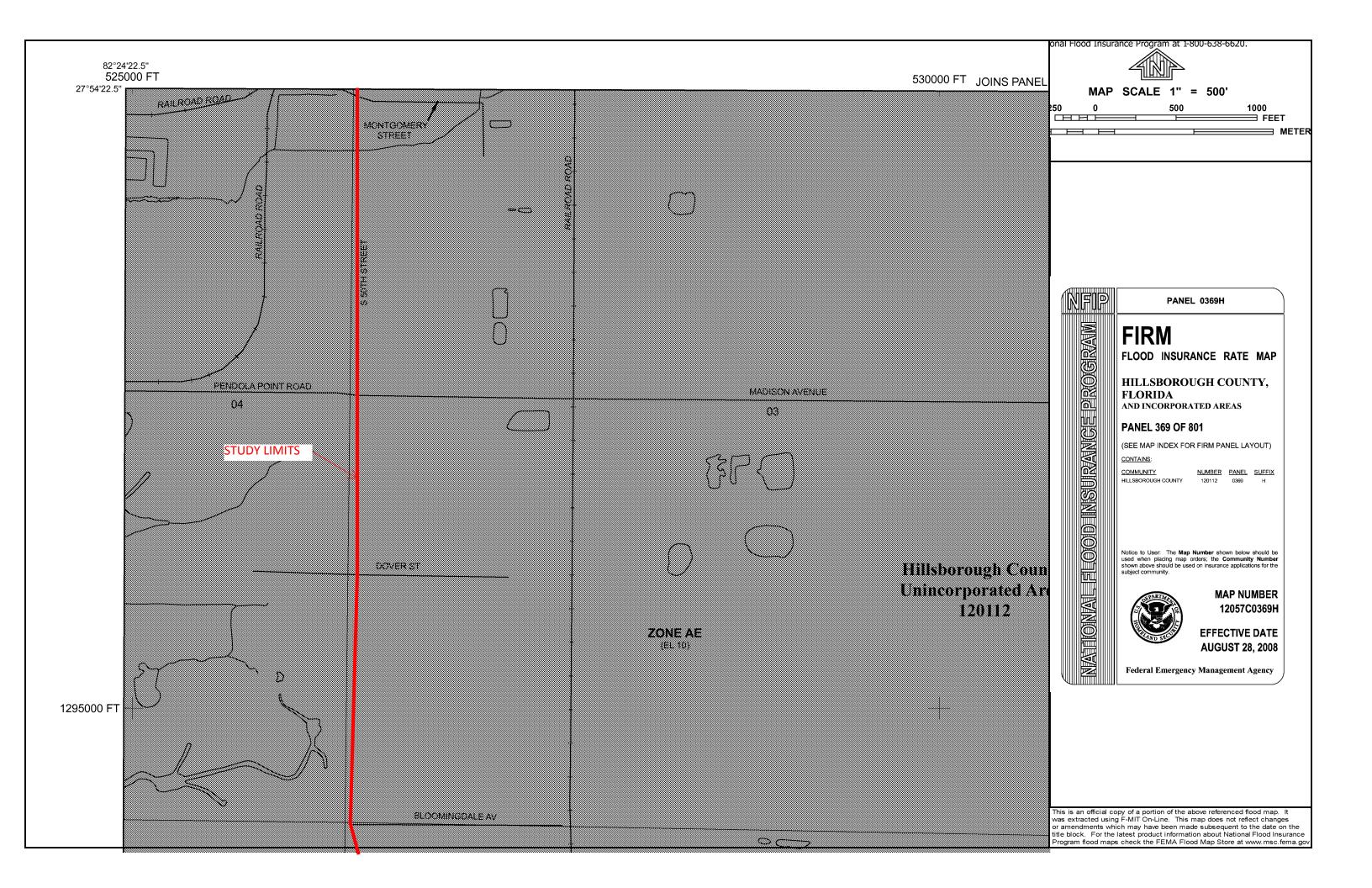


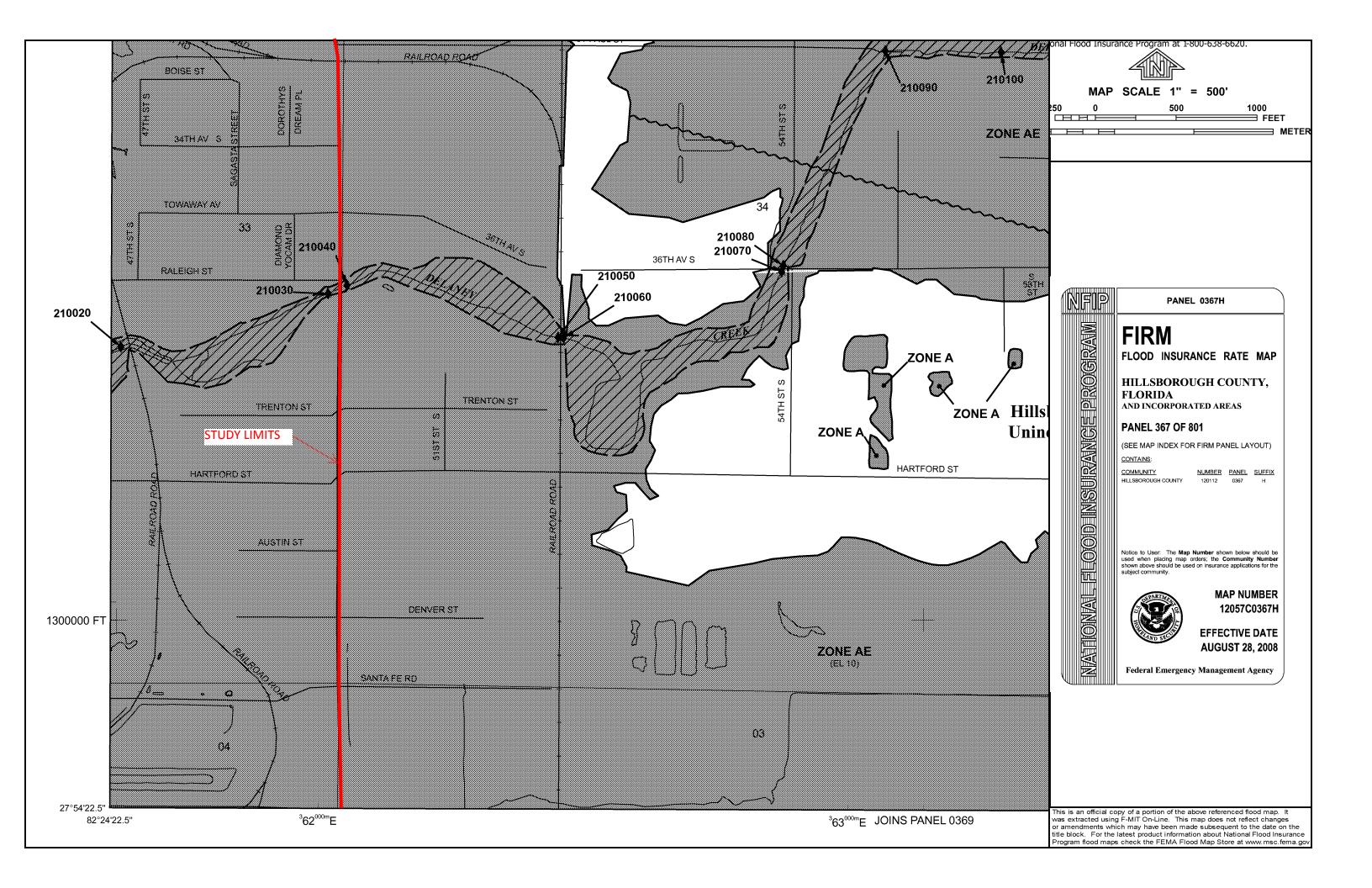


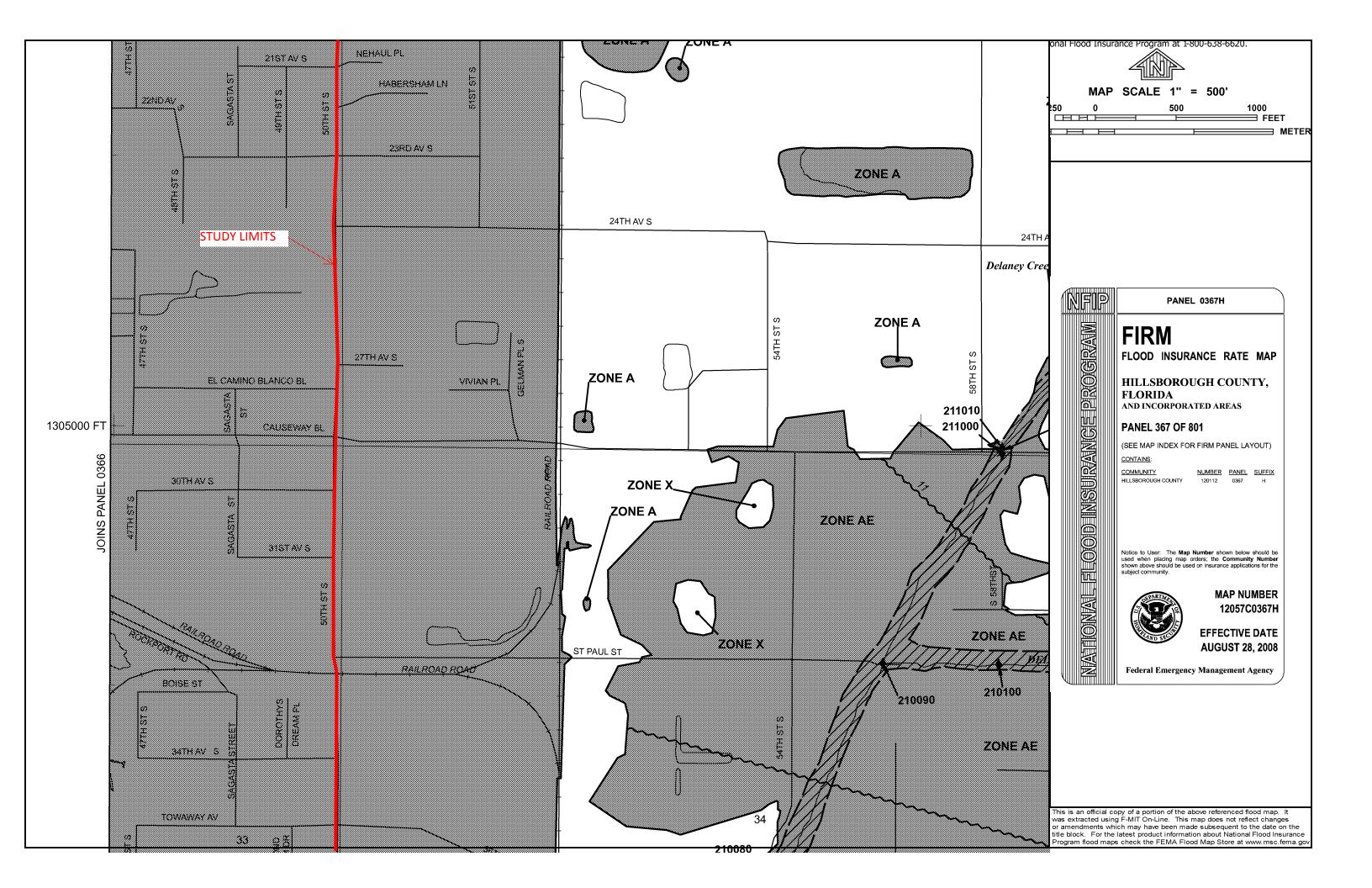


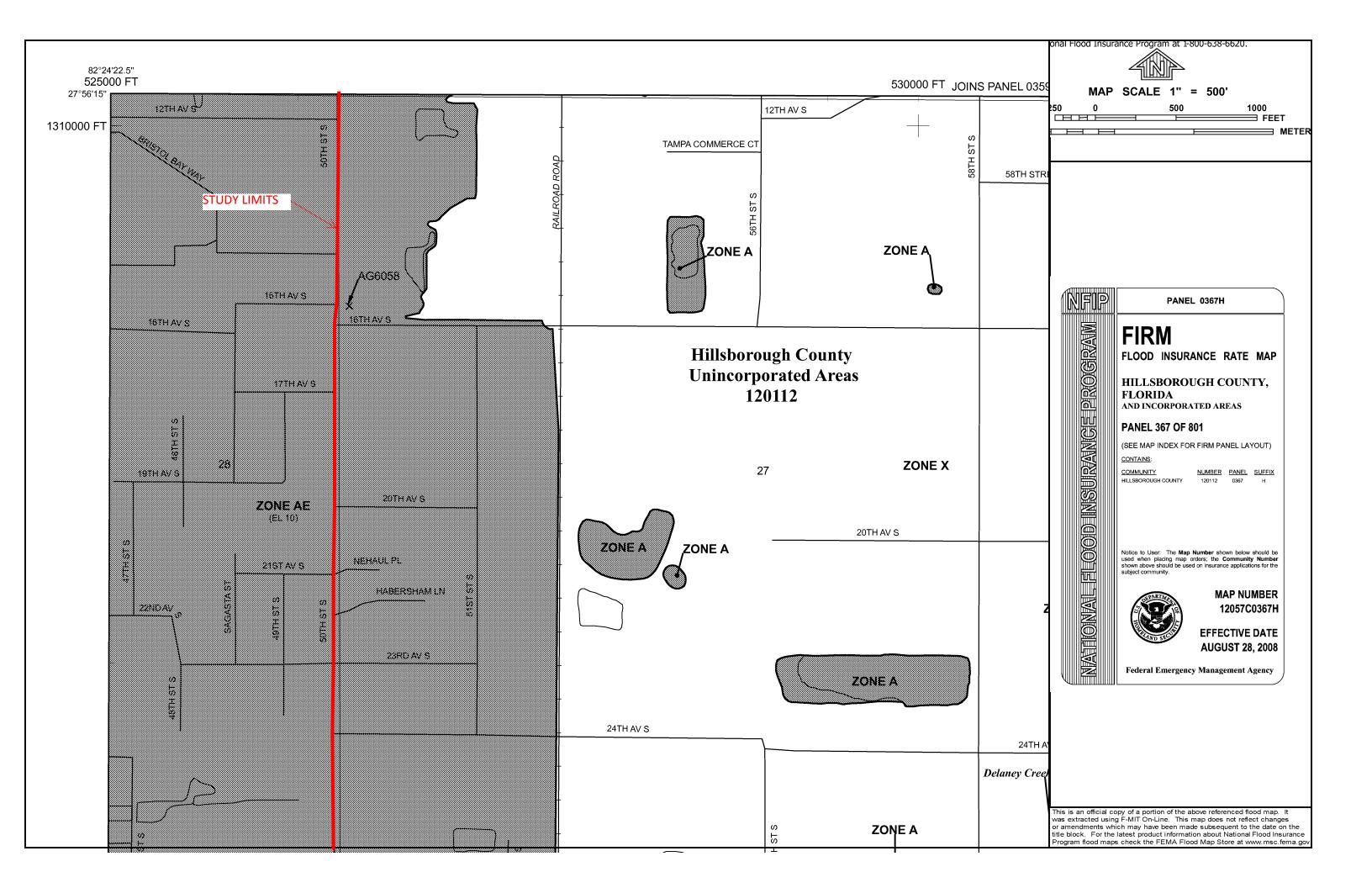


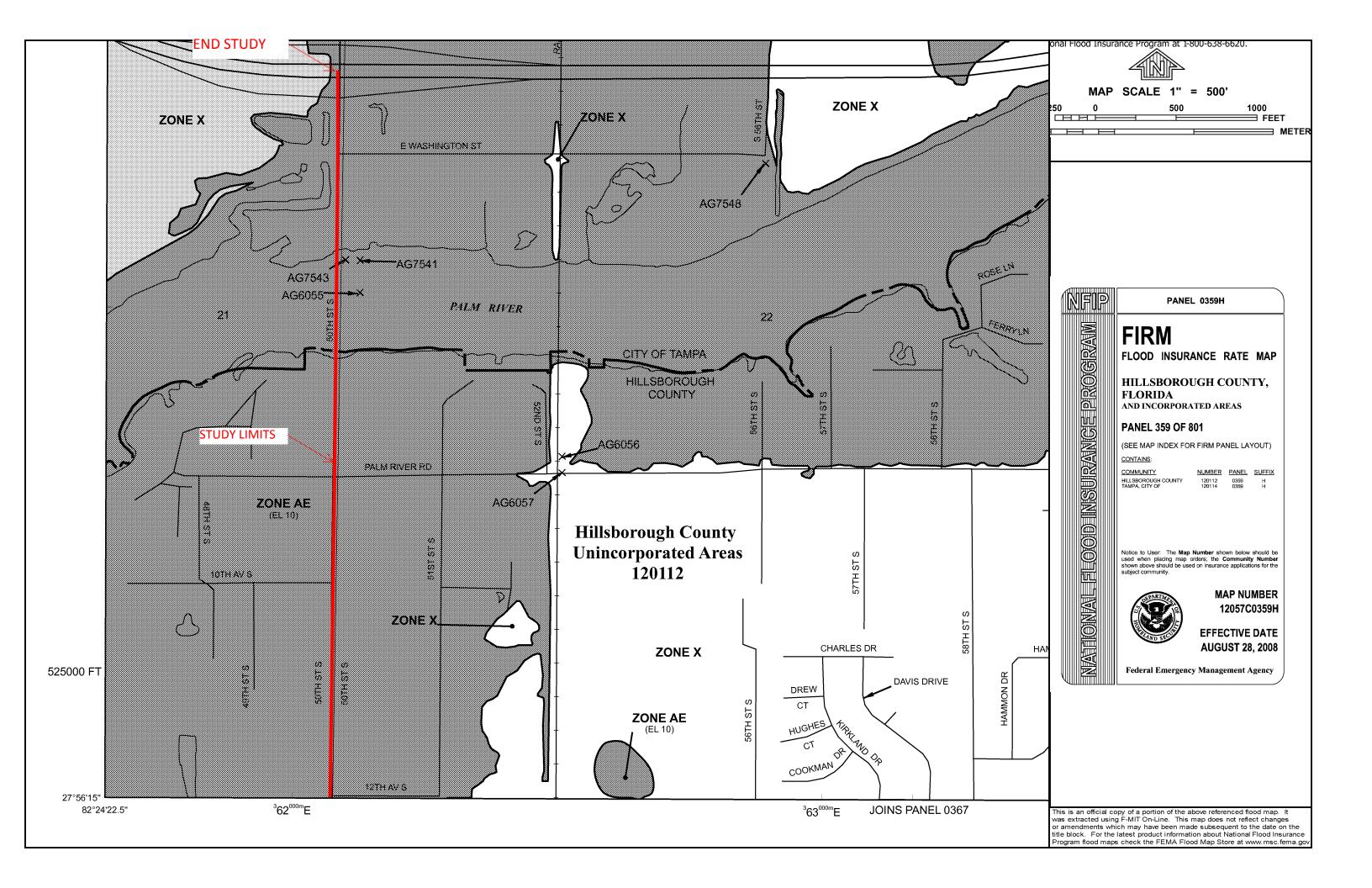


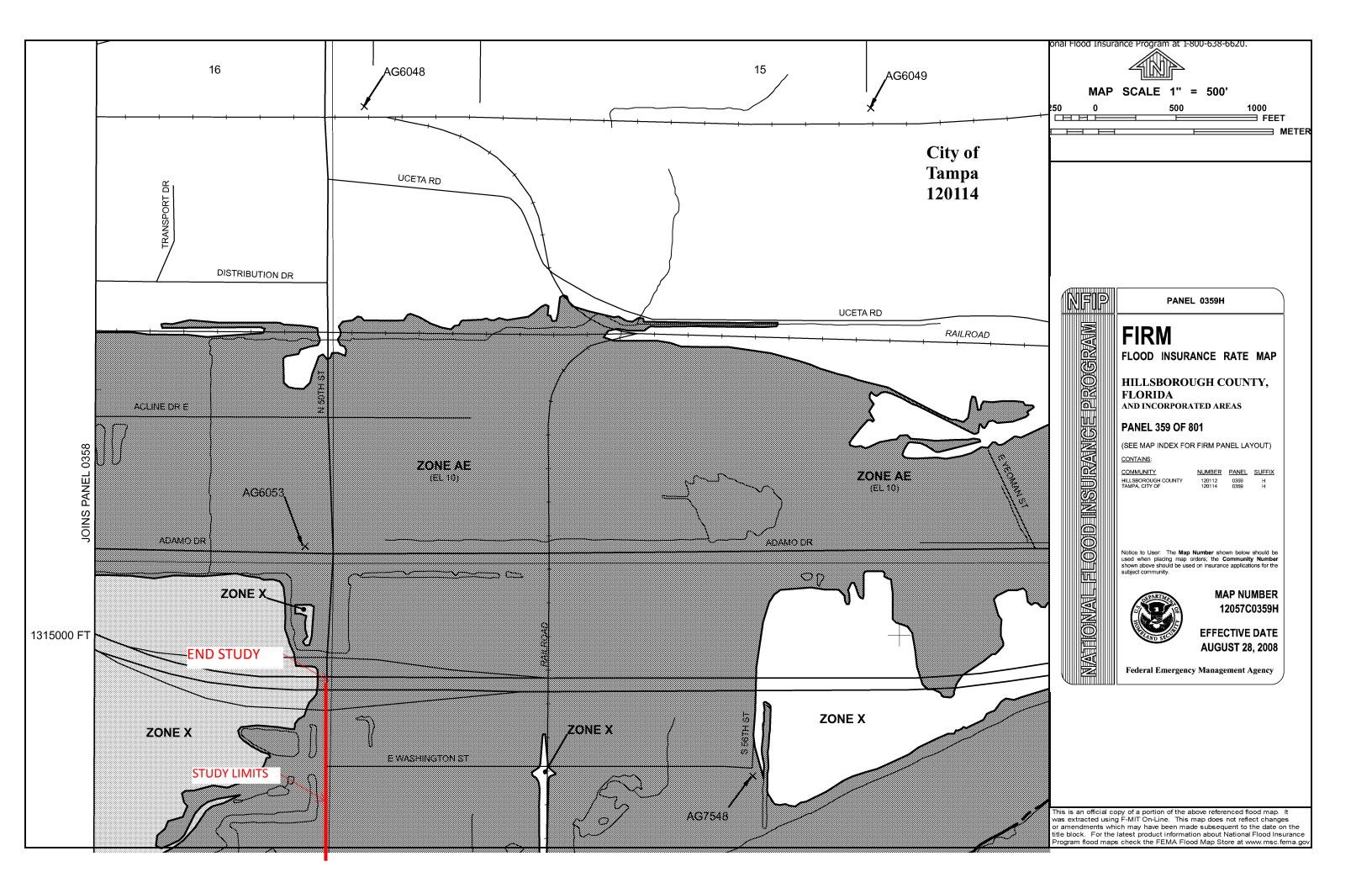












FLOOD INVESTIGATION INVENTORY SHEET

Flood Investigation # 1006222010925

Entry Date: 6/22/2010 2:06:31 PM

Revised Date:

Completed By: Stephanie Hildreth, HDR

SECTION 1: LOCATION

County - Hillsborough

State Road - SR 45, SR 599

Road Description - 4 lane(s), Principal Arterial, Roadside Ditches

Roadway Separation - Divided w/Non-Traversable Median

Direction of Travel - Two-Way

Functional System of Road - Urban

Specific Classification of Road - Principal Arterial

Roadway Drainage - Roadside Ditches

Flooding Condition - On-System

Local Road Subject to Flooding - Port Sutton Road

Business Name:

Business/Private Property Address Subject to Flooding -

4333 S 50th Street Tampa, FL 33619

Location:

Latitude: 27.906666 Longitude: -82.402259

Section/Township/Range - 4 / 30S / 19E

Project is Active - Yes

SECTION II: PROBLEM DESCRIPTION

Date of Original Complaint - 2/16/2009 Complainant Name - Bob Greene

Problem Description - Property Flooding

Details of the Problem - Flooding problem related to the business on the northwest corner of the intersection. The ditches on US 41 are shallow and tend to pop off through the property.

The owner stated that the water gets near the floor elevation and causes problems with the septic system onsite. He believes that the problem was caused with the recent resurfacing project which added curb ramps and pedestrian signals at the intersection of Port Sutton and US 41.

Frequency of Flooding - Several times per year Source for Frequency Data - Local Resident/Person Interviewed

Historic High Water - No historic high water data was available.

Water has come up to the building.

Flooding Event High Water - No event high water was recorded.

History of Problem - It is assumed that the problem has come up only after the widening of Port Sutton Road. Project 411276-1-52-04 (related projects 02 and 03). The project was completed in 2005 and tax records show that the property was sold in 2005.

SECTION III: PROBLEM ANALYSIS

Attachments

| Attachment | Attachment Type | Attachment Description | | | |
|-----------------------------------|-----------------------|---|--|--|--|
| Flooding_PortSutton.pdf | Other Data | Drainage Flooding Complaint Inventory Sheet | | | |
| project_ 1.pdf | Project Plans | Roadway plans for 411276-1-52-04 | | | |
| project_ 2.pdf | Project Plans | Signing and Pavement Marking Plans and Signalization Plans for 411276-1-52-04 | | | |
| aerial view_ port sutton.pdf | Aerial Photo | Aerial view | | | |
| swfwmd aerial_port sutton.pdf | SWFWMD Contour Map | SWFWMD Contour map | | | |
| cropped swfwmd_port sutton.pdf | SWFWMD Contour Map | Cropped SWFWMD aerial | | | |
| Deed_ port sutton.pdf | Other Data | Property Deed | | | |
| photos_port_sutton.pdf | Site Photo | Photos | | | |

SECTION IV: CONCLUSIONS AND RECOMMENDATIONS

Recommendation: It is not known for sure if the ramp work at this location caused the problem, but indications are that it may have added to a problem that already existed. The owner stated that he would be willing to provide FDOT a right of entry to install a pipe system to take water from the US 45 ditch to Port Sutton Road.

This problem cannon be adequately analyzed without a survey of the area to show flow direction and break over elevations.

Recommendation Date:

Project Ranking:

ROADWAY FLOODING MATRIX

Ranking of the roadway hazard level based on accident data, ADT, depth and location of water, and site specific factors.

(Weight Factor = 10)

0

Total Score

| | Ranking of the operational impacts (i.e. magnitude of vehicle speed reduction, ADT, frequency of flooding, availability of detour route, and cost to FDOT to handle problem, etc.) (Weight Factor = 7) | 0 |
|----------|---|---|
| | Ranking of the nuisance factor to the public and FDOT. (Weight Factor = 3) | 0 |
| | Ranking of the length of time before scheduled roadway improvements that will also provide remedy, are to be let to contract. | |
| | (Weight Factor = 5) | 0 |
| | Ranking of the costs to cure the problem, if any. (Weight Factor = 5) | 0 |
| | Total Score | 0 |
| <u>F</u> | Ranking of the potential financial impacts versus the flooding frequency that impacts the private property. (Weight Factor = 10) | 0 |
| | Ranking of the hazard level versus the flooding frequency that impacts the private property. (Weight Factor = 10) | 0 |
| | Ranking of the nuisance factor to the private property as well as FDOT. (Weight Factor = 5) | 0 |
| | Ranking of the costs to FDOT to cure the problem versus the financial impact to the private property if not cured. (Weight Factor = 10) | 0 |
| | Ranking of the length of time before scheduled roadway improvements that will also provide remedy, are to be let to contract. | 0 |
| | (Weight Factor = 5) | 0 |

0

FLOOD INVESTIGATION INVENTORY SHEET

Flood Investigation # 1005262005805

Entry Date: 5/26/2005 8:19:52 AM Revised Date: 8/2/2010 12:08:12 PM Completed By: Tom Ward, PBS&J

SECTION 1: LOCATION

County - Hillsborough State Road - SR 685

Road Description - 4 lane(s), null, Roadside Ditches **Roadway Separation -** Divided w/Traversable Median

Direction of Travel - Two-Way Functional System of Road - Rural Specific Classification of Road - null Roadway Drainage - Roadside Ditches

Flooding Condition - Off-System

Local Road Subject to Flooding - Business Name: Sandra O'Brian

Business/Private Property Address Subject to Flooding -

11860 SR 45

Gibsonton, FL 33534

Location:

Latitude: 27.828127 Longitude: -82.381384

Section/Township/Range - 35 / 30S / 19E

Project is Active - Yes

Associated Projects

| Project Date | State Project Number | Financial Project ID | Work Program ID | Project Description | Attachment |
|-----------------|-------------------------|-------------------------|-----------------------|------------------------|----------------------|
| 10/10/1991 | 10060 - 3580 | | 7113977 | Resurfacing | US_41_Sec- 06.pdf |

SECTION II: PROBLEM DESCRIPTION

Date of Original Complaint - 9/15/2004 Complainant Name - Sandra O'Brien Problem Description - Property Flooding

Details of the Problem - Renters complained to owner that during the heavy rains and the hurricane season of 2004, the ditch bottom inlet located near her home overtopped and flooded her front yard and the front porch of her home. The depth of flooding is not known. The water also traveled down the dirt road adjacent to her home, and impacted another home. The depth of flooding is not known. The inlet also overtopped at least one other time (exact date unknown by owner) in the past heavy rains.

Frequency of Flooding - Several times per year Source for Frequency Data - Local Resident/Person Interviewed

Historic High Water - A historic high water of located at Unknown was documented by Local Resident/Person Interviewed.

See above

Flooding Event High Water - No event high water was recorded.

History of Problem - Runoff from the US 41 Northbound Roadway travels to the roadside ditch, and then travels to ditch bottom inlets. According to the original drainage map from State Job No. 10060-3212, the flow travels from Florence Street south to the 10 ft x 8 ft box culvert located at Station 874+10. The drainage system from these plans shows roadside ditches along US 41 within the project limits. The drainage system was altered in 1991 when US 41 was resurfaced from Symmes Road to North of Big Bend Road, State Job No. 10060-3580. Ditch bottom inlets, side drains and pipe extensions in the ditches were added along portions of US 41 with this project. The drainage documentation from this project did not have the drainage basin delineated to compare current conditions with historic drainage patterns. The drainage pipes on the east side of US 41 from near the flooding site to the flooding site to the ultimate outfall at the 10 ft x 8 ft box culvert are all 18 inches in diameter. Although the extension of several 18-inch pipes caused some increase in head loss, this did not contribute substantially to flooding. The distance between flooding sites to the box culvert is approximately 700 feet. The creek at the box culvert is tidal. Based on comments from local residents, the highest tailwater ever witnessed was approximately 5.5 ft and did not get near this elevation during the reported flooding incident. The grate elevation of the ditch bottom inlet located adjacent to the property owner is 6.6 ft. Based on comments from residents, during the flooding complaint event, the water in the creek was near the elevation of the crown of the outfall pipe at elevation 3.7 ft. Based on drainage maps, field visits and contour aerials, the overall drainage basin limits for the area that contributes flow to the ditch in front of the flooding site are Florence Street to be the north, US 41 to the west, and CSX railroad to the east. Development in the basin area consists of mobile home parks, housing developments, and a fish hatchery. Much of this area is drained to the roadside ditch via lateral ditches that extend from the railroad ditch west to US 41 and are severely overgrown. Many of these ditches can popoff in several directions and it would be difficult to determine where runoff would flow without detailed modeling. In addition, the basin boundaries may have changed since the original US 41 project was constructed. The ditch on Florence Street is also overgrown and silted in. It is doubtful that much flow is being contributed from this ditch or the lateral inflow ditches. If ruunoff from the entire drainage area for the 10-year event is assumed to reach the pipes along US 41, the pipes are undersized. However, based on the indeterminate nature of the basin, a minimum discharge area was developed to evaluate the existing storm drain system. This area was developed by excluding areas conveyed by overgrown and silted in ditches. The drainage analysis of the existing storm drain system only includes US 41 runoff and portions of offsite runoff that run directly into the storm drain system. Based on this minimum drainage area, energy losses in the pipes associated with a 10-year event are 1.03 ft from the outfall to the subject property. There is 2.9 ft of head available between the inlet top (6.6 ft) and the tailwater elevation (3.7 ft). At the highest tailwater witnessed (5.5 ft), this would put the hydraulice grade line at the inlet top.

Persons Interviewed

Site Visit Date - 12/1/2004 Site Inspection By - Resident Last Name, Renter Interviewee(s) - Shayne Paynter, PBSJ Site Visit Conditions - Not Applicable

Observed High Water - No observed high water was observed on the date of the site visit.

Site Visit Details - Shayne Paynter met the residence on December 1, 2004 at the residence of the flooding and field reviewed the site on the same day. The FDOT 7 Tampa Maintenance office was visited to obtain plans and inquire as to flooding issues at this site. Maintenance personnel could not recall any

flooding problem at this location.

SECTION III: PROBLEM ANALYSIS

Attachments

| Attachment | Attachment Type | Attachment Description |
|--|-------------------------|---|
| US_41_Sec-01.pdf | Other Data | Drainage Complaint Inventory Work Sheet |
| US_41_Sec-04.pdf | FDOT Drainage Map | Drainage Map (SPN: 10060-3212) |
| US_41_Sec-05.pdf | Other Data | FDOT Correspondence not available |
| US_41_Sec-06.pdf | Project Plans | Key Sheet, Qunatities Sheet & plan sheet at area of flooding. |
| US_41_Sec-07.pdf | Other Data | Copies of Any FDOT, County, or City Drainage Studies not available. |
| Review of Drainage Complaint Investigation.pdf | Other Data | Review of Drainage Complaint Investigation |
| US41.pdf | Site Map | Location Map |
| REG.pdf | Project Plans | 10060-3580 partial plans |
| Hill 10060 3212 SR 45 US 41 Obrien.pdf | Other Data | Drainage Complaint Investigation Report |

SECTION IV: CONCLUSIONS AND RECOMMENDATIONS

Recommendation: The ditch from the box culvert at Station 874+00 to the mitered end section at Station 875+50 is overgrown and should be cleared to allow flow from the storm drain system to enter the outfall effectively. Also, many of the grate inlets are blocked with overgrown grass that prevents flow in the ditch from entering the inlet effectively, especially the inlet located just south of the flooding complaint at Station 881+40. From the flooding complaint site at Station 882+00, to south to the Box Culvert at Station 874+00, the existing 18" pipes should be inspected for any obstructions and all pipes should be desilted. The ditch bottom inlet located at the flooding site should be modified to include traversable slots and the immediate area should be graded to drain to these slots. The inlet elevation is currently very close to the floor elevation of the residence located adjacent to the inlet. Adding slots and grading the ground between the right-of-way and the inlet to slope the terrian towards the inlet will help to prevent water from flowing outside the right-of-way. Cleaning ditches and clearing ditch inlet grates will help alleviate the flooding problem by allowing water to enter the inlets effectively and by maximizing the capacity fo the system. All the 18" pipes carry flow south to a MES at Station 875+67.60, before entering the creek. It should be noted that the rainfall associated with the 2004 hurricane season and the resulting flooding complaint

exceeded the design parameters for the drainage system, which is estimated to be a 10-year event, and flooding will still occur as result of very large rainfall events. In summary, the following steps should be taken to address the flooding complaint: 1) Inspect all pipes from the flooding complaint site to the box culvert 2) Clear any obstructions and desilt pipes 3) Clear all inlet tops from the flooding site to the box culvert that have excessive grass growth or debris 4) Add traversable slots to the existing inlet in front of the property in question and grade the existing ground near the inlet to direct runoff to flow into the inlet.

Recommendation Date: 5/2/2005

Project Ranking:

ROADWAY FLOODING MATRIX

| Ranking of the roadway hazard level based on accident data, ADT, depth and location of water, and site specific factors. (Weight Factor = 10) | 0 |
|---|---|
| Ranking of the operational impacts (i.e. magnitude of vehicle speed reduction, ADT, frequency of flooding, availability of detour route, and cost to FDOT to handle problem, etc.) (Weight Factor = 7) | 0 |
| Ranking of the nuisance factor to the public and FDOT. (Weight Factor = 3) | 0 |
| Ranking of the length of time before scheduled roadway improvements that will also provide remedy, are to be let to contract. | |
| (Weight Factor = 5) | 0 |
| Ranking of the costs to cure the problem, if any. (Weight Factor = 5) | 0 |
| Total Score | 0 |
| | |
| PRIVATE PROPERTY FLOODING MATRIX | |
| Ranking of the potential financial impacts versus the flooding frequency that impacts the private property. (Weight Factor = 10) | 0 |
| Ranking of the hazard level versus the flooding frequency that impacts the private property. (Weight Factor = 10) | 0 |
| Ranking of the nuisance factor to the private property as well as | |
| FDOT. (Weight Factor = 5) | 0 |
| Ranking of the costs to FDOT to cure the problem versus the financial impact to the private property if not cured. (Weight Factor = 10) | 0 |
| Ranking of the length of time before scheduled roadway improvements that will also provide remedy, are to be let to contract. | |
| (Weight Factor = 5) | 0 |
| Total Score | 0 |

FLOOD INVESTIGATION INVENTORY SHEET

Flood Investigation # 1001032008834

Entry Date: 1/3/2008 8:41:11 AM Revised Date: 7/13/2010 11:29:51 AM Completed By: Hiren Patel, PBS&J

SECTION 1: LOCATION

County - Hillsborough State Road - SR 45, SR 599

Road Description - 4 lane(s), Principal Arterial, Roadside Ditches

Roadway Separation - Divided w/Non-Traversable Median

Direction of Travel - Two-Way **Functional System of Road -** Urban

Specific Classification of Road - Principal Arterial

Roadway Drainage - Roadside Ditches

Flooding Condition - Off-System

Local Road Subject to Flooding - Ohio Street

Business Name:

Business/Private Property Address Subject to Flooding -

12130 US 41 Gibsonton , FL 33534

Location:

Latitude: 27.822308 Longitude: -82.381614

Section/Township/Range - 35 / 30S / 19E

Project is Active - Yes

SECTION II: PROBLEM DESCRIPTION

Date of Original Complaint - 8/1/2007 Complainant Name - Gerry Javier Problem Description - Unknown

Details of the Problem - 3" PVC storm drain pipe discharging onto FDOT ROW. A drainage connection permit is not currently on file.

Frequency of Flooding - Unknown Source for Frequency Data - Unknown

Historic High Water - No historic high water data was available.

Flooding Event High Water - No event high water was recorded.

History of Problem - First reported by Gerry Javier FDOT Maintenance 08/01/2007 during routine maintenance of the right ditch fronting the property of concern.

Other Communications

| Communication Date | Туре | Communication From | Communication To | Communication Attachment Name |
|--------------------|-------|-------------------------|---------------------------|----------------------------------|
| 10/3/2007 | Email | Mark Micikas , PBS&J | Andrew Stevens, PBS&J | 25810416_Email100307.pdf |
| 10/3/2007 | Email | Mark Micikas , PBS&J | Andrew Stevens , PBS&J | 258104340 EmailOct0307.pdf |

SECTION III: PROBLEM ANALYSIS

Current Problem Analysis

Current Problem Analysis: Stormwater runoff for Eastwood Estates MHP is collected by storm drain and pumped to two outfall points; the FDOT R/W ditch; Ohio St. ditch. According to James Crowell (Property Maintenance), the storm drain pumps are turned on with floats once runoff depths begin to inundate the roadway within the park. The pumps appear to have been in place since the park inception prior to 1986. There is no history of apparent flooding or excessive erosion with in the S.R. 45 R/W due to the stormwater pumping.

Outfall Description: Manmade Channel or Ditch

Responsible Entity for Maintenance of Outfall: FDOT

Attachments

| Attachment | Attachment Type | Attachment Description | | | | |
|----------------------------|--------------------|------------------------|--|--|--|--|
| 258103627_SWFWMD023119.pdf | SWFWMD Contour Map | | | | | |
| 25810373_SWFWMD353019.pdf | SWFWMD Contour Map | | | | | |
| 258103858_Sitephotos.pdf | Site Photo | | | | | |
| 258103943_Fieldnotes.pdf | Other Data | Field Notes | | | | |

SECTION IV: CONCLUSIONS AND RECOMMENDATIONS

Recommendation: No action is recommended at this time due to the Eastwood Estates MHP and stormwater system being in place prior to 1986 along with the SWFWMD aerials showing historic water patterns consistent with the system in place.

Recommendation Date:

Project Ranking:

Total Score

ROADWAY FLOODING MATRIX

| | Ranking of the roadway hazard level based on accident data, ADT, depth and location of water, and site specific factors. (Weight Factor = 10) | 0 |
|----------|---|---|
| | Ranking of the operational impacts (i.e. magnitude of vehicle speed reduction, ADT, frequency of flooding, availability of detour route, and cost to FDOT to handle problem, etc.) (Weight Factor = 7) | 0 |
| | Ranking of the nuisance factor to the public and FDOT. (Weight Factor = 3) | 0 |
| | Ranking of the length of time before scheduled roadway improvements that will also provide remedy, are to be let to contract. | |
| | (Weight Factor = 5) | 0 |
| | Ranking of the costs to cure the problem, if any. (Weight Factor = 5) | 0 |
| | Total Score | 0 |
| | | |
| <u>I</u> | PRIVATE PROPERTY FLOODING MATRIX | |
| | Ranking of the potential financial impacts versus the flooding frequency that impacts the private property. (Weight Factor = 10) | 0 |
| | Ranking of the hazard level versus the flooding frequency that impacts the private property. (Weight Factor = 10) | 0 |
| | Ranking of the nuisance factor to the private property as well as FDOT. | |
| | (Weight Factor = 5) | 0 |
| | Ranking of the costs to FDOT to cure the problem versus the financial impact to the private property if not cured. (Weight Factor = 10) | 0 |
| | Ranking of the length of time before scheduled roadway improvements that will also provide remedy, are to be let to contract. | |
| | (Weight Factor = 5) | 0 |
| | | |

0

APPENDIX C

Hillsborough County Riverine Floodplain Elevations

Floodplain Encroachment and Compensation Calculation Summary Table 4-2 Calculation Basis

Basin 3

- Column 1: Length of basin times width of both sides
- Column 2: Encroachment area times depth of 0.5' (Based on estimated average fill below floodplain depth)
- Column 3: Encroachment volume times 1.25 (Based on 1' depth to water table and increased by 25% for grading)

Basin 4

- Column 1: Station 892+40.00 to 897+00.00 (460') times width of both sides
- Column 2: Encroachment area times depth of 0.5' (Based on estimated average fill below floodplain depth)
- Column 3: Encroachment volume times 1.25 (Based on 1' depth to water table and increased by 25% for grading)

Basin 10

- Column 1: Length of basin times width of both sides
- Column 2: Encroachment area times depth of 2.0' (Based on estimated average fill below floodplain depth)
- Column 3: Encroachment volume times 1.25 (Based on 1' depth to water table and increased by 25% for grading)

Basin 11

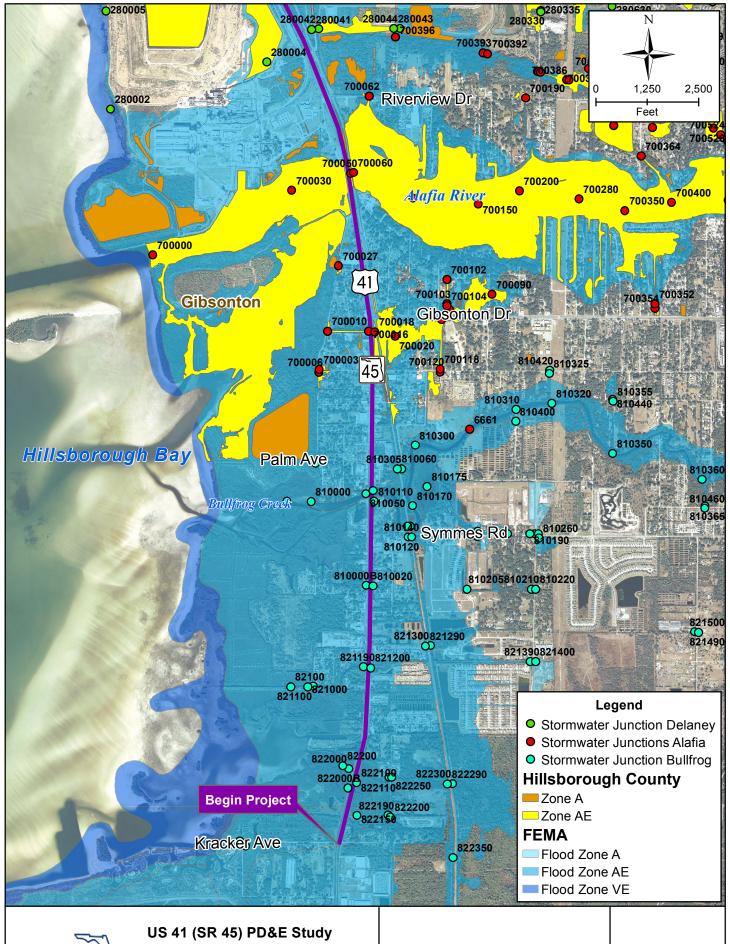
- Column 1: 700 ft times width of one side + rest of basin length times width of both sides
- Column 2: Encroachment area times depth of 0.5' (Based on estimated average fill below floodplain depth)
- Column 3: Encroachment volume times 1.25 (Based on 1' depth to water table and increased by 25% for grading)

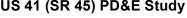
Basin 12

- Column 1: Length of basin times width of both sides
- Column 2: Encroachment area times depth of 1.0' (Based on estimated average fill below floodplain depth)
- Column 3: Encroachment volume times 1.25 (Based on 1' depth to water table and increased by 25% for grading)

Basin 13

- Column 1: Length of basin times width of both sides
- Column 2: Encroachment area times depth of 0.5' (Based on estimated average fill below floodplain depth)
- Column 3: Encroachment volume times 1.25 (Based on 1' depth to water table and increased by 25% for grading)



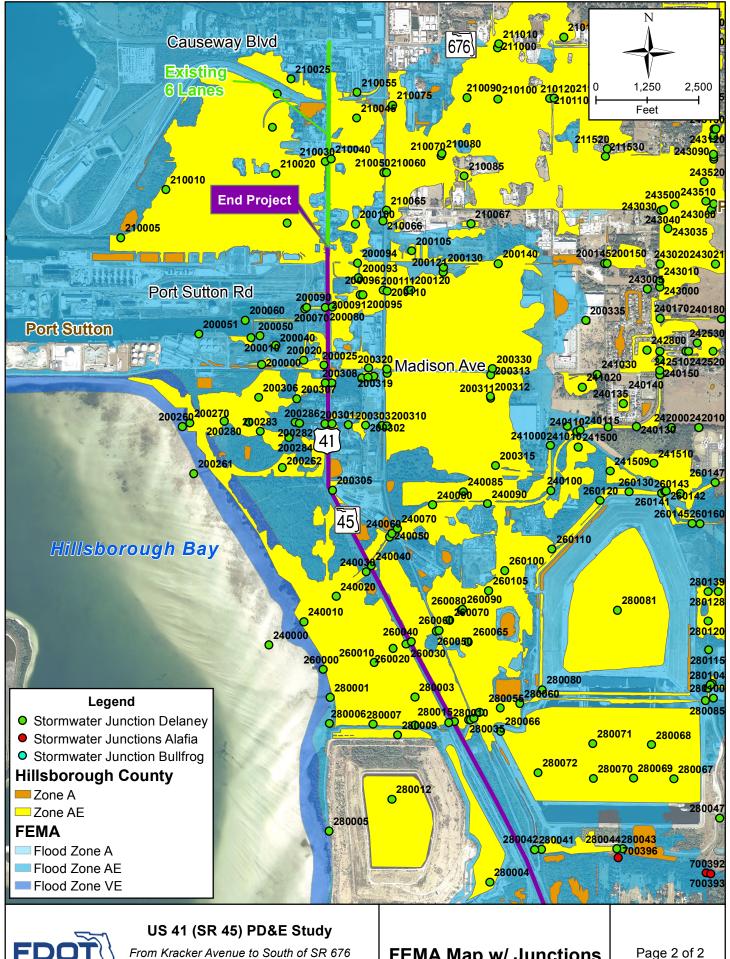


From Kracker Avenue to South of SR 676 (Causeway Boulevard)

WPI Segment No. 430056 1 - Hillsborough County

FEMA Map w/ Junctions

Page 1 of 2





(Causeway Boulevard)

WPI Segment No. 430056 1 - Hillsborough County

FEMA Map w/ Junctions

6.3 EXISTING CONDITIONS MODEL SIMULATION RESULTS

The 2.33-, 5-, 10-, 25-, 50- and 100-year design rainfall storm events, each with a design duration of 24 hours, were input to the calibrated model for simulation of peak flood elevations in channels and at structures. Water surface profiles have been generated to show maximum water level elevation for these events. These profiles are presented for each major conveyance system in Exhibits 6-1a through 6-1s. These conditions represent the existing baseline condition (no action plan) flooding response for the Bullfrog Creek/Wolf Branch watershed. A summary of simulated peak stages at all model nodes is presented in Table 6.2 for each design storm simulation.

Table 6.2
DESIGN STORM MODEL OUTPUT SUMMARY

| I | DESIGN STORM MODEL OUTPUT SUMMARY | | | | | | | |
|---------------|-----------------------------------|-------------|-------------------|------------------|----------------|----------|--|--|
| Model Node ID | | Existing Co | onditions Design | Flood Elevations | s (Feet, NGVD) | | | |
| | 2.33-year | 5-year | 10-year | 25-year | 50-year | 100-year | | |
| | | | Lower Bullfrog Cr | eek | | | | |
| 810000 | 2.2 | 2.3 | 2.6 | 2.9 | 3.3 | 3.6 | | |
| 810020 | 4.1 | 4.3 | 4.6 | 4.9 | 5.3 | 5.5 | | |
| 810040 | 2.5 | 3.0 | 3.8 | 4.8 | 5.1 | 5.1 | | |
| 810050 | 2.9 | 3.4 | 4.1 | 4.6 | 5.5 | 6.1 | | |
| 810060 | 3.3 | 3.6 | 4.3 | 4.8 | 5.8 | 7.4 | | |
| 810100 | 2.9 | 3.5 | 4.2 | 4.7 | 5.8 | 6.5 | | |
| 810110 | 2.9 | 3.5 | 4.2 | 4.7 | 5.8 | 6.5 | | |
| 810115 | 3.6 | 4.2 | 5.1 | 5.7 | 6.7 | 7.4 | | |
| 810120 | 3.7 | 4.2 | 5.1 | 5.7 | 6.7 | 7.4 | | |
| 810130 | 3.8 | 4.5 | 5.5 | 6.3 | 7.8 | 7.5 | | |
| 810140 | 4.2 | 4.5 | 5.5 | 6.3 | 7.8 | 7.5 | | |
| 810170 | 4.0 | 4.8 | 5.8 | 6.6 | 8.0 | 8.0 | | |
| 810175 | 4.0 | 4.8 | 5.8 | 6.6 | 8.0 | 8.0 | | |
| 810180 | 4.0 | 4.8 | 5.8 | 6.6 | 8.0 | 8.0 | | |
| 810185 | 5.0 | 5.2 | 5.8 | 6.6 | 8.0 | 8.0 | | |
| 810190 | 8.7 | 8.9 | 9.3 | 9.5 | 10.0 | 10.2 | | |
| 810195 | 11.1 | 11.9 | 12.1 | 12.2 | 12.2 | 12.2 | | |
| 810200 | 5.0 | 5.5 | 6.1 | 6.7 | 8.0 | 8.2 | | |
| 810205 | 5.2 | 5.6 | 6.2 | 6.8 | 8.0 | 8.2 | | |
| 810210 | 6.9 | 7.2 | 7.4 | 7.6 | 8.0 | 8.4 | | |
| 810220 | 9.5 | 9.9 | 10.4 | 10.9 | 11.8 | 12.5 | | |
| 810240 | 11.4 | 12.5 | 13.3 | 13.6 | 13.6 | 13.6 | | |
| 810260 | 12.3 | 13.5 | 13.7 | 13.7 | 13.8 | 13.9 | | |
| 810300 | 4.4 | 5.2 | 6.3 | 7.1 | 8.5 | 8.6 | | |
| 810305 | 4.4 | 5.2 | 5.6 | 6.3 | 7.8 | 7.5 | | |
| 810310 | 5.2 | 6.1 | 7.3 | 8.2 | 9.7 | 10.0 | | |
| 810320 | 5.3 | 6.2 | 7.5 | 8.3 | 9.8 | 10.2 | | |
| 810325 | 7.7 | 7.8 | 7.9 | 8.3 | 9.8 | 10.2 | | |
| 810350 | 8.8 | 10.1 | 11.8 | 12.7 | 14.2 | 14.9 | | |
| 810355 | 10.2 | 10.3 | 11.8 | 12.7 | 14.2 | 14.9 | | |
| 810360 | 10.2 | 11.5 | 13.2 | 14.2 | 15.8 | 16.6 | | |
| 810365 | 12.6 | 12.8 | 13.2 | 14.2 | 15.8 | 16.6 | | |
| 810370 | 10.9 | 12.2 | 14.0 | 14.9 | 16.6 | 17.4 | | |
| 810380 | 11.0 | 12.3 | 14.1 | 15.1 | 16.8 | 17.7 | | |

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Table 6.2
DESIGN STORM MODEL OUTPUT SUMMARY

| Model Node ID | | Existing C | onditions Design I | Flood Elevations | s (Feet, NGVD) | |
|---------------|-----------|------------|-----------------------|------------------|----------------|----------|
| | 2.33-year | 5-year | 10-year | 25-year | 50-year | 100-year |
| 817695 | 73.7 | 74.6 | 75.6 | 76.3 | 77.3 | 78.8 |
| 817700 | 73.8 | 74.7 | 75.7 | 76.4 | 77.4 | 79.0 |
| 817740 | 73.9 | 74.7 | 75.7 | 76.4 | 77.4 | 79.0 |
| 817750 | 74.1 | 75.1 | 76.3 | 77.2 | 78.5 | 79.7 |
| 817800 | 80.1 | 80.4 | 80.7 | 80.9 | 81.2 | 79.8 |
| • | 1 | Unnamed S | outhern Fork - Little | | 1 | |
| 818000 | 57.8 | 58.3 | 58.9 | 59.3 | 60.0 | 60.4 |
| 818010 | 67.6 | 68.1 | 68.8 | 69.2 | 70.0 | 70.4 |
| 818020 | 77.8 | 78.3 | 79.1 | 79.5 | 80.4 | 80.8 |
| 818100 | 78.6 | 79.8 | 82.4 | 83.8 | 84.6 | 84.8 |
| 818120 | 88.0 | 89.2 | 91.0 | 92.4 | 95.2 | 96.6 |
| 818150 | 90.1 | 90.2 | 91.0 | 92.4 | 95.2 | 96.7 |
| 818200 | 80.7 | 81.3 | 81.9 | 82.5 | 83.3 | 83.7 |
| 818250 | 81.6 | 82.0 | 82.6 | 83.5 | 85.5 | 87.2 |
| | 9 110 | | North Prong - Upper | | | <u></u> |
| 819000 | 48.0 | 49.4 | 51.2 | 52.3 | 55.0 | 55.1 |
| 819020 | 48.7 | 49.6 | 51.4 | 52.4 | 55.2 | 55.1 |
| 819050 | 52.7 | 54.2 | 55.0 | 55.4 | 55.9 | 56.2 |
| 819060 | 76.5 | 76.7 | 77.0 | 77.2 | 77.5 | 77.6 |
| 819080 | 78.2 | 78.5 | 78.9 | 79.1 | 79.5 | 79.7 |
| 819090 | 85.9 | 86.1 | 86.3 | 86.4 | 86.8 | 86.9 |
| 819095 | 86.5 | 87.3 | 88.7 | 90.0 | 90.5 | 90.6 |
| 819100 | 90.7 | 90.9 | 91.1 | 91.3 | 91.5 | 91.6 |
| 819200 | 89.3 | 89.5 | 89.7 | 89.9 | 90.1 | 90.1 |
| 017200 | 07.0 | 07.0 | Dug Creek - Coas | | 7011 | 70.1 |
| 821000 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 | 2.4 |
| 821100 | 2.2 | 2.3 | 2.2 | 2.1 | 2.3 | 2.7 |
| 821190 | 3.3 | 3.8 | 4.5 | 5.0 | 5.3 | 5.4 |
| 821200 | 3.3 | 3.9 | 4.7 | 5.3 | 5.8 | 5.9 |
| 821290 | 4.1 | 4.7 | 5.4 | 5.9 | 6.4 | 6.7 |
| 821300 | 4.4 | 5.1 | 6.1 | 6.8 | 7.8 | 8.4 |
| 821390 | 9.8 | 10.2 | 10.7 | 11.1 | 11.5 | 11.7 |
| 821400 | 10.3 | 10.5 | 10.9 | 11.2 | 12.0 | 12.7 |
| 821490 | 20.0 | 20.3 | 20.6 | 20.9 | 21.3 | 21.5 |
| 821500 | 22.5 | 22.9 | 23.9 | 25.1 | 26.3 | 26.4 |
| | - | | Kitchen Branch - Co | | | |
| 822000 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| 822050 | 2.1 | 2.3 | 2.8 | 3.3 | 4.5 | 4.7 |
| 822100 | 2.1 | 2.2 | 2.5 | 2.8 | 3.4 | 3.7 |
| 822110 | 2.4 | 2.6 | 2.9 | 3.3 | 3.8 | 4.1 |
| 822150 | 2.1 | 2.3 | 2.5 | 2.8 | 3.4 | 3.8 |
| 822190 | 2.1 | 2.3 | 2.5 | 2.8 | 3.4 | 3.8 |
| 822200 | 2.2 | 2.3 | 2.5 | 2.9 | 3.6 | 4.0 |
| 822250 | 2.5 | 2.7 | 3.1 | 3.6 | 4.3 | 4.6 |
| 822290 | 4.2 | 4.6 | 5.2 | 5.6 | 6.0 | 6.2 |
| 822300 | 4.2 | 4.8 | 5.6 | 6.2 | 7.1 | 7.7 |
| 822350 | 4.6 | 5.1 | 5.7 | 6.2 | 6.8 | 7.1 |

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TABLE 6.11-2 ALAFIA RIVER WATERSHED MANAGEMENT PLAN UPDATE ALAFIA RIVER MAIN STEM SUBWATERSHED EXISTING CONDITIONS FLOOD ELEVATIONS SUMMARY

| MODEL JUNCTION | LOCATION DESCRIPTION | | 24-HOU | R DURATIO I FLOOD EL 10-YEAR | EVATION, | ft NAVD 88 | 100-YEAR |
|-------------------|---|--------------|----------------|------------------------------------|----------------|----------------|----------------|
| Alafia River fro | n Hillsborough Bay to U.S. Highway 301 | | | | | | |
| 700000 | Hillsborough Bay | 1.09 | 1.09 | 1.09 | 1.09 | 1.09 | 1.09 |
| 700030 | | 1.14 | 1.17 | 1.23 | 1.35 | 1.48 | 1.61 |
| 700050 | U.S. Highway 41 Bridge (d/s); FEMA XS No 1 | 1.16 | 1.20 | 1.29 | 1.45 | 1.62 | 1.80 |
| 700060 | U.S. Highway 41 Bridge (u/s); FEMA XS No 2B | 1.16 | 1.21 | 1.30 | 1.46 | 1.64 | 1.82 |
| 700100 700150 | FEMA XS No 5 (A) | 1.17 1.19 | 1.22 | 1.32 | 1.50 | 1.69 1.82 | 1.89 2.05 |
| 700150 | FEMA XS No 6 FEMA XS No 7 (B) | 1.19 | 1.26 1.29 | 1.38 1.43 | 1.60 1.68 | 1.82 | 2.05 |
| 700280 | FEMA XS No 8 | 1.23 | 1.31 | 1.47 | 1.74 | 2.01 | 2.28 |
| 700350 | FEMA XS No 9 | 1.26 | 1.36 | 1.56 | 1.88 | 2.19 | 2.48 |
| 700400 | FEMA XS No 10 (C) | 1.36 | 1.52 | 1.80 | 2.25 | 2.66 | 3.04 |
| 700500 | FEMA XS No 11 | 1.43 | 1.62 | 1.95 | 2.47 | 2.93 | 3.35 |
| 700550 | FEMA XS No 12 | 1.46 | 1.66 | 2.02 | 2.56 | 3.04 | 3.48 |
| 700600 | FEMA XS No 13 (D) | 1.50 | 1.72 | 2.10 | 2.68 | 3.19 | 3.64 |
| 700700 | I-75 Bridge (d/s) | 1.51 | 1.74 | 2.13 | 2.72 | 3.23 | 3.69 |
| 700750 700900 | I-75 Bridge (u/s) FEMA XS No 14 | 1.57 1.68 | 1.83 1.99 | 2.26 2.49 | 2.91 3.22 | 3.46 3.84 | 3.96 4.39 |
| 701000 | FEMA XS No 15 (E) | 1.76 | 2.10 | 2.49 | 3.43 | 4.09 | 4.66 |
| 701020 | FEMA XS No 16 | 1.84 | 2.22 | 2.80 | 3.64 | 4.34 | 4.94 |
| 701100 | [S-20-T30-R20] | 1.91 | 2.32 | 2.94 | 3.82 | 4.54 | 5.16 |
| 701180 | FEMA XS No 17 | 1.98 | 2.41 | 3.06 | 3.98 | 4.74 | 5.38 |
| 701200 | FEMA XS No 18 | 2.04 | 2.49 | 3.17 | 4.12 | 4.90 | 5.56 |
| 701250 | U.S. Highway 301 Bridge (d/s); FEMA XS No 19 | 2.24 | 2.76 | 3.54 | 4.60 | 5.45 | 6.17 |
| Aletie Diver | m II C Himburgu 204 to Dieg Crast | | | | | | |
| 701350 | m U.S Highway 301 to Rice Creek U.S. Highway 301 Bridge (u/s); FEMA XS No 20B (F) | 2.30 | 2.84 | 3.65 | 4.75 | 5.62 | 6.36 |
| 701330 | FEMA XS No 21 | 2.34 | 2.04 | 3.74 | 4.75 | 5.76 | 6.51 |
| 701370 | FEMA XS No 22 | 2.36 | 2.93 | 3.76 | 4.89 | 5.78 | 6.54 |
| 701390 | FEMA XS No 23 | 2.40 | 2.98 | 3.82 | 4.96 | 5.86 | 6.62 |
| 701400 | [S17-T30-R20] | 2.44 | 3.03 | 3.88 | 5.04 | 5.95 | 6.71 |
| 701500 | FEMA XS No 24 (G) | 2.68 | 3.36 | 4.33 | 5.61 | 6.60 | 7.41 |
| 701600 | Rice Creek | 2.80 | 3.51 | 4.53 | 5.87 | 6.90 | 7.74 |
| Alofia Divor fro | m Rice Creek to Buckhorn Creek | | | | | | |
| 701700 | FEMA XS No 25 | 2.83 | 3.56 | 4.59 | 5.94 | 6.98 | 7.83 |
| 701800 | FEMA XS No 26 (H) | 3.05 | 3.85 | 4.95 | 6.39 | 7.49 | 8.39 |
| 701900 | | 3.25 | 4.11 | 5.26 | 6.75 | 7.88 | 8.81 |
| 701950 | FEMA XS No 27 | 3.32 | 4.19 | 5.37 | 6.88 | 8.02 | 8.95 |
| 702000 | | 3.46 | 4.38 | 5.59 | 7.14 | 8.32 | 9.27 |
| 702100 | FEMA XS No 28 | 3.71 | 4.70 | 5.95 | 7.54 | 8.73 | 9.71 |
| 702200 | FEMA XS No 29 (I) | 3.81 | 4.82 | 6.08 | 7.71 | 8.94 | 9.95 |
| 702205 702250 | FEMA XS No 30 | 4.02 4.19 | 5.07 5.27 | 6.34 6.54 | 7.96 8.17 | 9.19 9.40 | 10.19 10.41 |
| 702400 | Buckhorn Creek; FEMA XS No 31 (J) | 4.19 | 5.99 | 7.37 | 9.11 | 10.40 | 11.44 |
| 702400 | DUCKHOIT CICCK, I ENITE NO OT (0) | 4.11 | 0.00 | 7.07 | 5.11 | 10.40 | 11.77 |
| Alafia River fro | m Buckhorn Creek to Bell Creek | | | | | | |
| 702450 | FEMA XS No 32 | 5.23 | 6.59 | 8.07 | 9.91 | 11.28 | 12.39 |
| 702500 | FEMA XS No 33 (K) | 5.27 | 6.69 | 8.22 | 10.07 | 11.45 | 12.57 |
| 702600 | | 5.34 | 6.77 | 8.29 | 10.16 | 11.54 | 12.66 |
| 702650 | FEMA XS No 34 | 5.41 | 6.88 | 8.47 | 10.36 | 11.73 | 12.83 |
| 702700 | FEMA XS No 35 (L) | 5.49 | 6.98 | 8.60 | 10.58 | 12.02 | 13.18 |
| 702800 702880 | FEMA XS No 36 | 5.65 5.71 | 7.20 7.28 | 8.85 8.92 | 10.83 10.92 | 12.33 12.44 | 13.53 13.64 |
| 702900 | I LIVE ACTION OF | 5.97 | 7.57 | 9.23 | 11.22 | 12.44 | 13.89 |
| 702950 | FEMA XS No 37 | 6.43 | 8.15 | 9.77 | 11.71 | 13.17 | 14.34 |
| 703000 | | 6.60 | 8.33 | 9.95 | 11.89 | 13.34 | 14.50 |
| 703050 | FEMA XS No 38 | 6.81 | 8.60 | 10.24 | 12.19 | 13.64 | 14.79 |
| 703100 | FEMA XS No 39 (M) | 7.26 | 9.21 | 10.97 | 13.02 | 14.53 | 15.73 |
| 703200 | | 7.33 | 9.32 | 11.13 | 13.23 | 14.78 | 16.01 |
| 703300 | FEMA XS No 40 (N) | 7.34 | 9.35 | 11.19 | 13.33 | 14.91 | 16.15 |
| 703400 | FEMA XS No 41 (O) | 7.62 | 9.77 | 11.68 | 13.83 | 15.40 | 16.64 |
| 703500 703550 | FEMA XS No 42 FEMA XS No 43 | 8.17 8.28 | 10.19 10.30 | 12.06 12.15 | 14.16 14.26 | 15.70 15.79 | 16.92 17.01 |
| 703550 | FEMA XS No 44 (P) | 9.20 | 11.04 | 12.15 | 14.26 | 16.35 | 17.01 |
| 703700 | Bell Creek | 9.44 | 11.30 | 13.06 | 15.09 | 16.54 | 17.70 |
| . 557.55 | | 0.11 | | | | | |
| Alafia River fro | m Bell Creek to Bell Shoals Road Bridge | | | | | | |
| 703790 | FEMA XS No 45 | 9.59 | 11.44 | 13.19 | 15.21 | 16.66 | 17.82 |
| 703800 | FEMA XS No 46 | 9.62 | 11.47 | 13.23 | 15.26 | 16.72 | 17.89 |
| 703850 | FEMA XS No 47 | 9.92 | 11.84 | 13.62 | 15.63 | 17.08 | 18.24 |
| 703900 | FEMA XS No 48 | 10.50 | 12.52 | 14.42 | 16.58 | 18.16 | 19.34 |

Table 6-4 Comparison of Peak WSEL for the 100-Year, 1-Day and 100-Year, 5-Day Events

| Model Junction ID | Subwatershed | 100-Year, 1-Day Peak WSEL (ft NAVD) | 100-Year, 1-Day Time to Peak (Hr) | 100-Year, 5-Day Peak WSEL (ft NAVD) | 100-Year, 5-Day Time to Peak (Hr) | Z5D - Z1D (ft) |
|-------------------|-----------------|---|---|---|---|-------------------|
| 200000 | Delaney Pop-off | 6.86 | 14.40 | 6.80 | 62.90 | (0.06) |
| 200010 | Delaney Pop-off | 6.77 | 14.30 | 6.72 | 62.90 | (0.05) |
| 200020 | Delaney Pop-off | 7.60 | 24.80 | 7.82 | 64.40 | 0.22 |
| 200025 | Delaney Pop-off | 7.60 | 24.80 | 7.83 | 64.40 | 0.23 |
| 200040 | Delaney Pop-off | 11.52 | 25.40 | 11.67 | 62.30 | 0.15 |
| 200050 | Delaney Pop-off | 3.29 | 13.40 | 3.41 | 62.90 | 0.12 |
| 200051 | Delaney Pop-off | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 200060 | Delaney Pop-off | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 200065 | Delaney Pop-off | 3.39 | 19.80 | 3.50 | 68.20 | 0.11 |
| 200070 | Delaney Pop-off | 5.49 | 19.80 | 5.86 | 68.30 | 0.37 |
| 200080 | Delaney Pop-off | 5.53 | 19.60 | 5.90 | 68.30 | 0.37 |
| 200090 | Delaney Pop-off | 5.98 | 19.50 | 6.41 | 68.30 | 0.43 |
| 200091 | Delaney Pop-off | 6.09 | 19.50 | 6.50 | 68.20 | 0.41 |
| 200092 | Delaney Pop-off | 6.09 | 19.50 | 6.50 | 68.20 | 0.41 |
| 200093 | Delaney Pop-off | 6.09 | 19.70 | 6.50 | 69.00 | 0.41 |
| 200094 | Delaney Pop-off | 6.09 | 19.70 | 6.50 | 68.90 | 0.41 |
| 200095 | Delaney Pop-off | 7.53 | 17.50 | 8.01 | 66.90 | 0.48 |
| 200096 | Delaney Pop-off | 7.61 | 17.50 | 8.09 | 66.80 | 0.48 |
| 200100 | Delaney Pop-off | 6.10 | 20.10 | 6.51 | 69.20 | 0.41 |
| 200105 | Delaney Pop-off | 9.40 | 13.90 | 9.40 | 61.90 | 0.00 |
| 200110 | Delaney Pop-off | 7.70 | 18.00 | 8.20 | 67.40 | 0.50 |
| 200111 | Delaney Pop-off | 7.73 | 18.30 | 8.22 | 67.60 | 0.49 |
| 200120 | Delaney Pop-off | 7.82 | 18.60 | 8.31 | 67.90 | 0.49 |
| 200121 | Delaney Pop-off | 7.86 | 18.50 | 8.34 | 67.90 | 0.48 |
| 200130 | Delaney Pop-off | 8.30 | 13.90 | 8.57 | 67.50 | 0.27 |
| 200140 | Delaney Pop-off | 8.91 | 14.30 | 9.05 | 64.20 | 0.14 |
| 200145 | Delaney Pop-off | 11.12 | 15.00 | 11.07 | 63.80 | (0.05) |
| 200150 | Delaney Pop-off | 12.98 | 16.00 | 13.02 | 64.80 | 0.04 |
| 200260 | Delaney Pop-off | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 200261 | Delaney Pop-off | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 200262 | Delaney Pop-off | 2.03 | 13.10 | 1.81 | 61.30 | (0.22) |
| 200270 | Delaney Pop-off | 2.38 | 13.30 | 2.23 | 62.00 | (0.15) |
| 200280 | Delaney Pop-off | 2.80 | 13.40 | 2.68 | 62.20 | (0.12) |
| 200281 | Delaney Pop-off | 2.94 | 13.50 | 2.83 | 62.30 | (0.11) |
| 200282 | Delaney Pop-off | 2.94 | 13.50 | 2.84 | 62.20 | (0.10) |
| 200283 | Delaney Pop-off | 2.97 | 13.50 | 2.86 | 62.30 | (0.11) |
| 200284 | Delaney Pop-off | 2.97 | 13.50 | 2.86 | 62.30 | (0.11) |
| 200285 | Delaney Pop-off | 5.17 | 13.60 | 4.79 | 62.30 | (0.38) |

Table 6-4 Comparison of Peak WSEL for the 100-Year, 1-Day and 100-Year, 5-Day Events

| Model Junction ID | Subwatershed | 100-Year, 1-Day Peak WSEL (ft NAVD) | 100-Year, 1-Day Time to Peak (Hr) | 100-Year, 5-Day Peak WSEL (ft NAVD) | 100-Year, 5-Day Time to Peak (Hr) | Z5D - Z1D (ft) |
|-------------------|-----------------|---|---|---|---|-------------------|
| 200286 | Delaney Pop-off | 3.01 | 13.50 | 2.90 | 62.20 | (0.11) |
| 200290 | Delaney Pop-off | 3.10 | 13.50 | 2.99 | 62.20 | (0.11) |
| 200300 | Delaney Pop-off | 5.82 | 13.60 | 5.35 | 62.20 | (0.47) |
| 200301 | Delaney Pop-off | 6.13 | 13.50 | 5.61 | 62.10 | (0.52) |
| 200302 | Delaney Pop-off | 6.23 | 13.40 | 5.71 | 62.10 | (0.52) |
| 200303 | Delaney Pop-off | 7.43 | 26.60 | 7.73 | 72.00 | 0.30 |
| 200305 | Delaney Pop-off | 7.43 | 12.80 | 7.14 | 61.10 | (0.29) |
| 200306 | Delaney Pop-off | 3.01 | 13.40 | 2.85 | 62.20 | (0.16) |
| 200307 | Delaney Pop-off | 3.04 | 13.50 | 2.87 | 62.10 | (0.17) |
| 200308 | Delaney Pop-off | 3.06 | 13.50 | 2.89 | 62.10 | (0.17) |
| 200310 | Delaney Pop-off | 7.47 | 26.60 | 7.81 | 72.00 | 0.34 |
| 200311 | Delaney Pop-off | 7.47 | 26.60 | 7.81 | 72.00 | 0.34 |
| 200312 | Delaney Pop-off | 7.53 | 26.10 | 7.87 | 72.00 | 0.34 |
| 200313 | Delaney Pop-off | 7.54 | 26.10 | 7.87 | 71.90 | 0.33 |
| 200315 | Delaney Pop-off | 7.47 | 26.70 | 7.80 | 72.00 | 0.33 |
| 200319 | Delaney Pop-off | 7.46 | 27.30 | 7.80 | 72.00 | 0.34 |
| 200320 | Delaney Pop-off | 6.96 | 64.00 | 7.04 | 72.00 | 0.08 |
| 200330 | Delaney Pop-off | 8.86 | 15.90 | 9.09 | 65.10 | 0.23 |
| 200335 | Delaney Pop-off | 8.94 | 15.30 | 9.15 | 64.60 | 0.21 |
| 200340 | Delaney Pop-off | 4.30 | 13.40 | 3.77 | 61.50 | (0.53) |
| 200345 | Delaney Pop-off | 5.45 | 15.30 | 5.44 | 64.30 | (0.01) |
| 200346 | Delaney Pop-off | 5.47 | 16.00 | 5.51 | 64.80 | 0.04 |
| 200347 | Delaney Pop-off | 5.49 | 16.10 | 5.52 | 64.90 | 0.03 |
| 200350 | Delaney Pop-off | 5.52 | 15.10 | 5.50 | 64.30 | (0.02) |
| 210000 | Delaney Creek | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 210005 | Delaney Creek | 5.24 | 18.60 | 5.65 | 67.10 | 0.41 |
| 210010 | Delaney Creek | 5.49 | 18.50 | 5.89 | 67.10 | 0.40 |
| 210015 | Delaney Creek | 5.50 | 18.50 | 5.89 | 67.10 | 0.39 |
| 210020 | Delaney Creek | 5.61 | 18.30 | 6.01 | 66.90 | 0.40 |
| 210021 | Delaney Creek | 5.62 | 18.60 | 6.01 | 67.10 | 0.39 |
| 210022 | Delaney Creek | 5.61 | 19.20 | 6.01 | 67.10 | 0.40 |
| 210025 | Delaney Creek | 5.51 | 18.60 | 5.90 | 67.20 | 0.39 |
| 210030 | Delaney Creek | 5.97 | 17.20 | 6.32 | 66.10 | 0.35 |
| 210040 | Delaney Creek | 7.74 | 16.10 | 7.95 | 65.10 | 0.21 |
| 210045 | Delaney Creek | 7.76 | 16.60 | 7.98 | 65.50 | 0.22 |
| 210050 | Delaney Creek | 8.28 | 15.80 | 8.47 | 64.70 | 0.19 |
| 210055 | Delaney Creek | 7.77 | 16.70 | 7.99 | 65.60 | 0.22 |
| 210060 | Delaney Creek | 10.25 | 15.60 | 10.39 | 64.40 | 0.14 |

Table 6-4 Comparison of Peak WSEL for the 100-Year, 1-Day and 100-Year, 5-Day Events

| Model Junction ID | Subwatershed | 100-Year, 1-Day Peak WSEL (ft NAVD) | 100-Year, 1-Day Time to Peak (Hr) | 100-Year, 5-Day Peak WSEL (ft NAVD) | 100-Year, 5-Day Time to Peak (Hr) | Z5D - Z1D (ft) |
|-------------------|-----------------|---|---|---|---|-------------------|
| 230160 | Delaney Creek | 33.26 | 45.30 | 35.89 | 72.00 | 2.63 |
| 230170 | Delaney Creek | 33.94 | 32.30 | 35.92 | 72.00 | 1.98 |
| 230175 | Delaney Creek | 35.67 | 23.30 | 37.04 | 63.60 | 1.37 |
| 230177 | Delaney Creek | 40.13 | 13.00 | 39.87 | 61.20 | (0.26) |
| 230178 | Delaney Creek | 37.87 | 14.30 | 38.18 | 63.80 | 0.31 |
| 230179 | Delaney Creek | 41.41 | 12.70 | 41.17 | 61.00 | (0.24) |
| 230180 | Delaney Creek | 35.69 | 23.20 | 37.20 | 63.50 | 1.51 |
| 230185 | Delaney Creek | 35.66 | 25.20 | 36.39 | 67.60 | 0.73 |
| 230186 | Delaney Creek | 35.70 | 23.20 | 37.25 | 63.40 | 1.55 |
| 230190 | Delaney Creek | 39.26 | 15.10 | 39.81 | 61.30 | 0.55 |
| 230195 | Delaney Creek | 45.97 | 13.50 | 46.00 | 61.60 | 0.03 |
| 230196 | Delaney Creek | 46.26 | 12.90 | 46.17 | 61.20 | (0.09) |
| 230197 | Delaney Creek | 52.89 | 13.10 | 52.59 | 61.30 | (0.30) |
| 230200 | Delaney Creek | 49.85 | 25.80 | 50.80 | 65.30 | 0.95 |
| 231000 | Delaney Creek | 33.52 | 13.80 | 33.55 | 62.80 | 0.03 |
| 231001 | Delaney Creek | 33.55 | 13.80 | 33.57 | 62.80 | 0.02 |
| 233000 | Delaney Creek | 43.73 | 24.80 | 44.15 | 63.80 | 0.42 |
| 233010 | Delaney Creek | 38.69 | 25.60 | 42.36 | 72.00 | 3.67 |
| 233015 | Delaney Creek | 38.69 | 25.60 | 42.36 | 72.00 | 3.67 |
| 234000 | Delaney Creek | 37.71 | 15.50 | 38.40 | 62.70 | 0.69 |
| 240000 | Delaney Pop-off | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 240010 | Delaney Pop-off | 3.90 | 13.60 | 3.94 | 62.30 | 0.04 |
| 240020 | Delaney Pop-off | 4.25 | 14.00 | 4.45 | 63.50 | 0.20 |
| 240030 | Delaney Pop-off | 4.47 | 16.40 | 4.70 | 64.30 | 0.23 |
| 240040 | Delaney Pop-off | 4.90 | 16.50 | 5.22 | 64.50 | 0.32 |
| 240050 | Delaney Pop-off | 5.58 | 16.40 | 5.87 | 64.60 | 0.29 |
| 240060 | Delaney Pop-off | 6.72 | 16.40 | 7.08 | 64.70 | 0.36 |
| 240070 | Delaney Pop-off | 7.09 | 16.40 | 7.49 | 64.70 | 0.40 |
| 240080 | Delaney Pop-off | 7.16 | 16.30 | 7.55 | 64.70 | 0.39 |
| 240085 | Delaney Pop-off | 6.19 | 26.30 | 7.12 | 70.70 | 0.93 |
| 240090 | Delaney Pop-off | 7.40 | 16.10 | 7.78 | 64.50 | 0.38 |
| 240100 | Delaney Pop-off | 7.71 | 15.80 | 8.10 | 64.30 | 0.39 |
| 240110 | Delaney Pop-off | 9.01 | 14.40 | 9.34 | 63.30 | 0.33 |
| 240115 | Delaney Pop-off | 9.40 | 14.20 | 9.68 | 63.10 | 0.28 |
| 240120 | Delaney Pop-off | 10.02 | 14.00 | 10.27 | 62.70 | 0.25 |
| 240130 | Delaney Pop-off | 10.42 | 14.00 | 10.65 | 62.70 | 0.23 |
| 240135 | Delaney Pop-off | 10.51 | 14.00 | 10.71 | 62.60 | 0.20 |
| 240140 | Delaney Pop-off | 10.64 | 14.10 | 10.89 | 62.80 | 0.25 |

Table 6-4 Comparison of Peak WSEL for the 100-Year, 1-Day and 100-Year, 5-Day Events

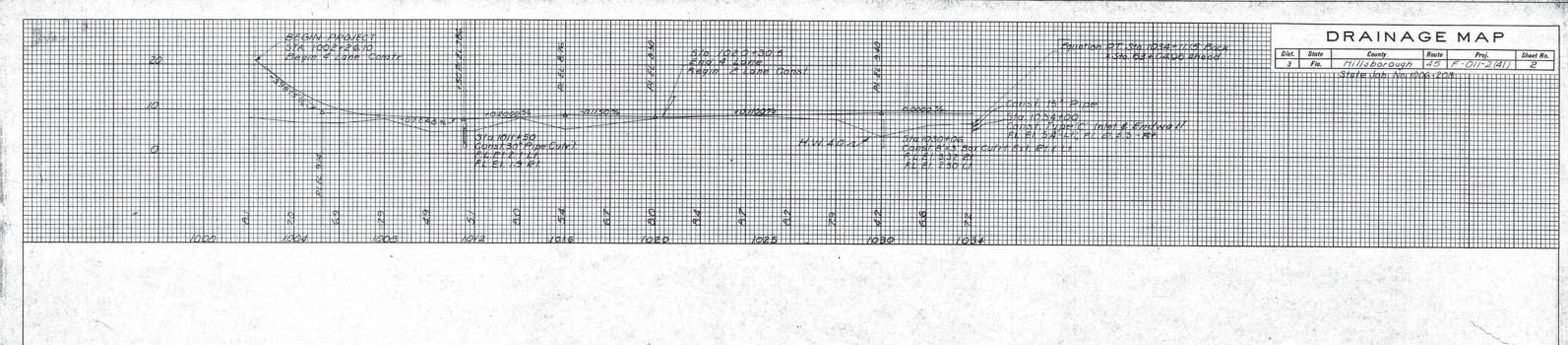
| Model Junction ID | Subwatershed | 100-Year, 1-Day Peak WSEL (ft NAVD) | 100-Year, 1-Day Time to Peak (Hr) | 100-Year, 5-Day Peak WSEL (ft NAVD) | 100-Year, 5-Day Time to Peak (Hr) | Z5D - Z1D (ft) |
|-------------------|--------------------|---|---|---|---|-------------------|
| 252000 | Delaney Pop-off | 28.93 | 18.10 | 29.27 | 67.60 | 0.34 |
| 252020 | Delaney Pop-off | 28.93 | 18.40 | 29.26 | 67.80 | 0.33 |
| 252025 | Delaney Pop-off | 29.20 | 12.90 | 29.27 | 67.90 | 0.07 |
| 252030 | Delaney Pop-off | 28.93 | 18.60 | 29.24 | 67.40 | 0.31 |
| 252040 | Delaney Pop-off | 29.01 | 15.00 | 29.24 | 67.30 | 0.23 |
| 252050 | Delaney Pop-off | 29.10 | 14.40 | 29.24 | 67.40 | 0.14 |
| 252051 | Delaney Pop-off | 28.61 | 25.40 | 29.15 | 72.00 | 0.54 |
| 252052 | Delaney Pop-off | 28.61 | 34.40 | 29.15 | 72.00 | 0.54 |
| 252053 | Delaney Pop-off | 28.61 | 32.90 | 29.15 | 72.00 | 0.54 |
| 252054 | Delaney Pop-off | 28.74 | 13.90 | 29.15 | 72.00 | 0.41 |
| 252055 | Delaney Pop-off | 29.74 | 25.10 | 30.26 | 72.00 | 0.52 |
| 252060 | Delaney Pop-off | 29.39 | 14.00 | 29.31 | 62.80 | (0.08) |
| 252065 | Delaney Pop-off | 29.96 | 12.80 | 30.26 | 72.00 | 0.30 |
| 252500 | Delaney Pop-off | 29.01 | 15.00 | 29.24 | 67.50 | 0.23 |
| 252505 | Delaney Pop-off | 69.10 | 14.00 | 60.00 | 63.20 | (9.10) |
| 252510 | Delaney Pop-off | 29.01 | 15.00 | 29.24 | 67.80 | 0.23 |
| 253000 | Delaney Pop-off | 28.89 | 19.70 | 29.27 | 67.80 | 0.38 |
| 253005 | Delaney Pop-off | 29.49 | 12.90 | 29.27 | 67.30 | (0.22) |
| 253010 | Delaney Pop-off | 28.88 | 19.70 | 29.26 | 67.40 | 0.38 |
| 253015 | Delaney Pop-off | 31.79 | 12.80 | 30.13 | 63.30 | (1.66) |
| 253020 | Delaney Pop-off | 28.88 | 19.50 | 29.26 | 67.40 | 0.38 |
| 253025 | Delaney Pop-off | 32.65 | 12.70 | 31.09 | 61.20 | (1.56) |
| 254000 | Delaney Pop-off | 29.51 | 17.40 | 29.98 | 65.80 | 0.47 |
| 254010 | Delaney Pop-off | 29.55 | 18.20 | 30.00 | 66.40 | 0.45 |
| 254020 | Delaney Pop-off | 29.55 | 18.10 | 30.00 | 66.40 | 0.45 |
| 254030 | Delaney Pop-off | 29.99 | 12.60 | 30.01 | 66.40 | 0.02 |
| 254040 | Delaney Pop-off | 30.77 | 12.50 | 30.01 | 66.20 | (0.76) |
| 254050 | Delaney Pop-off | 31.20 | 12.50 | 30.67 | 60.80 | (0.53) |
| 260000 | North Archie Creek | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 260010 | North Archie Creek | 3.54 | 28.40 | 3.76 | 72.00 | 0.22 |
| 260020 | North Archie Creek | 3.83 | 28.40 | 4.08 | 72.00 | 0.25 |
| 260030 | North Archie Creek | 4.09 | 28.30 | 4.35 | 72.00 | 0.26 |
| 260040 | North Archie Creek | 4.45 | 27.70 | 4.83 | 72.00 | 0.38 |
| 260050 | North Archie Creek | 4.96 | 27.20 | 5.35 | 72.00 | 0.39 |
| 260060 | North Archie Creek | 5.92 | 26.60 | 6.75 | 72.00 | 0.83 |
| 260065 | North Archie Creek | 6.01 | 26.40 | 6.81 | 72.00 | 0.80 |
| 260070 | North Archie Creek | 6.56 | 27.00 | 7.31 | 72.00 | 0.75 |
| 260080 | North Archie Creek | 7.09 | 27.10 | 7.65 | 72.00 | 0.56 |

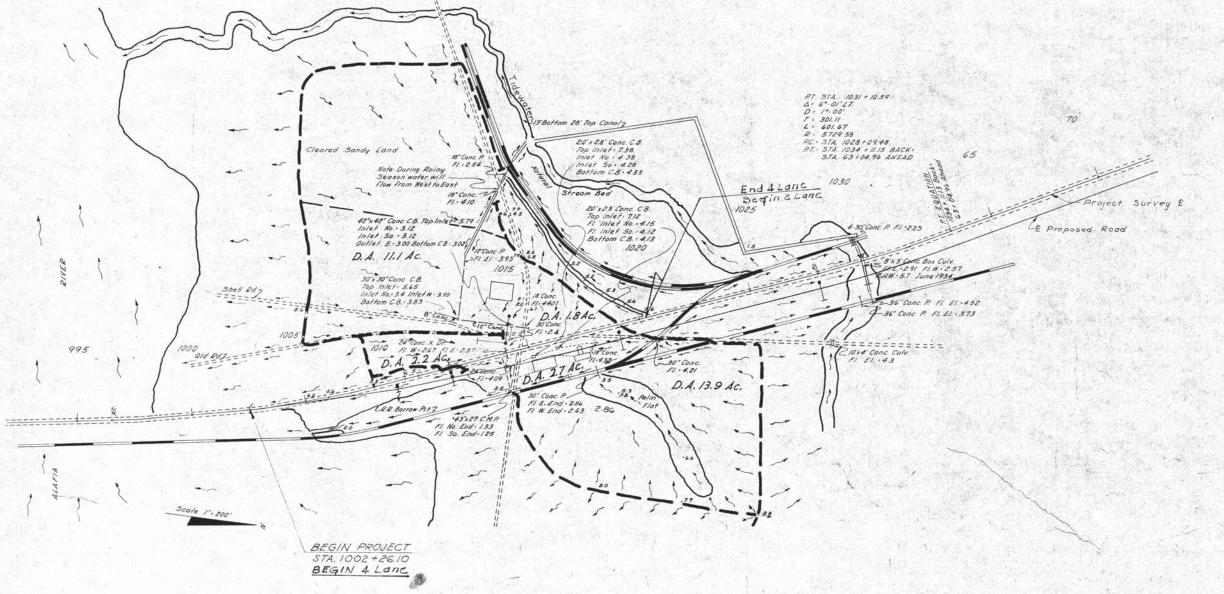
Table 6-4 Comparison of Peak WSEL for the 100-Year, 1-Day and 100-Year, 5-Day Events

| Model Junction ID | Subwatershed | 100-Year, 1-Day Peak WSEL (ft NAVD) | 100-Year, 1-Day Time to Peak (Hr) | 100-Year, 5-Day Peak WSEL (ft NAVD) | 100-Year, 5-Day Time to Peak (Hr) | Z5D - Z1D (ft) |
|-------------------|--------------|---|---|---|---|-------------------|
| 280003 | Archie Creek | 1.93 | 13.70 | 1.84 | 62.40 | (0.09) |
| 280004 | Archie Creek | 3.98 | 13.00 | 3.10 | 61.40 | (0.88) |
| 280005 | Archie Creek | 1.77 | 24.80 | 1.84 | 70.30 | 0.07 |
| 280006 | Archie Creek | 1.60 | 0.00 | 1.60 | 0.00 | 0.00 |
| 280007 | Archie Creek | 2.89 | 21.30 | 3.05 | 69.80 | 0.16 |
| 280008 | Archie Creek | 3.23 | 21.30 | 3.40 | 69.80 | 0.17 |
| 280009 | Archie Creek | 8.60 | 25.00 | 9.96 | 72.00 | 1.36 |
| 280010 | Archie Creek | 3.55 | 21.30 | 3.72 | 69.80 | 0.17 |
| 280012 | Archie Creek | 170.64 | 25.00 | 171.29 | 72.00 | 0.65 |
| 280015 | Archie Creek | 3.86 | 21.30 | 4.07 | 69.80 | 0.21 |
| 280020 | Archie Creek | 4.16 | 21.30 | 4.37 | 69.80 | 0.21 |
| 280030 | Archie Creek | 4.46 | 21.30 | 4.72 | 69.80 | 0.26 |
| 280035 | Archie Creek | 6.56 | 20.70 | 7.15 | 69.30 | 0.59 |
| 280040 | Archie Creek | 6.56 | 20.70 | 7.14 | 69.30 | 0.58 |
| 280041 | Archie Creek | 7.19 | 20.00 | 7.82 | 68.80 | 0.63 |
| 280042 | Archie Creek | 7.66 | 19.70 | 8.54 | 68.40 | 0.88 |
| 280043 | Archie Creek | 7.72 | 19.60 | 8.59 | 68.40 | 0.87 |
| 280044 | Archie Creek | 8.05 | 19.40 | 8.91 | 68.20 | 0.86 |
| 280047 | Archie Creek | 8.21 | 19.20 | 9.03 | 68.00 | 0.82 |
| 280050 | Archie Creek | 6.54 | 20.70 | 7.11 | 69.70 | 0.57 |
| 280055 | Archie Creek | 6.54 | 20.80 | 7.11 | 69.90 | 0.57 |
| 280060 | Archie Creek | 6.54 | 20.80 | 7.11 | 69.80 | 0.57 |
| 280066 | Archie Creek | 11.00 | 25.00 | 11.40 | 72.00 | 0.40 |
| 280067 | Archie Creek | 11.00 | 25.00 | 11.39 | 72.00 | 0.39 |
| 280068 | Archie Creek | 11.00 | 25.00 | 11.39 | 72.00 | 0.39 |
| 280069 | Archie Creek | 11.02 | 25.00 | 11.42 | 72.00 | 0.40 |
| 280070 | Archie Creek | 10.98 | 25.00 | 11.36 | 72.00 | 0.38 |
| 280071 | Archie Creek | 10.98 | 25.00 | 11.36 | 72.00 | 0.38 |
| 280072 | Archie Creek | 11.29 | 25.00 | 11.81 | 72.00 | 0.52 |
| 280080 | Archie Creek | 9.94 | 13.10 | 9.35 | 62.00 | (0.59) |
| 280081 | Archie Creek | 111.07 | 25.00 | 111.52 | 72.00 | 0.45 |
| 280085 | Archie Creek | 8.30 | 18.90 | 9.08 | 67.90 | 0.78 |
| 280086 | Archie Creek | 8.86 | 17.60 | 9.61 | 67.10 | 0.75 |
| 280088 | Archie Creek | 10.05 | 18.50 | 10.87 | 66.90 | 0.82 |
| 280089 | Archie Creek | 10.99 | 18.80 | 11.74 | 66.70 | 0.75 |
| 280100 | Archie Creek | 8.74 | 12.60 | 9.09 | 68.00 | 0.35 |
| 280104 | Archie Creek | 8.86 | 17.60 | 9.61 | 67.10 | 0.75 |
| 280105 | Archie Creek | 8.87 | 17.60 | 9.62 | 67.10 | 0.75 |

APPENDIX D

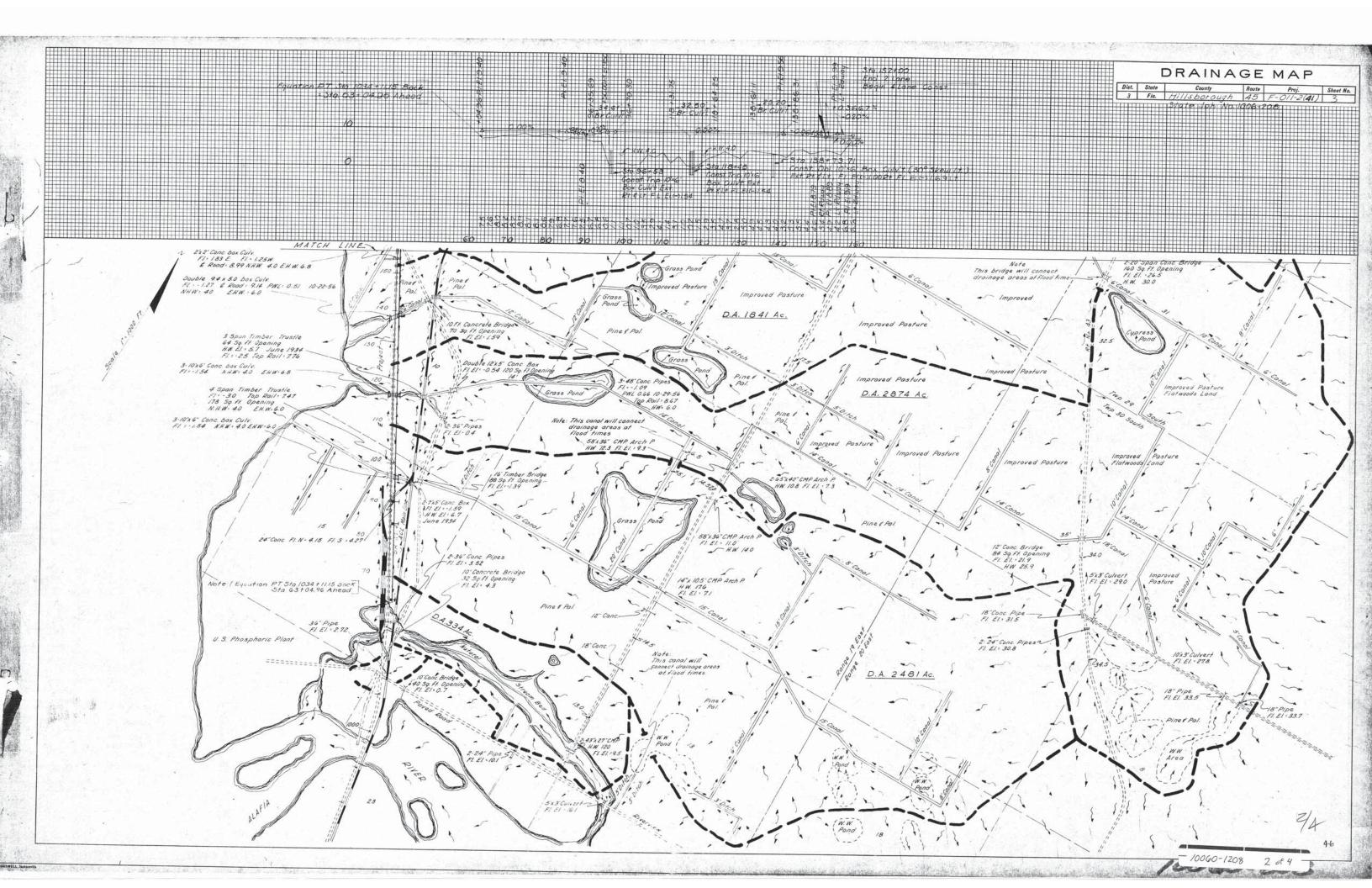
Historical District 7 Drainage Maps

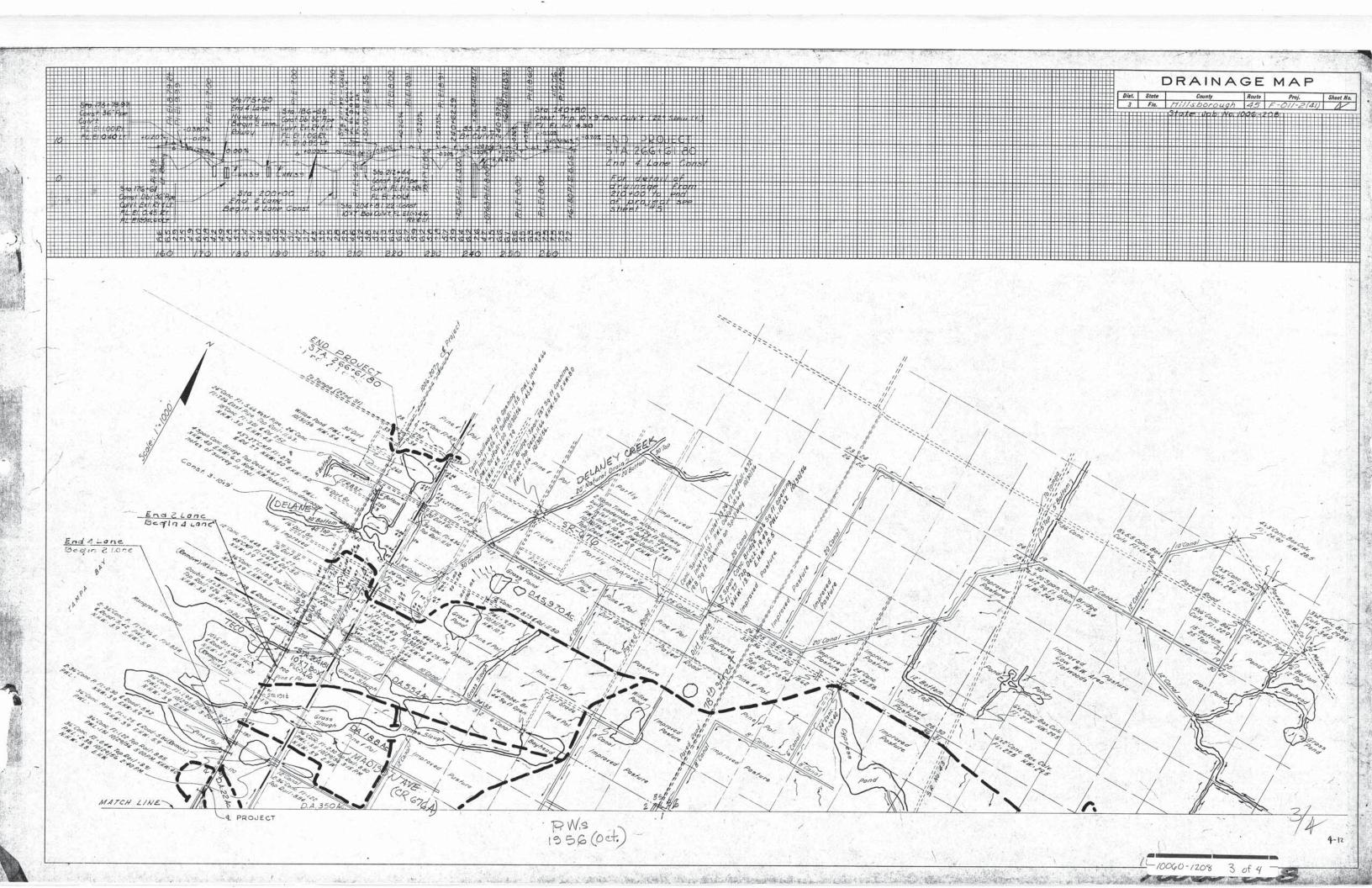


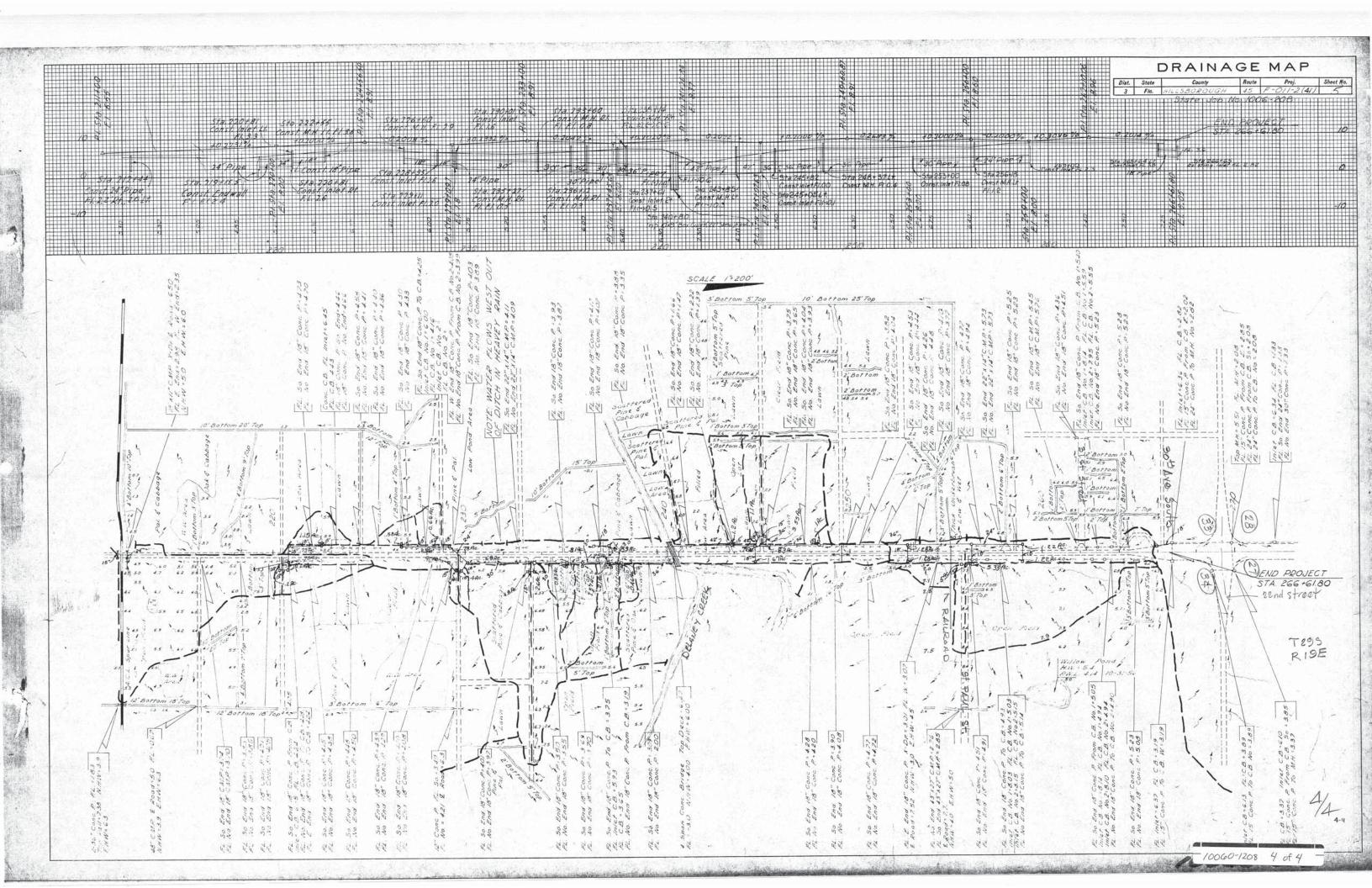


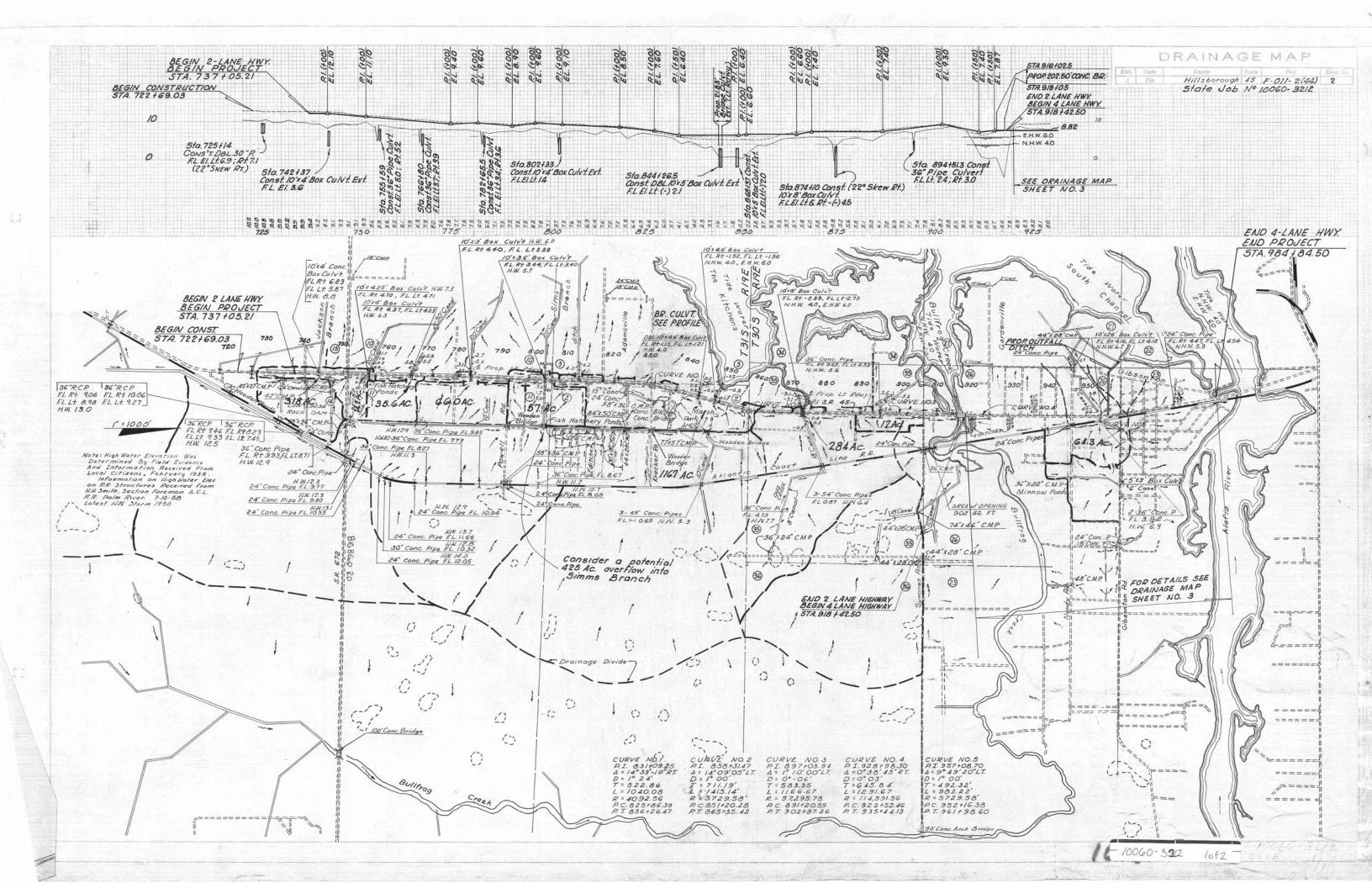
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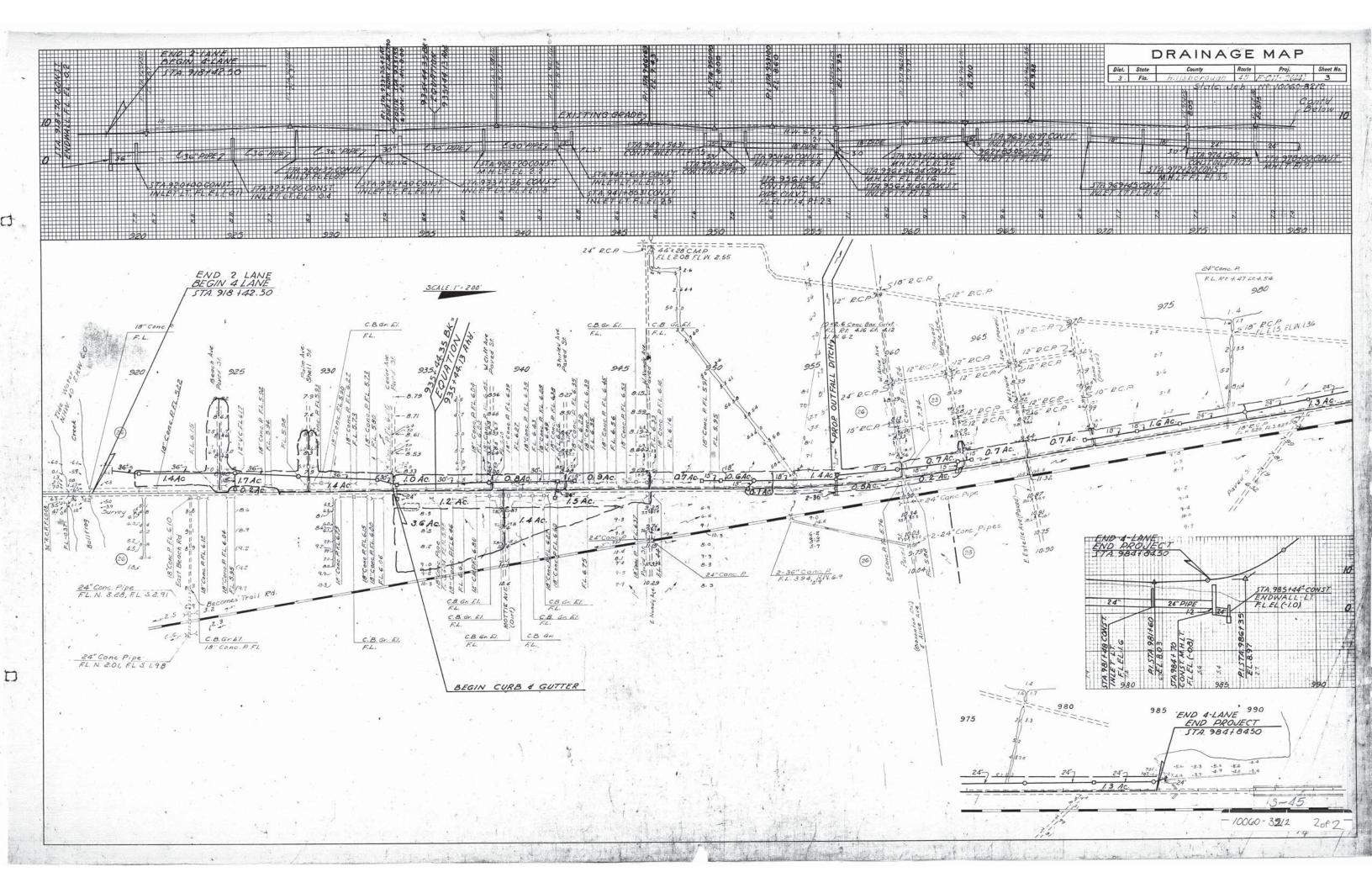
10060-1208 1094











APPENDIX E

Agency Coordination

THIS FORM IS INTENDED TO FACILITATE AND GUIDE THE DIALOGUE DURING A PRE-APPLICATION MEETING BY PROVIDING A PARTIAL "PROMPT LIST" OF DISCUSSION SUBJECTS. IT IS NOT A LIST OF REQUIREMENTS FOR SUBMITTAL BY THE APPLICANT.



SOUTHWEST FLORIDA WATER MANAGEMENT DISTRICT RESOURCE REGULATION DIVISION PRE-APPLICATION MEETING NOTES

FILE NUMBER:

PA 400801

Date: 1/22/2014 **Time:** 11:00

Project Name: FDOT US 41 PD&E Study from south of Causeway to Kracker Ave.

Attendees: Richard Alt; Chaz LaRiche; Andrew Goldsmith, American Consulting, agoldsmith@acp-

fl.com; Michael Ryan, American Consulting, Christopher Salicco, American Consulting

County:HillsboroughSec/Twp/Rge:MultipleTotal Land Acreage:159Project Acreage:159 acres

Prior On-Site/Off-Site Permit Activity:

ERP – Researching

Project Overview:

- Widen from 4 lane to 6 lane
- Wetlands/Surface Waters Yes
- FDOT ETDM 5180

Environmental Discussion: (Wetlands On-Site, Wetlands on Adjacent Properties, Delineation, T&E species, Easements, Drawdown Issues, Setbacks, Justification, Elimination/Reduction, Permanent/Temporary Impacts, Secondary and Cumulative Impacts, Mitigation Options, SHWL, Upland Habitats, Site Visit, etc.)

- Review the ETDM report for specific issues associated with the potential wetland/surface water issues
- Replacement of bridges over the rivers and creeks
- Provide the limits of jurisdictional wetlands.
- Provide appropriate mitigation using UMAM for impacts, if applicable.
- Demonstrate elimination and reduction of wetland impacts.
- Maintain minimum 15 foot, average 25 foot wetland conservation area setback or address secondary impacts.

Site Information Discussion: (SHW Levels, Floodplain, Tailwater Conditions, Adjacent Off-Site Contributing Sources, Receiving Waterbody, etc.)

- Existing roadway/intersections.
- Eleven WBID's 8 are impaired for nutrients
- Discharging to impaired waters.
- Need coordination with DEP on adjacent contaminated sites.

Water Quantity Discussions: (Basin Description, Storm Event, Pre/Post Volume, Pre/Post Discharge, etc.)

- Demonstrate that discharges from proposed project area will not cause an adverse impact for a 25-year, 24-hour storm event if the pond does not discharge to an infinite basin. Or demonstrate no adverse impacts if attenuation is not provided.
- Demonstrate that site will not impede the conveyance of contributing off-site flows.
- Demonstrate that the project will not increase riverine flood stages up- or down-stream of the project area(s).
- Provide equivalent compensating storage for all 100-year, 24-hour riverine floodplain impacts if applicable.

Water Quality Discussions: (Type of Treatment, Technical Characteristics, Non-presumptive Alternatives, etc.)

- Provide water quality treatment for the required project area.
- In addition, if the project discharges to an impaired water body, must provide a net environmental improvement.
- Applicant must demonstrate a net improvement for the parameters of concern by performing a pre/post pollutant loading analysis based on existing land use and the proposed land use.
- Will acknowledge compensatory treatment to offset pollutant loads associated with portions of the project area that cannot be physically treated.

Sovereign Lands Discussion: (Determining Location, Correct Form of Authorization, Content of Application, Assessment of Fees, Coordination with FDEP)

• Any work below the MHW line will require coordination with Tampa Port Authority

Operation and Maintenance/Legal Information: (Ownership or Perpetual Control, O&M Entity, O&M Instructions, Homeowner Association Documents, Coastal Zone requirements, etc.)

- The permit must be issued to the FDOT.
- Provide proof of ownership in the form of a deed or contract for sale.
- Provide appropriate O&M instructions.
- Provide detailed construction surface water management plan.

Application Type and Fee Required:

- SWERP Sections A, C and E of the ERP Application.
- < 640 acres of project area and <50 acres of wetland or surface water impacts \$3,106.00 Online Submittal

Other: (Future Pre-Application Meetings, Fast Track, Submittal Date, Construction Start Date, Required District Permits – WUP, WOD, Well Construction, etc.)

•

Disclaimer: The District ERP pre-application meeting process is a service made available to the public to assist interested parties in preparing for submittal of a permit application. Information shared at pre-application meetings is superseded by the actual permit application submittal. District permit decisions are based upon information submitted during the application process and Rules in effect at the time the application is complete.



American Consulting Engineers of Florida, LLC

2818 Cypress Ridge Blvd, Suite 200 Wesley Chapel, Florida 33544 Tel 813.435.2600 • Fax 813.435.2601 american@ace-fla.com • www.ace-fla.com

SWFWMD PRE APPLICATION MEETING MINUTES

| Meeting Date: | January 22, 2014 | Date Issued: | January 22, 2 | 2014 | | | |
|---------------|---|-------------------|-----------------|------------------|--|--|--|
| Location: | SWFWMD Tampa Office | | | | | | |
| Project Name: | US 41 PD&E Study from Kracker Avenue to south of Causeway Blvd. | | | | | | |
| Purpose: | To discuss stormwater management permitting criteria | | | | | | |
| Notes by: | Michael Ryan | Ameri | can Project #: | 5127041 | | | |
| Copies to: | Attendees, Andrew Goldsmith, Chris Larry Weatherby | topher Salicco, F | File: 5127041.B | .03, Bill Adams, | | | |

| <u>Attendees</u> | Representing | Phone | Fax or e-mail |
|-------------------------|-------------------------------|--------------|-------------------------------|
| Richard Alt | SWFWMD | 813-985-7481 | Richard.alt@wattermaters.org |
| Chastity 'Chaz' LaRiche | SWFWMD | 813-985-7481 | Chaz.LaRiche@watermatters.org |
| Andrew Goldsmith | American Consulting Engineers | 813-435-2602 | agoldsmith@acp-fl.com |
| Michael Ryan | American Consulting Engineers | 813-435-2623 | mryan@acp-fl.com |
| Christopher Salicco | American Consulting Engineers | 813-435-2617 | csalicco@acp-fl.com |

The following notes reflect our understanding of the discussions and decisions made at this meeting. If you have any questions, additions or comments, please contact us at the above address. We will consider the minutes to be accurate unless written notice is received within 10 working days of the date issued.

Water Quality Treatment:

Wet detention may not be sufficient and will only remove roughly 42% of nutrients. May require use of a treatment train with dry detention swale pretreatment. The governing water quality volume will be the greater of standard water quality (presumptive) or nutrient removal requirements.

If a WBID identifies no impairments for nutrients but is directly discharging to the impaired bay, then nutrient removal requirements will apply. The definition of directly connected is a gray area and engineering judgment should be used based on proximity to the bay. If the WBID identifies no impairments and is not within close proximity to be considered directly connected, such as WBIDs 1628A and 1632, then presumptive criteria will apply.

Compensatory treatment is allowable.

Water Quantity:

Open basin criteria. The design shall meet the 25-year 24-hour discharge attenuation, unless there exists a directly connected discharge to the bay (essentially an infinite basin). Engineering judgment will determine if the SWMF discharge is directly connected since there is no definitive definition of this. If a directly connected discharge is found to exist the 25-year attenuation criteria will not apply and the pond will be designed to release detained runoff as fast as possible. This could also apply to a SWMF located on the east side of the roadway if the SWMF discharges to a riverine system and is directly connected to the bay, the timing of the peak discharges between the onsite system and the riverine system will have to be evaluated to determine if 25-year attenuation criteria apply. For example, if the peak discharge from the onsite system occurs at hour 12 and the peak discharge from the riverine system occurs at hour 24, it will be assumed that the onsite system peak discharge will have no effect on the riverine system peak discharge.

Floodplain:

Richard Alt stated that the base flood elevations for Zone AE indicated on the FIRM are based on storm surge elevations and would not apply for floodplain encroachment estimates. Mr. Alt said to contact Dr. Sue for the riverine water surface profiles in the area. He stated that the riverine analysis used tailwaters of approximately 3 feet and the 100-year water surface profiles at U.S.41 would be significantly lower. He said that we should provide floodplain compensation based on flood elevations reported per the water surface profiles from Dr. Sue.

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SOUTHWEST FLORIDA WATER MANAGEMENT DISTRICT RESOURCE REGULATION DIVISION PRE-APPLICATION MEETING NOTES

FILE NUMBER:

PA 402518

Date: 8/19/2015 **Time:** 11:00

Project Name: FDOT US41 S of Causeway to Kracker Ave

Attendees: Richard Alt, Al Gagne, Andrew Goldsmith - American Consulting agoldsmith@acp-

fl.com William Adams, Larry Weatherby

County: Hillsborough Sec/Twp/Rge:

Total Land Acreage: 170 Project Acreage: 170 acres

Prior On-Site/Off-Site Permit Activity:

4 lane rural

• PA 400801, ETDM 5180

Project Overview:

Expand to 6 lane urban and suburban

Environmental Discussion: (Wetlands On-Site, Wetlands on Adjacent Properties, Delineation, T&E species, Easements, Drawdown Issues, Setbacks, Justification, Elimination/Reduction, Permanent/Temporary Impacts, Secondary and Cumulative Impacts, Mitigation Options, SHWL, Upland Habitats, Site Visit, etc.)

- Project is located in both the Tampa Bay/Coastal Basin and the Alafia Basin. Impacts in the Alafia basin
 may be located within the service area for the Tampa Bay Mitigation Bank. Will need to verify this. If so,
 they may be able to use a connectivity argument to mitigate Alafia impacts at the Tampa Bay Mit Bank.
 Will need to submit a cumulative impact analysis using a connectivity argument for tidal systems.
- Provide the limits of jurisdictional wetlands.
- Provide appropriate mitigation using UMAM for impacts, if applicable.
- Demonstrate elimination and reduction of wetland impacts.
- Maintain minimum 15 foot, average 25 foot wetland conservation area setback or address secondary impacts.
- If the project is located in a county which is listed as a coastal county under the Coastal Zone Management Act (CZM) and the project has wetland impacts, it will require a noticing period once the permit application is deemed complete. Wetland and/or surface waters impacts less than 1 acre in size will require a 10 day noticing period, prior to the issuance of the permit. Wetland and/or surface water impacts greater than 1 acre in size will require a 30 day noticing period, prior to the issuance of the permit. Permits could be issued as early as the 11th or 31st day, but staffs' schedule and workload will determine the actual issuance date.

Site Information Discussion: (SHW Levels, Floodplain, Tailwater Conditions, Adjacent Off-Site Contributing Sources, Receiving Waterbody, etc.)

- Existing roadway/intersections –
- WBIDs need to be independently verified by the consultant WBID 1682,1676, 1666A, 1664, 1621G, 1628A, 1632, 1637, and 1636
- Discharging to impaired waters in some areas.

Water Quantity Discussions: (Basin Description, Storm Event, Pre/Post Volume, Pre/Post Discharge, etc.)

- Demonstrate that discharges from proposed project area will not cause an adverse impact for a 25-year,
 24-hour storm event. Only SMF 12/13 will need to attenuate, all others (as shown during the meeting) will not require attenuation.
- Demonstrate that site will not impede the conveyance of contributing off-site flows.
- Demonstrate that the project will not increase flood stages up- or down-stream of the project area(s).
- Provide equivalent compensating storage for all 100-year, 24-hour riverine floodplain impacts if applicable.

Water Quality Discussions: (Type of Treatment, Technical Characteristics, Non-presumptive Alternatives, etc.)

- Provide water quality treatment for the required project area.
- In addition, must provide a net environmental improvement.
- Applicant must demonstrate a net improvement for the parameters of concern by performing a pre/post pollutant loading analysis based on existing land use and the proposed land use.
- Will acknowledge compensatory treatment to offset pollutant loads associated with portions of the project area that cannot be physically treated.

Sovereign Lands Discussion: (Determining Location, Correct Form of Authorization, Content of Application, Assessment of Fees, Coordination with FDEP)

• N/A. Tampa Port Authority owns the bottom lands in Hillsborough County. Will need to coordinate with EPC and the Tampa Port Authority.

Operation and Maintenance/Legal Information: (Ownership or Perpetual Control, O&M Entity, O&M Instructions, Homeowner Association Documents, Coastal Zone requirements, etc.)

- The permit must be issued to the FDOT.
- Provide proof of ownership in the form of a deed or contract for sale.
- Provide appropriate O&M instructions.
- Provide detailed construction surface water management plan.

Application Type and Fee Required:

- SWERP Sections A, C, and E of the ERP Application.
- < 640 acres of project area and < 50 acres of wetland or surface water impacts \$3,105.75

Other: (Future Pre-Application Meetings, Fast Track, Submittal Date, Construction Start Date, Required District Permits – WUP, WOD, Well Construction, etc.)

• In accordance with Rule 40D-1.603(2), F.A.C., no later than 30 days after submittal of an initial application of an Individual surface water management permit the applicant shall publish at the applicant's expense a notice of the District's receipt of the application in a newspaper having general circulation as defined in Chapter 50, F.S., in the county or counties in which the activity is proposed. Please provide documentation that such noticing has been accomplished. Note that the published notices of receipt for an ERP must be in accordance with the language provided in Rule 40D-1.603(10), F.A.C., and receipt of an affidavit establishing proof of this publication will be considered a completeness item of this ERP Application. Per Rule 40D-1.603(12), F.A.C., this must be received before the application will be considered complete and the 60-day timeframe for taking agency action on the application will commence.

40D-1.603(12) – "Applicants required to publish a notice of receipt of application must provide to the District a publisher's affidavit establishing proof of publication pursuant to Sections 50.041 and 50.051, F.S., before the application will be considered complete and the applicable timeframe for taking agency action on the application will commence."

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